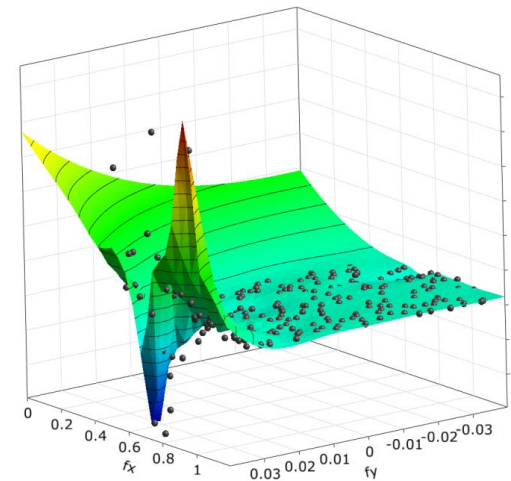
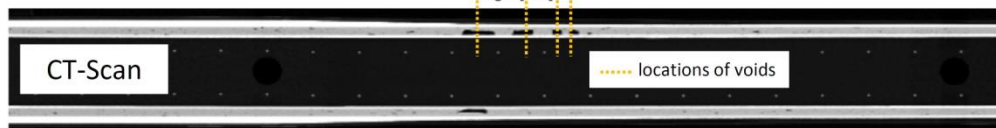
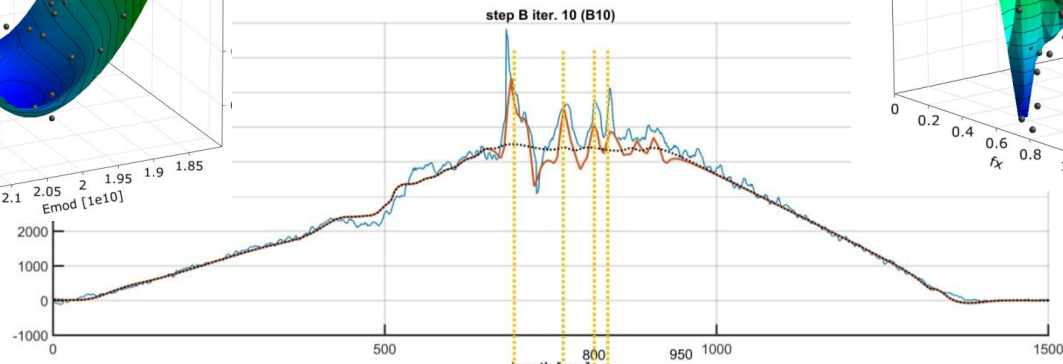
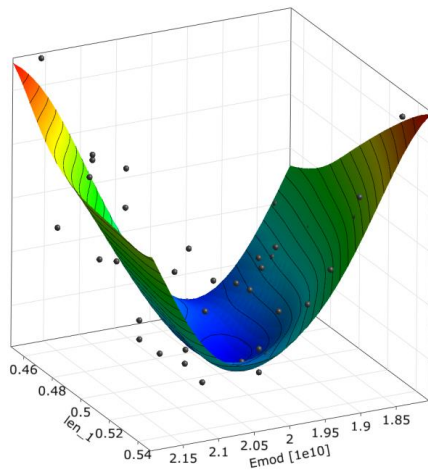


Parameter Identification based on quasi-continuous strain data captured by high resolution fiber optic sensing

Parameteridentifikation auf Basis faseroptisch gemessener quasi-kontinuierlicher Dehnungssignale

Andreas Künzel
TU Berlin



Parameter Identification based on quasi-continuous strain data captured by high resolution fiber optic sensing

1. Motivation
2. Parameter identification
3. Quasi-continuous strain data
4. Fiber-optic strain measurement
5. Stepwise parameter identification approach
6. Experimental work
7. Summary and outlook

