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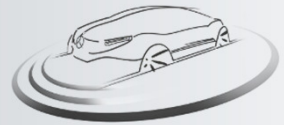
presented at the 10th Weimar Optimization and Stochastic Days 2013 /
Source: www.dynardo.de/en/library

Sensitivity of brake squealing concerning scattered component, joint and bearing properties

Dr. Ronaldo F. Nunes, Daimler AG, Mercedes-Benz Cars and M.Sc. Christian Büttner (Altair Engineering GmbH)

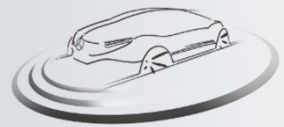
22.11.2013



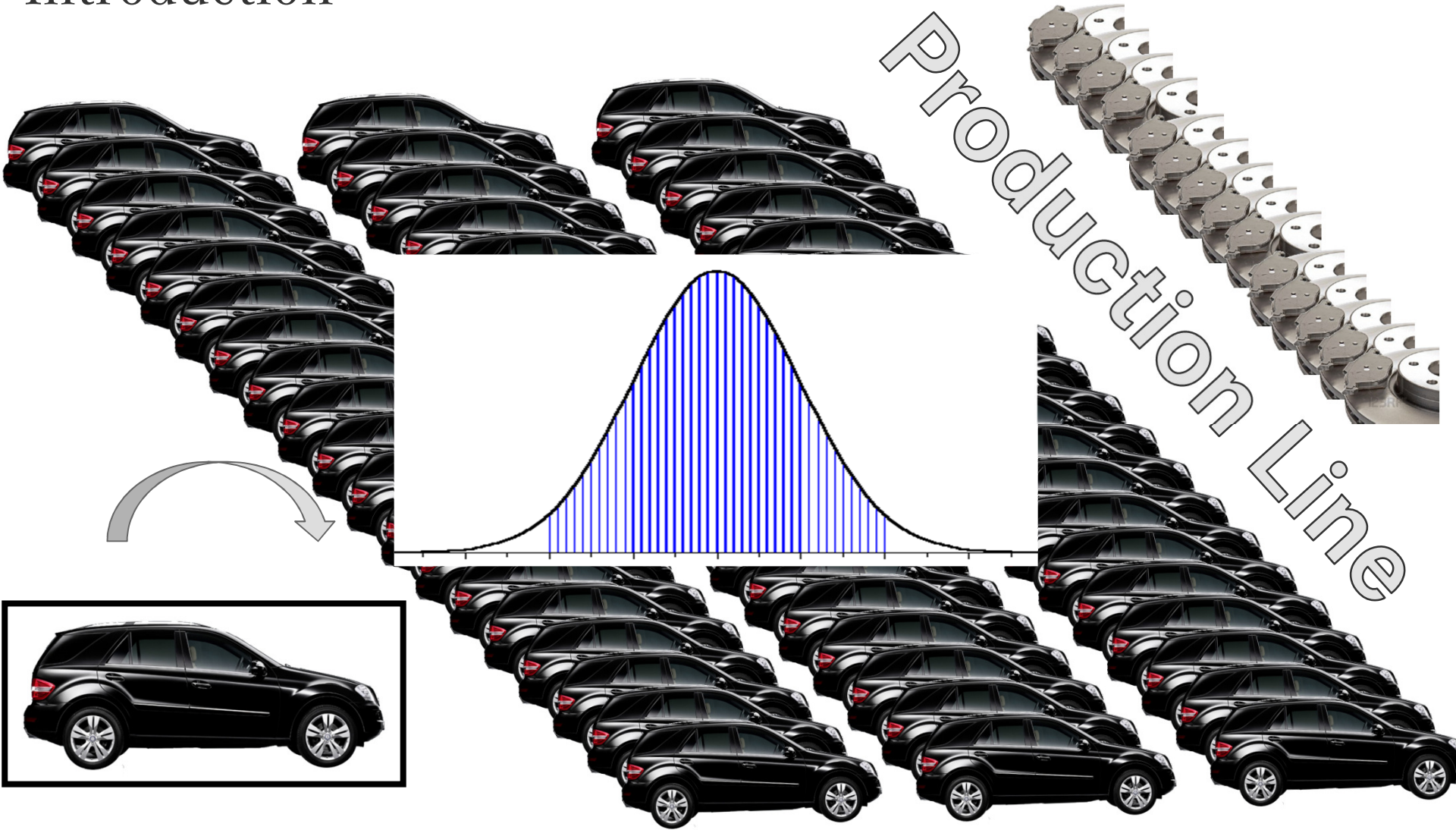


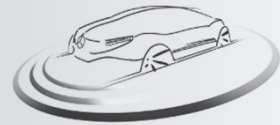
Agenda

- 1 Simulation, Bench and Vehicle
- 2 NVH - Target
- 3 NVH - Squealing Joints Influence
- 4 Summary

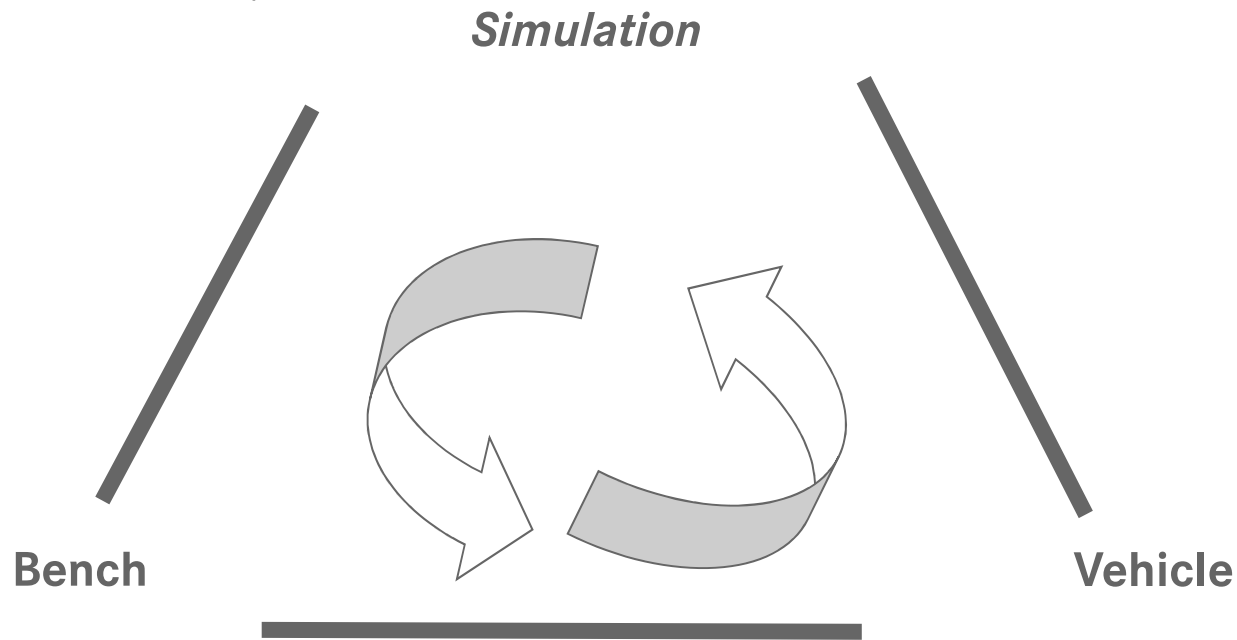


Introduction





Simulation, Bench and Vehicle (Interdisciplinary Strategy: Cross Correlation Simulation, Bench and Vehicle)