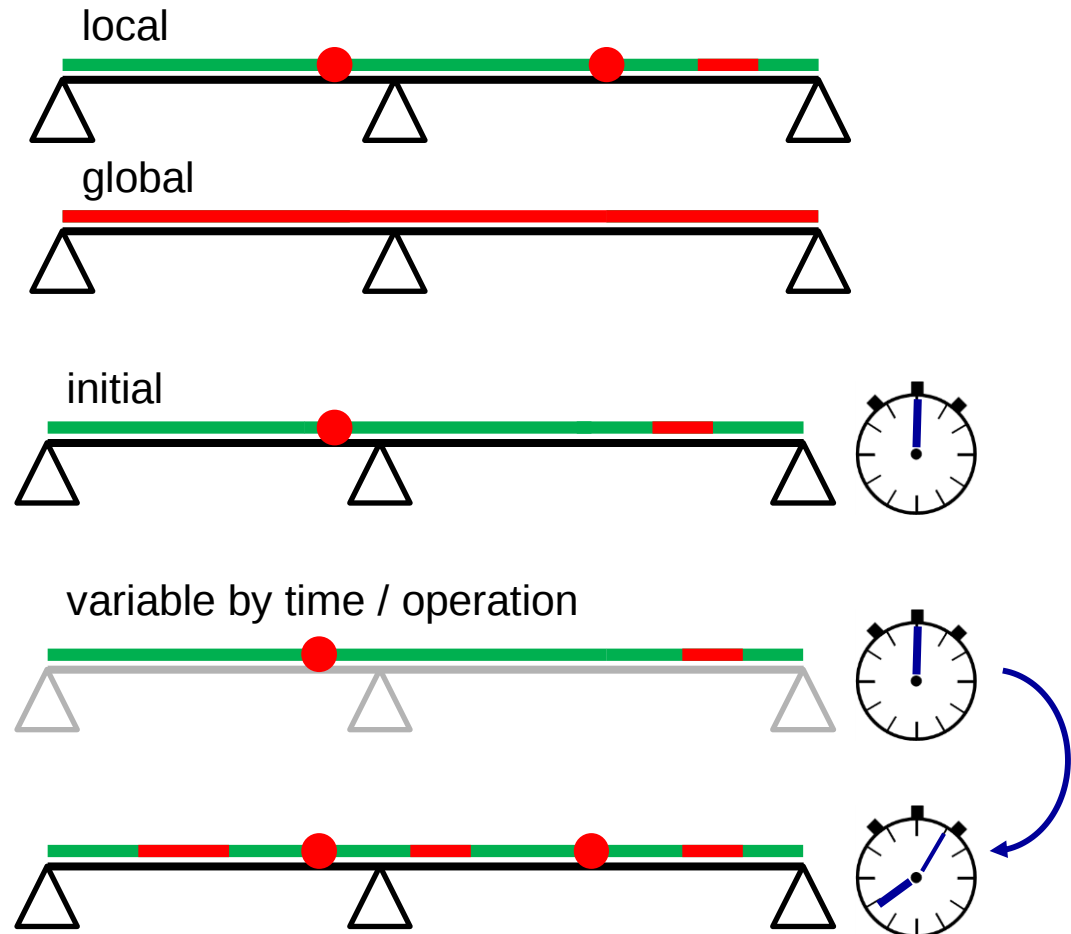
Structural Health Monitoring (SHM)



Assessment of structural integrity

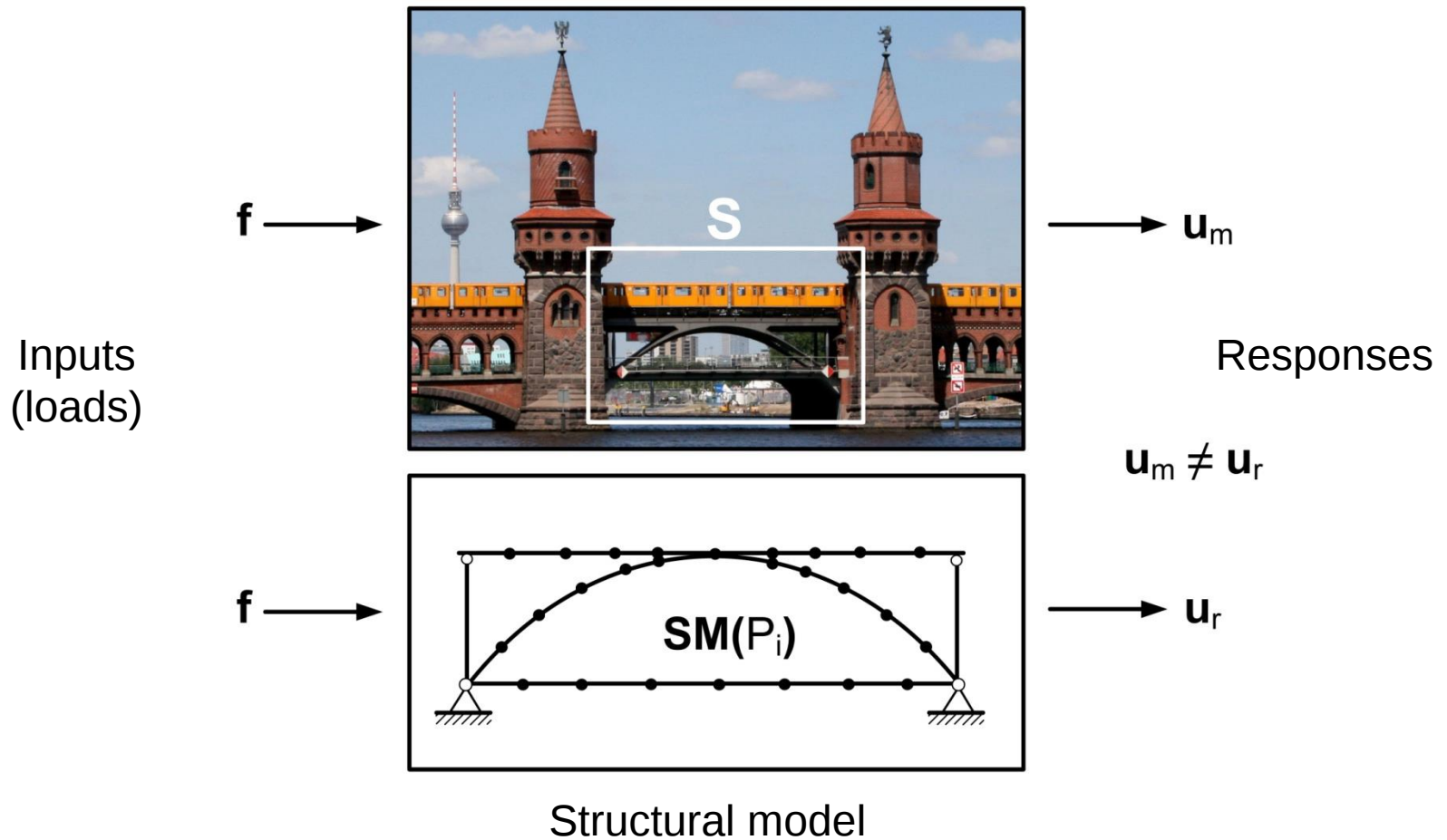
- 1) Capture of initial state / reference state
- 2) Identification of imperfections and damage
- 3) Prediction of future state by physically meaningful model

Types of degradation



Basic approach

Structural system



Procedure

design variables:

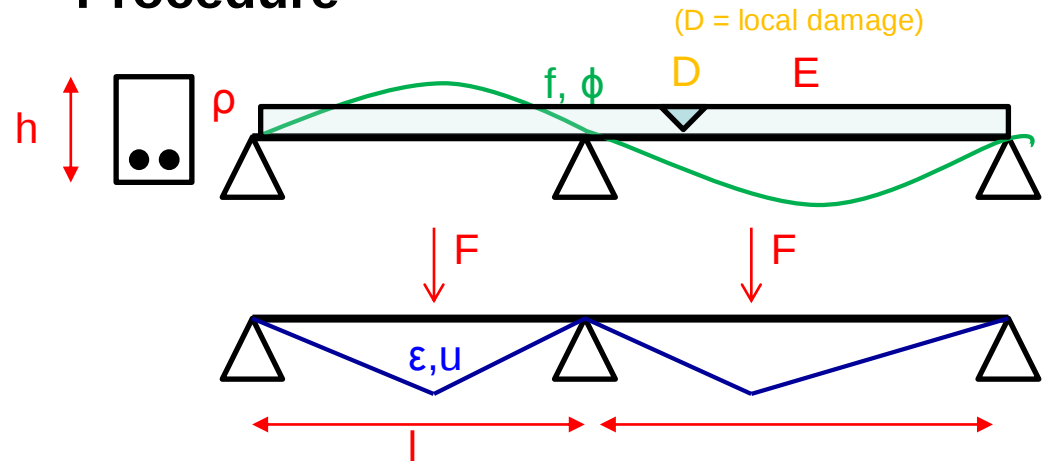
global
local

$$\mathbf{p} = \begin{bmatrix} E \\ h \\ I \\ \rho \\ F \\ D \\ \dots \end{bmatrix}$$

system responses:

derived
direct

$$\mathbf{v} = \begin{bmatrix} f \\ \phi \\ \epsilon \\ u \\ \dots \end{bmatrix}$$



Vector of measured responses

Parameters /
design variables

Vector of residuals: $\epsilon_w = \mathbf{W}_v \cdot \epsilon = \mathbf{W}_v(\mathbf{v}_M - \mathbf{v}(p))$

Objective function: $f(p) = \sum \epsilon_{wi}^2$

Weighting matrix
e.g. identity matrix

Optimization task: $\min f(p)$

Parameter identification is basically an optimization task which can be performed in many ways



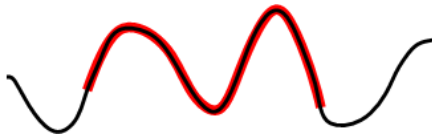
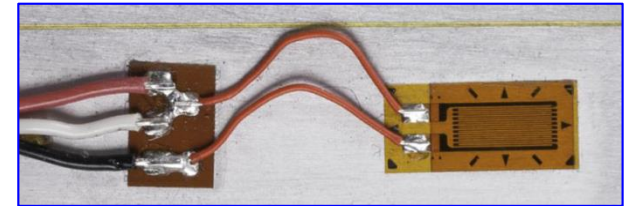
Use OptiSlang

3. Quasi-Continuous Strain Data

From discrete to quasi-continuous measurement data



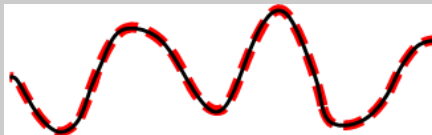
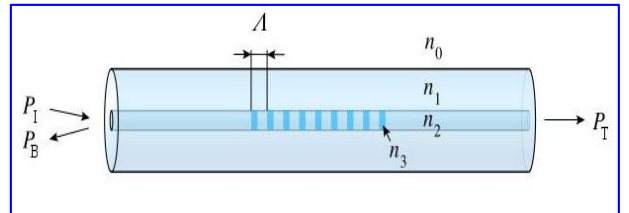
Point sensor,
e.g. strain gauge, accelerometer,
temperature sensor,
displacement sensor



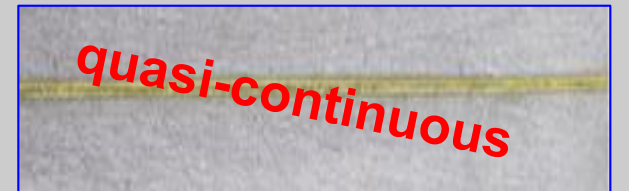
Integrating sensor, e.g. fiber-
optic extensometer