✓ **Quality Control regarding Brake disc Eigenfrequency, lining material, etc.**



Uncertain Parameters: E-Modulus, Material Density and Geometry (for example Knuckle)

Operating Points

Material
(Lining material,
Disc, Caliper, Axle,
Shim and so on)

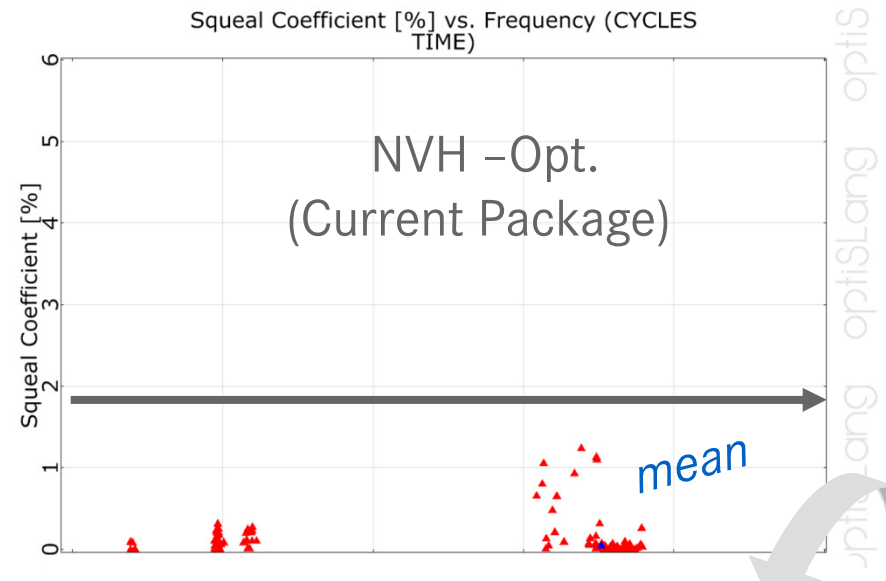
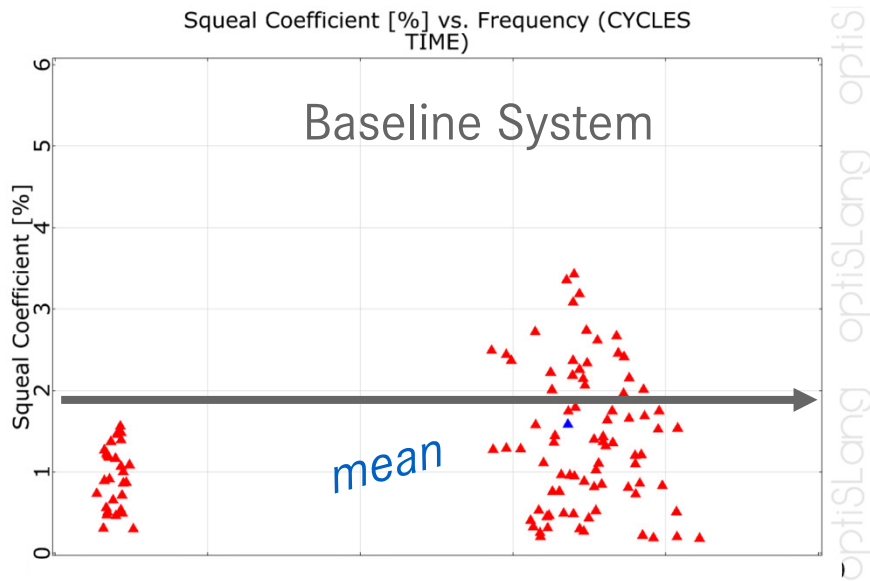
Geometry