Distributed sensor, e.g. Fiber-
Bragg-Grating Sensor

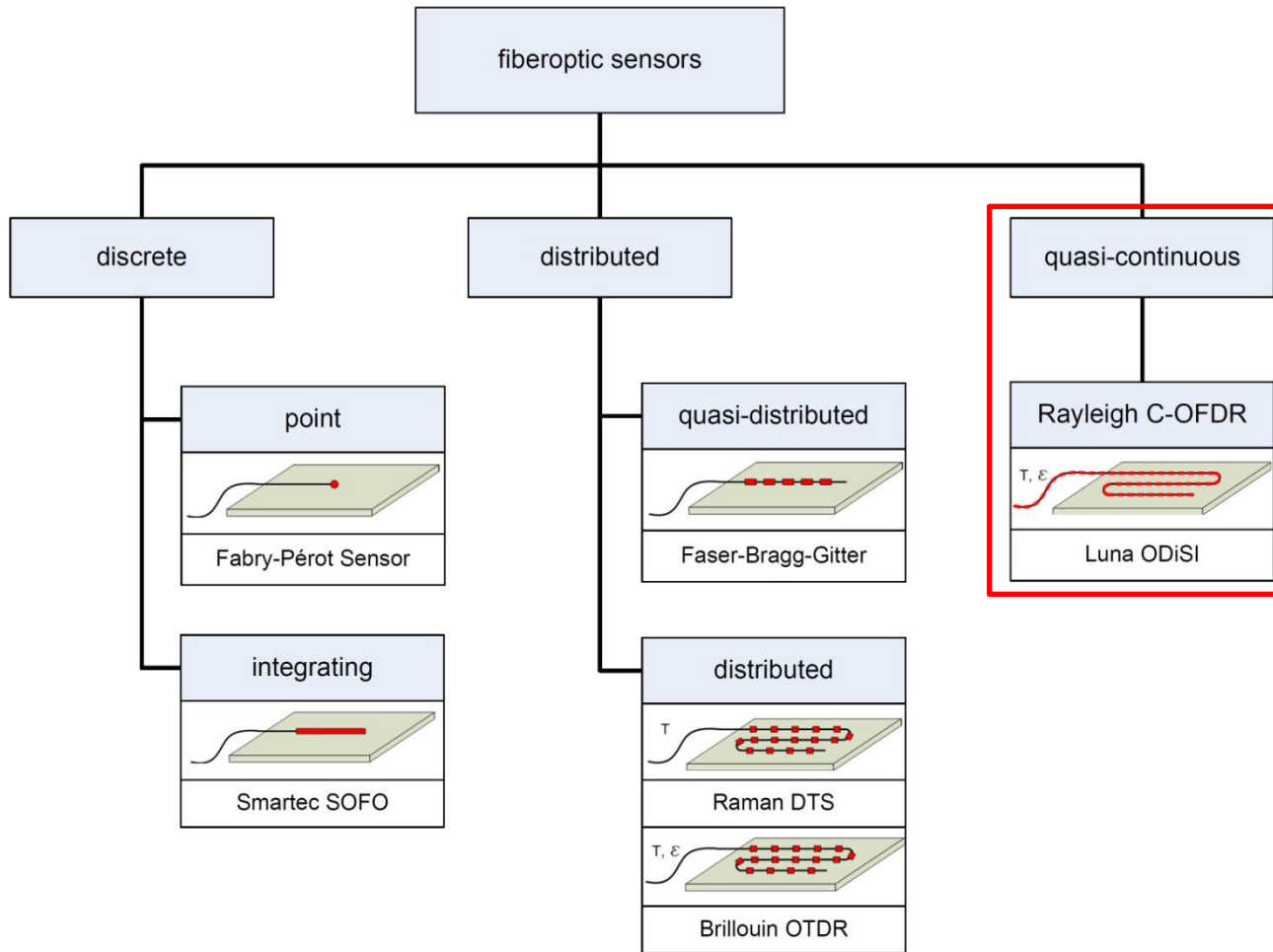


High resolution sensor, e.g.
Rayleigh-based fiber-sensing

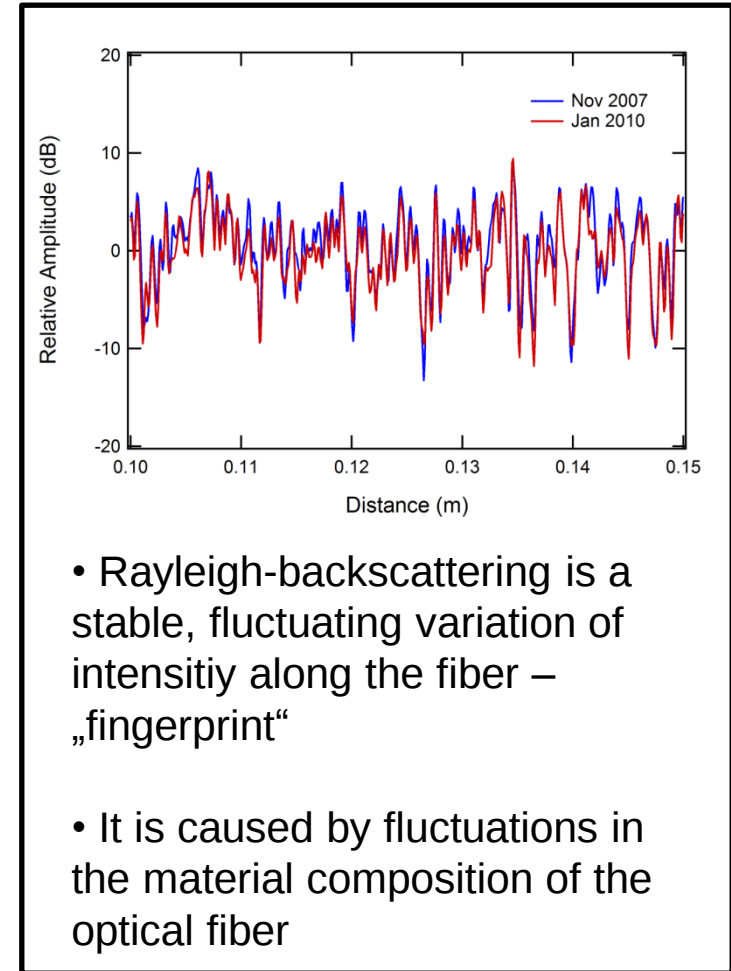
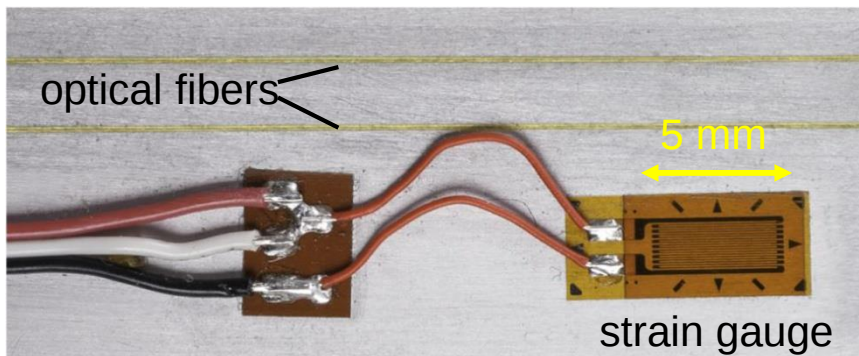
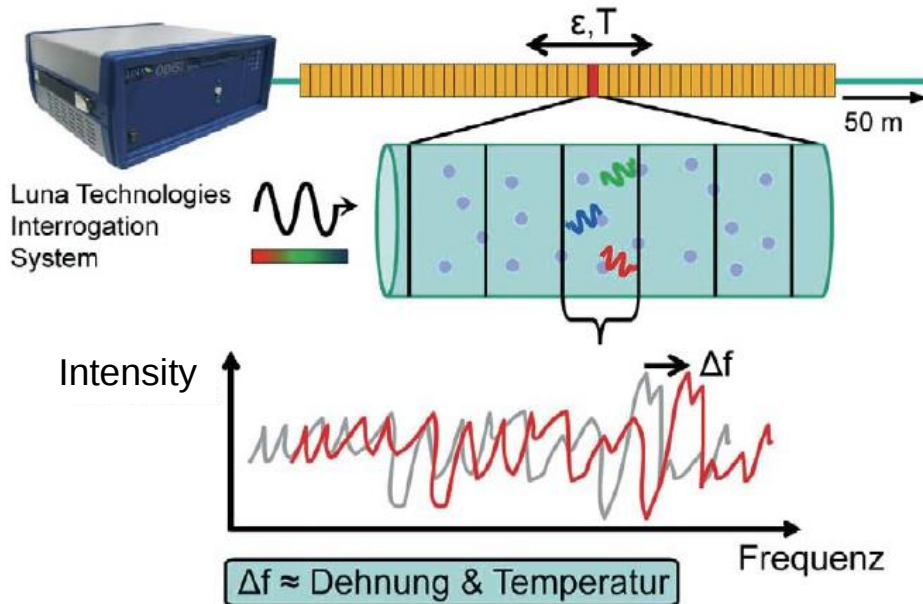