#	Name	Distribution	Mean	CoV	Stddev	Lower Cut	Upper Cut	Format	Active	Constant
1	friction_disc_pad	Uniform	0.6	0.09622504486493...	0.05773502691896...	0.5	0.7	%20.13e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
2	ROTATING_VELOCIT...	Uniform	2.5	0.34641016151377...	0.86602540378443...	1.0	4.0	%20.13e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
3	OPERATING_PRESSURE	Uniform	10250.0	0.5491868414242782	5629.165124598851	500.0	20000.0	%18.11e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
4	DISK	Uniform	9.75E7	0.07401926528072...	7216878.364870323	8.5E7	1.1E8	%14.7e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
5	E1_Pad	Normal	1.289E7	0.1	1289000.0	-	-	%20.13e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
6	E3_Pad	Uniform	750000.0	0.19245008972987...	144337.567297406...	500000.0	1000000.0	%20.13e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
7	SHIM_ADHESIVE	Normal	500000.0	0.01	5000.0	-	-	%9.2f	<input checked="" type="checkbox"/>	<input type="checkbox"/>
8	SHIM_ELASTOMERE	Normal	5000000.0	0.01	50000.0	-	-	%20.13e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
9	SHIM_STEEL	Normal	-	-	-	-	-	%20.13e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
10	AL	Normal	-	-	-	-	-	%20.13e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
11	AL_KNUCKLE	Normal	-	-	-	-	-	%20.13e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
12	AL_TCA	Normal	-	-	-	-	-	%20.13e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
13	AL_SUSPENSION	Normal	-	-	-	-	-	%20.13e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
14	Caliper	Normal	-	-	-	-	-	%20.13e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
15	inner_shoe	Normal	-	-	-	-	-	%20.13e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
16	outer_shoe	Normal	-	-	-	-	-	%20.13e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
17	Anchor	Normal	-	-	-	-	-	%20.13e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
18	Steel	Normal	-	-	-	-	-	%11.5e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
19	ST100C6	Normal	-	-	-	-	-	%11.5e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
20	D4512	Normal	-	-	-	-	-	%12.2f	<input checked="" type="checkbox"/>	<input type="checkbox"/>
21	Piston	Normal	-	-	-	-	-	%11.2f	<input checked="" type="checkbox"/>	<input type="checkbox"/>
22	SHIM_ADHESIVE_RHO	Normal	-	-	-	-	-	%10.4e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
23	SHIM_ELATOMERE_R...	Normal	-	-	-	-	-	%10.4e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
24	SHIM_STEEL_RHO	Normal	-	-	-	-	-	%10.4e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
25	AL_RHO	Normal	-	-	-	-	-	%10.4e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
26	AL_KNUCKLE_RHO	Normal	-	-	-	-	-	%10.4e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
27	AL_TCA_RHO	Normal	2.7E-6	0.01	2.7E-8	-	-	%10.4e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
28	AL_SUSPENSION_RHO	Normal	2.7E-6	0.01	2.7E-8	-	-	%10.4e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
29	DISK_RHO	Normal	7.035E-6	0.01	7.035E-8	-	-	%9.3e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
30	Caliper_RHO	Normal	7.03E-6	0.01	7.03E-8	-	-	%10.4e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
31	Piston_RHO	Normal	2.09E-6	0.01	2.09E-8	-	-	%10.4e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
32	inner_shoe_rho	Normal	7.8E-6	0.01	7.8E-8	-	-	%10.4e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
33	outer_shoe_rho	Normal	7.8E-6	0.01	7.8E-8	-	-	%10.4e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
34	Anchor_RHO	Normal	7.295E-6	0.01	7.295E-8	-	-	%9.3e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
35	D4512_RHO	Normal	7.2E-6	0.01	7.2E-8	-	-	%7.1e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
36	Lining_RHO	Normal	2.57E-6	0.01	2.57E-8	-	-	%8.2e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
37	ST100C6_RHO	Normal	7.82E-6	0.01	7.82E-8	-	-	%11.5e	<input checked="" type="checkbox"/>	<input type="checkbox"/>
38	KNUCKLE_SHAPE1	Uniform	0.5	0.5773502691896258	0.28867513459481...	0.0	1.0	%6.4f	<input checked="" type="checkbox"/>	<input type="checkbox"/>
39	KNUCKLE_SHAPE2	Uniform	0.5	0.5773502691896258	0.28867513459481...	0.0	1.0	%6.4f	<input checked="" type="checkbox"/>	<input type="checkbox"/>

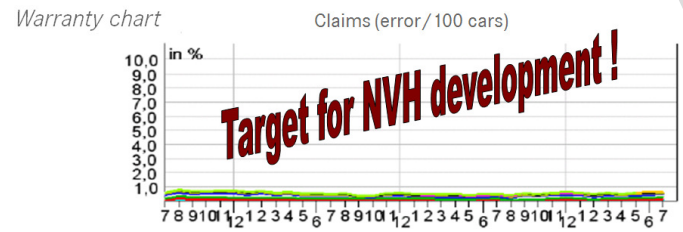
Notice: Factor 1 means 0.8 to 1.5 mm tolerance



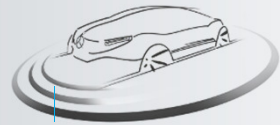
Robustness Analysis Combined with Optimization Strategy (120 Designs – Complex Eigenvalue Analysis)



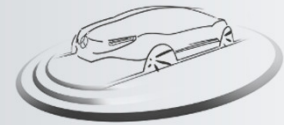
NVH - Target : Focus to find out the best solution taking into account the influence of uncertain parameters



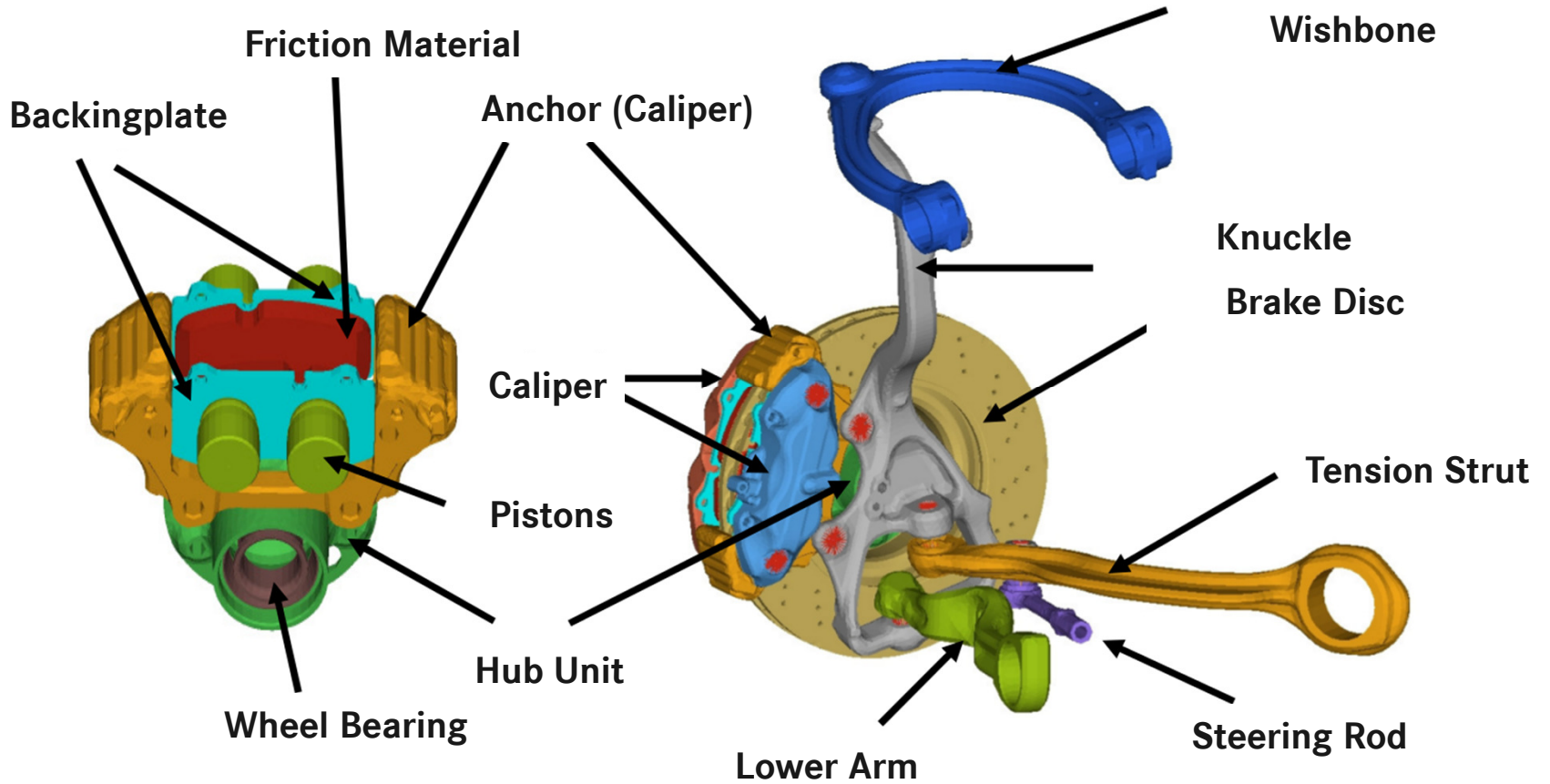
...you get ideal curves with constant slopes at low percentage values