3. Quasi-Continuous Strain Data

Fiber optic sensing topologies



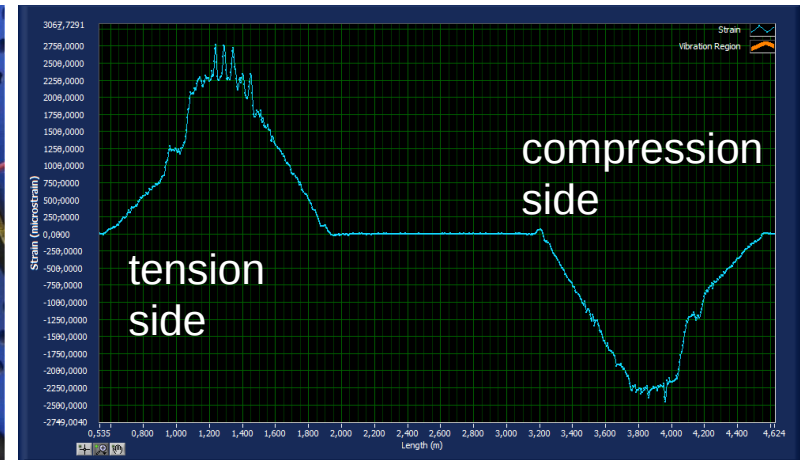
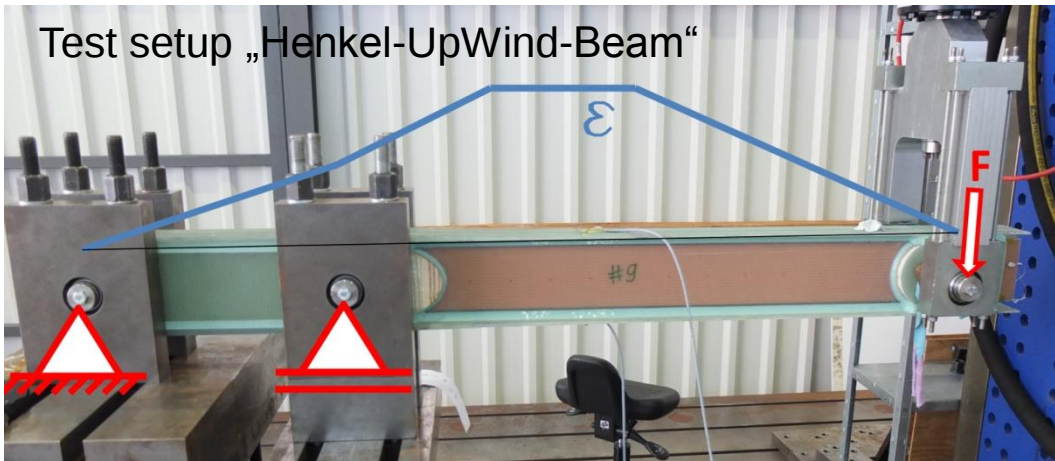
Principle: Rayleigh-scattering based strain sensing