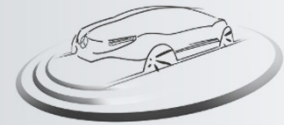


NVH – Squealing Joints Influence



CAD Model – Car Brake and Suspension





Background: Brake Squeal Analysis

Mathematical Equations

➤ $[M \lambda + D \lambda + C] \{\omega\} = 0$

➤ $\lambda = \alpha \pm i\omega$

α = Real Part

ω = Imaginary Part (Squeal Frequency)

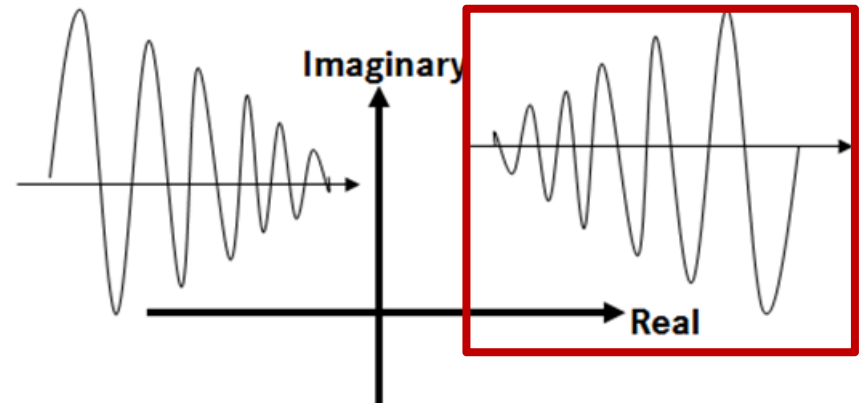
Complex Eigenvalue Analysis (CEA)

➤ $x(t) = A * e^{\lambda t} = A * e^{(\alpha \pm i\omega)t}$
 $= e^{\alpha t} (A1 * \cos \omega t + A2 * i \sin \omega t)$

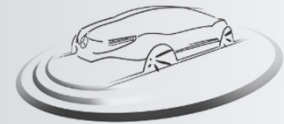
Stable / Unstable – Evaluation of complex Modes

➤ $\alpha < 0$ System is stable

➤ $\alpha > 0$ System not stable

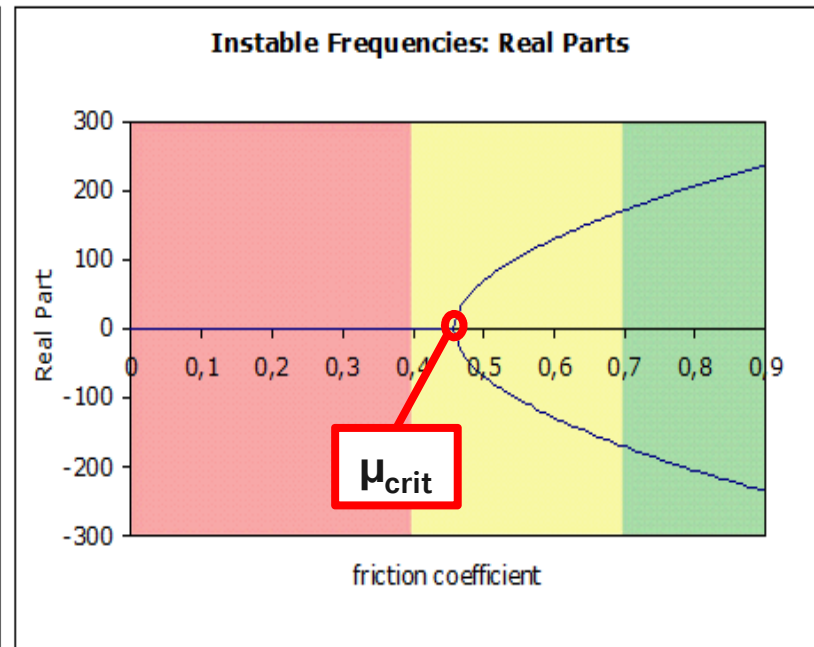
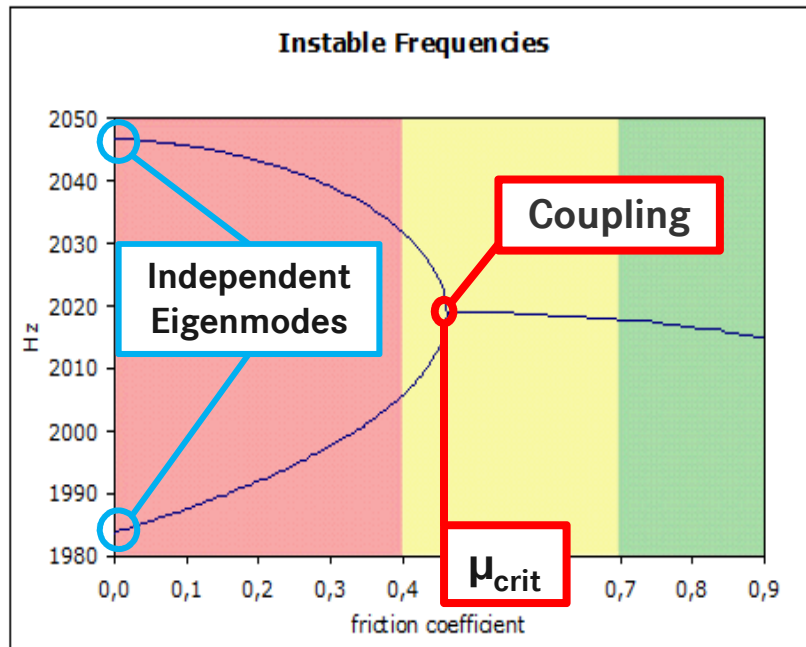


Positive α indicates a system behavior with an increasing amplitude of the brake oscillation



Background: Complex Eigenvalue Analysis

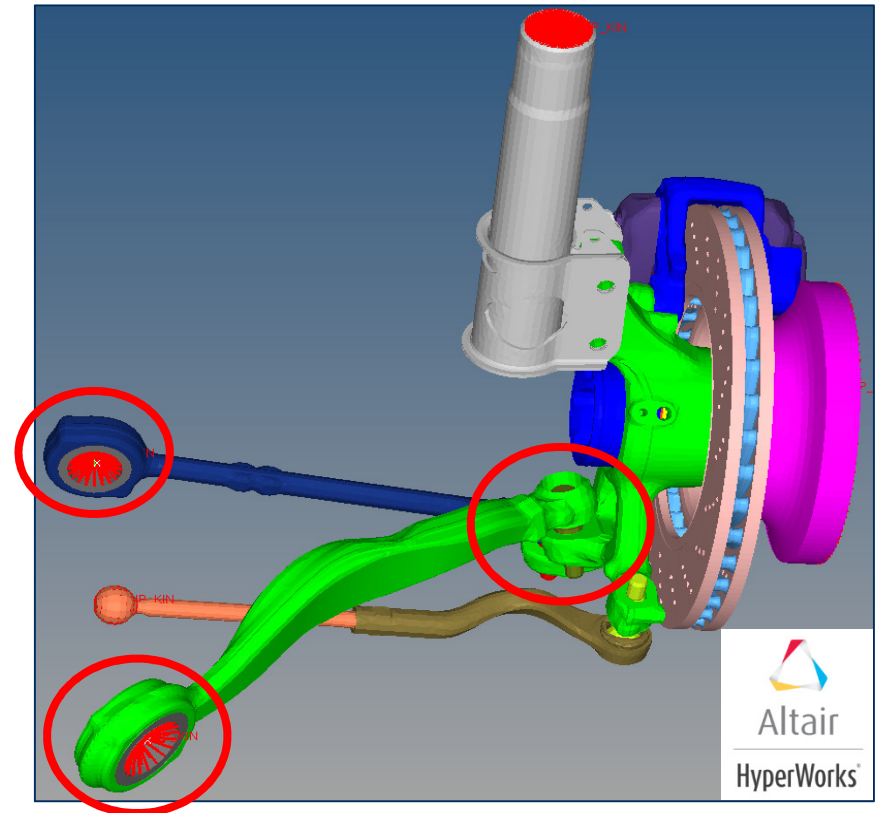
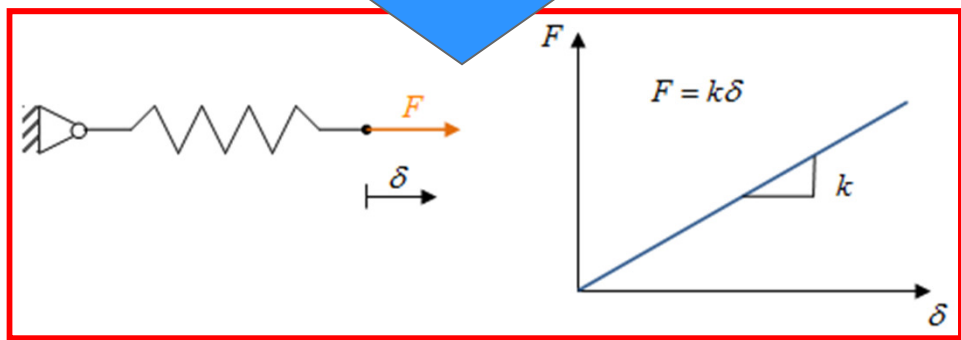
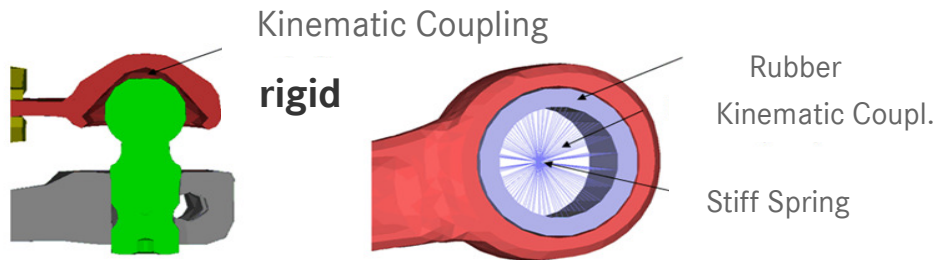
- Without Friction: Independent Eigenmodes
- Convergence of Eigenfrequencies with increasing μ
- Mode Coupling at μ_{crit}
- **Unstable System (Squealing Propensity)**





Joints Modeling

- Bearings, Ball Joints and Kinematic Description





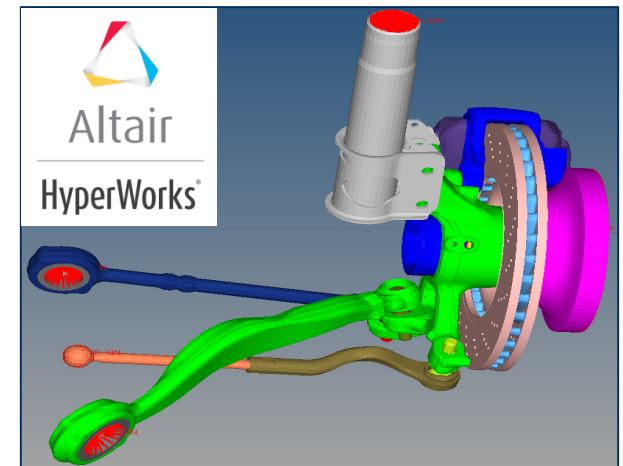
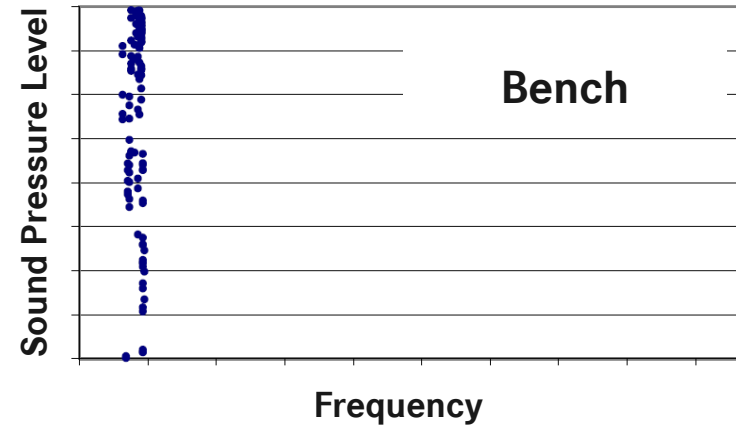
Bench Test – Noise Problem

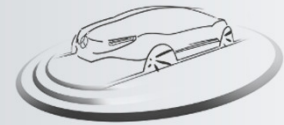
- Noise problem identified
- **Deterministic FE simulation was not able to find the critical frequency !!**



➤ Sensitivity Analysis

Ball Joints, Bearings stiffness
Pad and Disc stiffness/Geometry
Brake Pressure



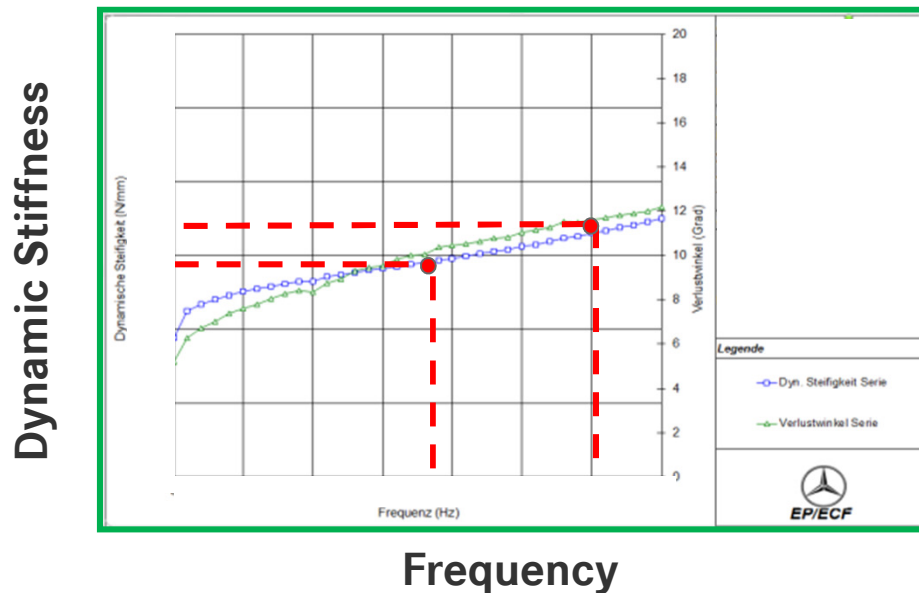


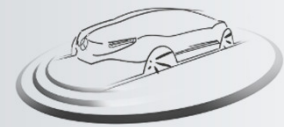
Material Behavior in CEA

- Complexe Eigenvalue Analysis investigates **Stationary System**

$$[Mp^2 + Cp + K] \{u\} = 0$$

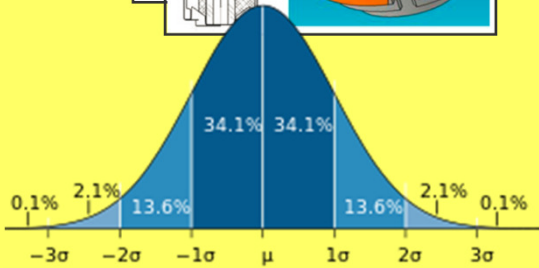
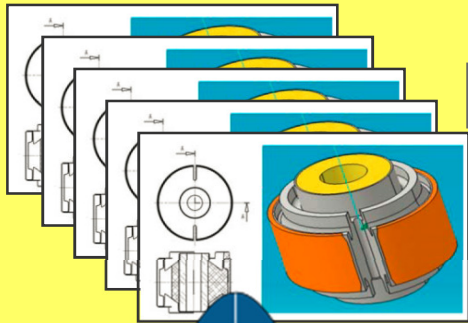
- Frequency, amplitude and temperature depending behavior not considered in single Calculation





Workflow: Sensitivity Analysis

Variation of Material and Geometry



FEM Process

Stable?
→ Calculation

$$[M \lambda + D \lambda + C] \{\omega\} = 0$$

$$\lambda = \alpha \pm i\omega$$

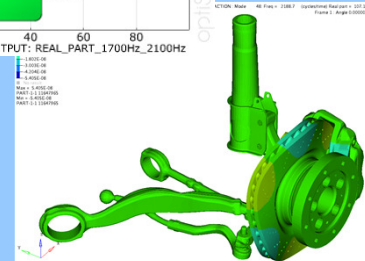
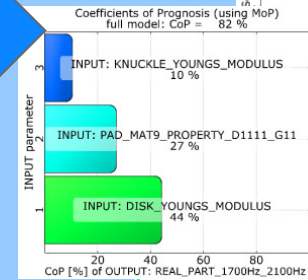
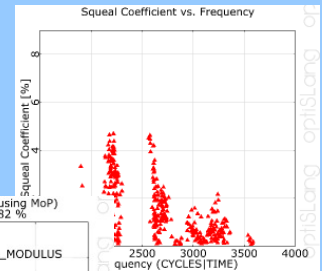
α = Real Part

ω = Imaginary Part



Post Processing

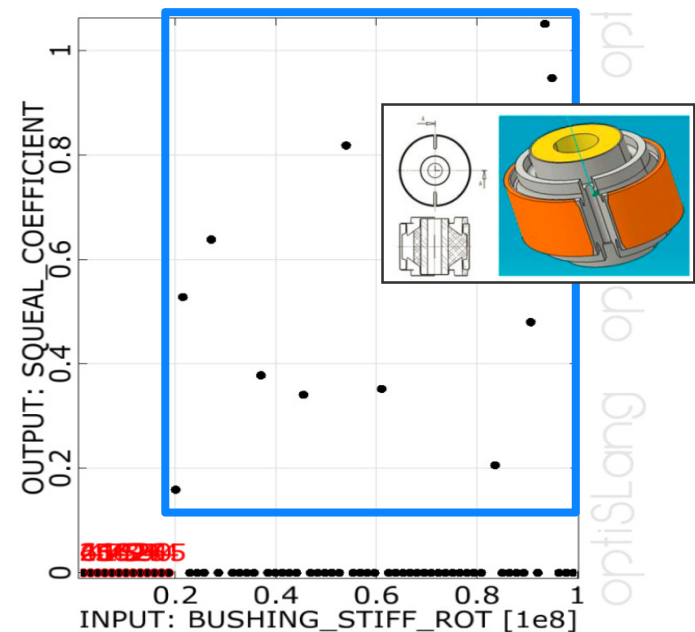
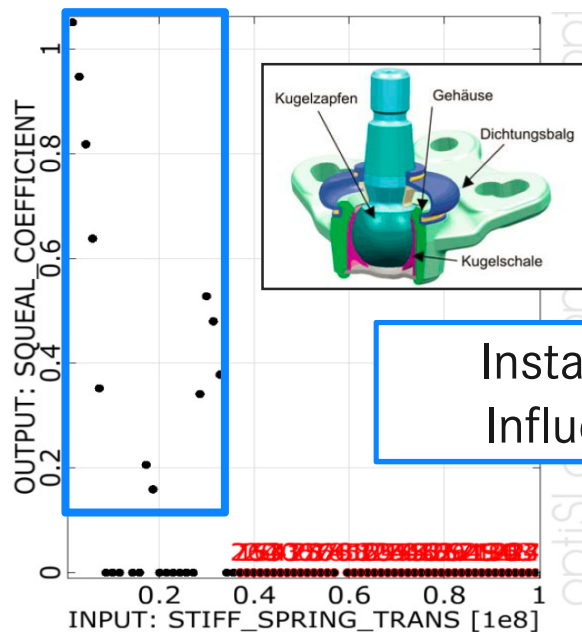
Statistical Evaluation of the Analysis

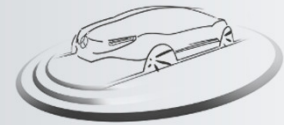




Sensitivity Analysis: Joints Influence

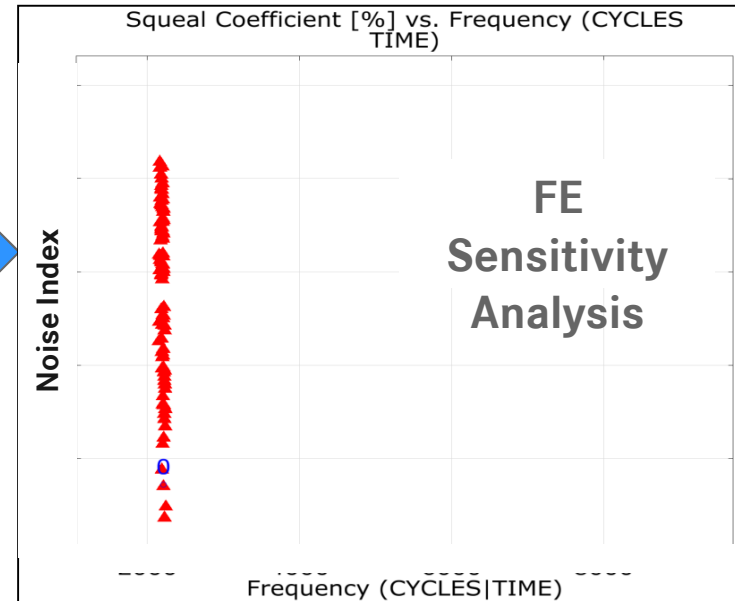
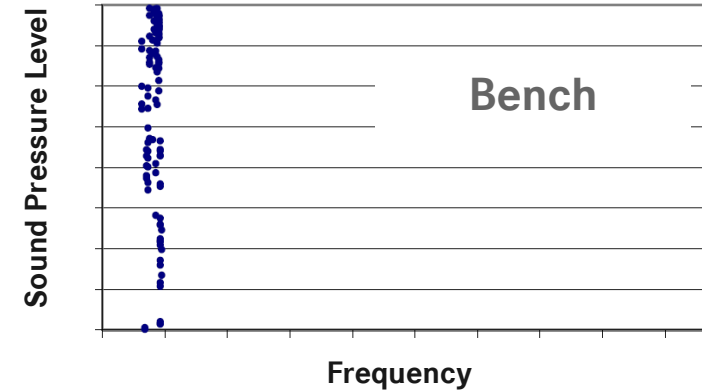
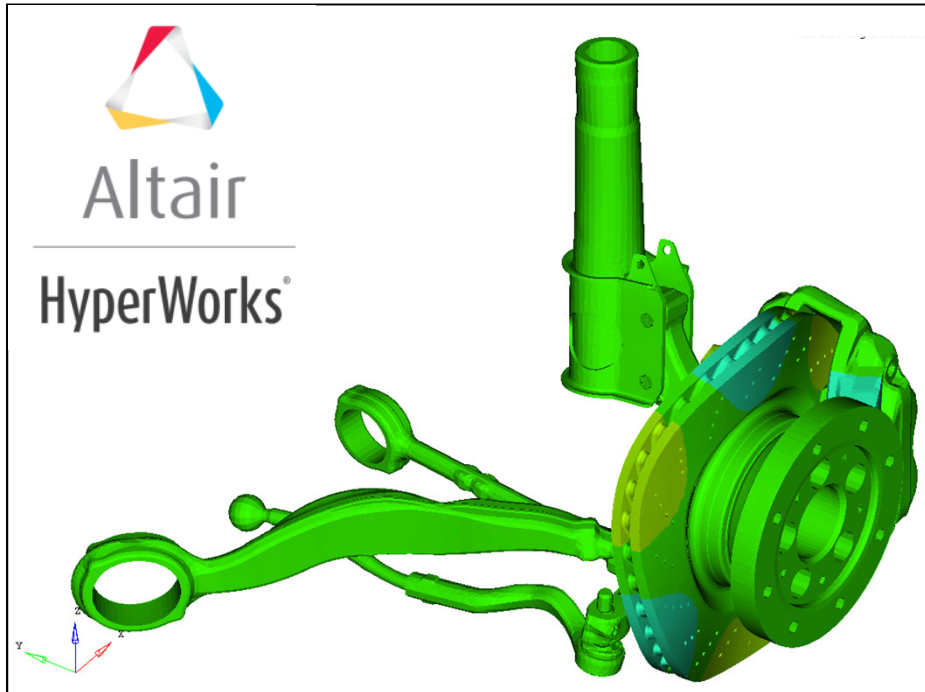
- Dynamic Measurements Available: Ball joints and Bearings
- **Sensitivity Analysis was adopted in order to identify the influence of Joint stiffness to the noise problem**

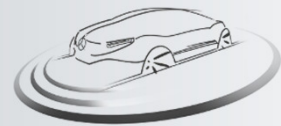




Bench and Sensitivity Analysis Validation

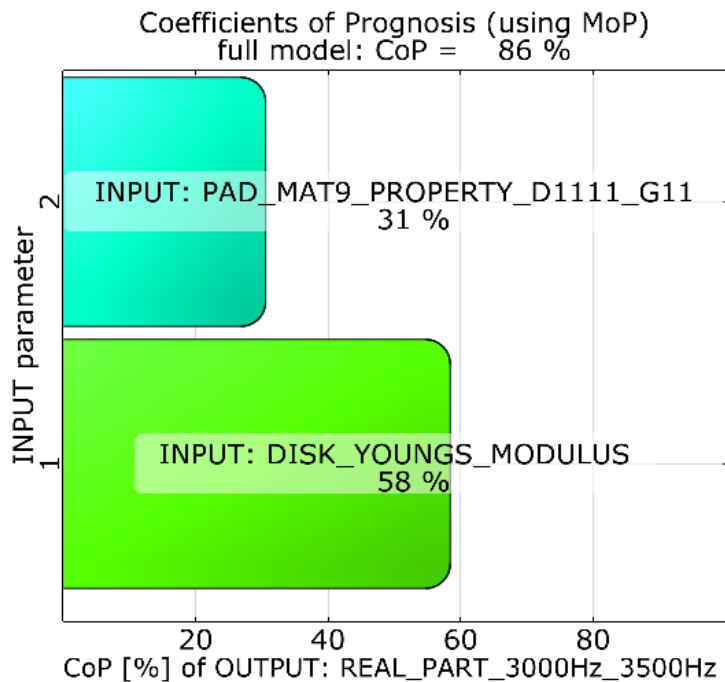
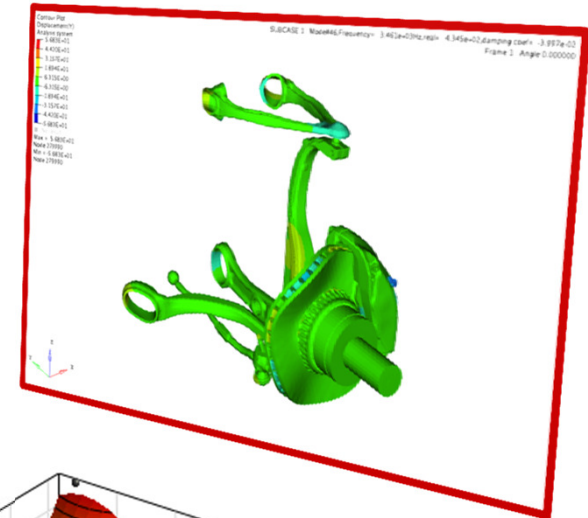
- Frequency identified
- Additional optimization to fix the problem



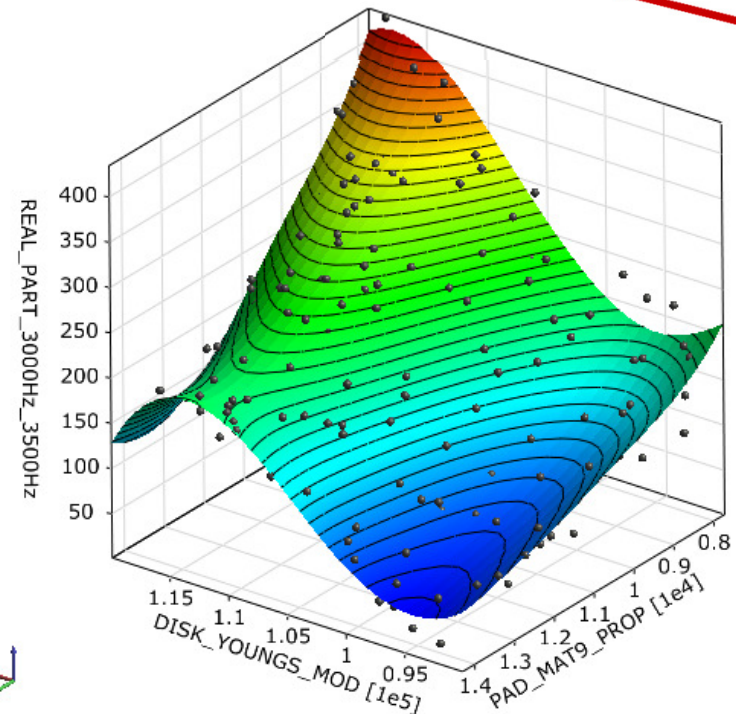


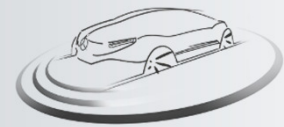
Model Improvements

- Better Identification of main influences and local minimum / maximum
- Better prediction of system behavior



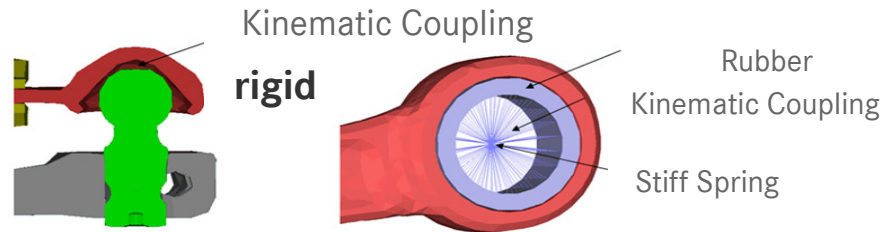
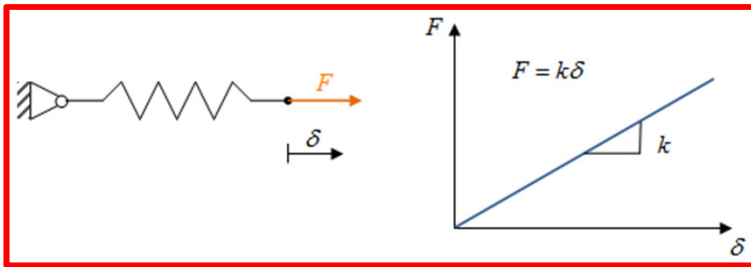
optiSlang or



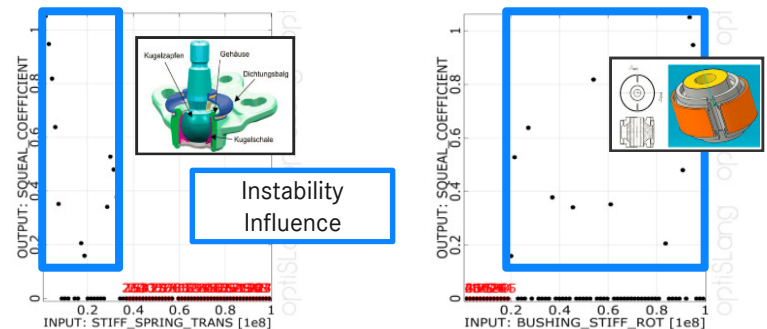


Conclusion

- Improvements in Modelling Brake System
 - Better Identification of main influences
 - Better prediction of system behavior
 - Results fitting better with bench vehicles



- Using Sensitivity Analysis
 - Identification of ideal parameter range
 - Joint parameters haven't a strong influence





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Thank you for your attention !