Alle Bilder: Quelle: Luna Technologies

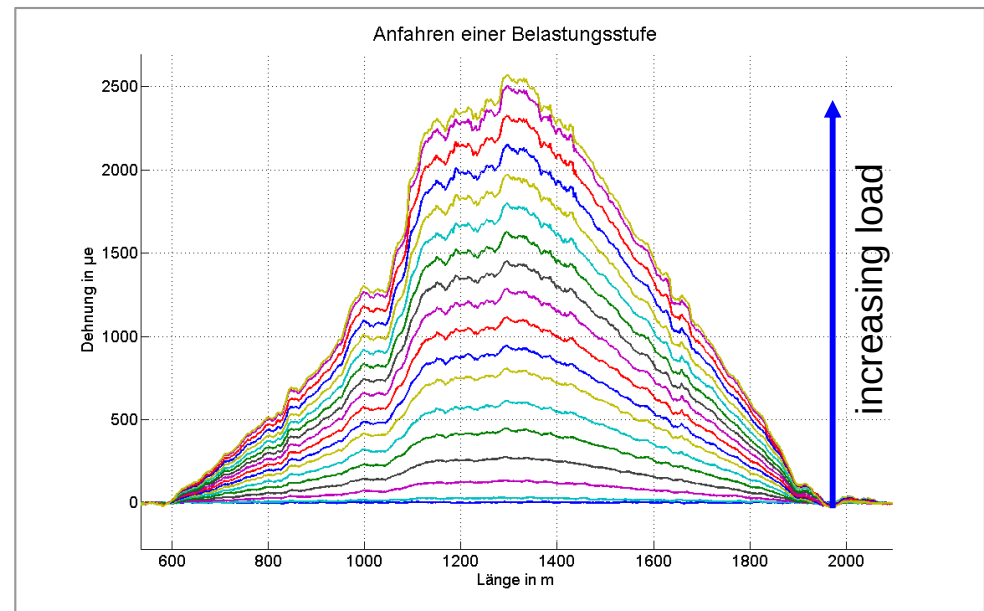
4. Fiber-Optic Strain Sensing

Test setup „Henkel-UpWind-Beam“



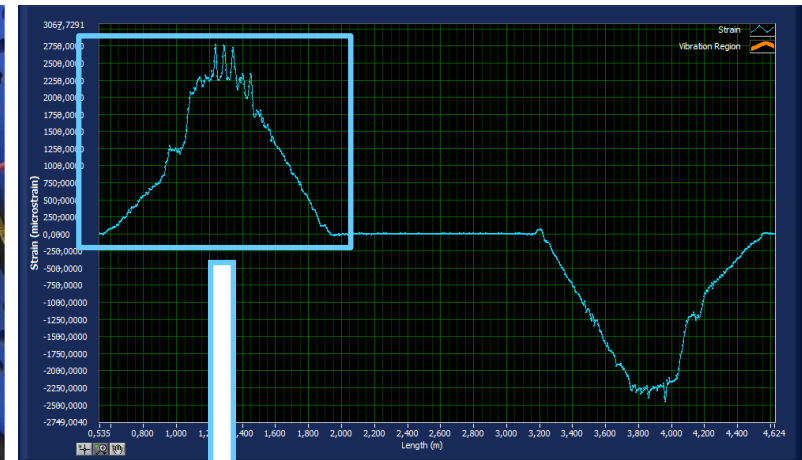
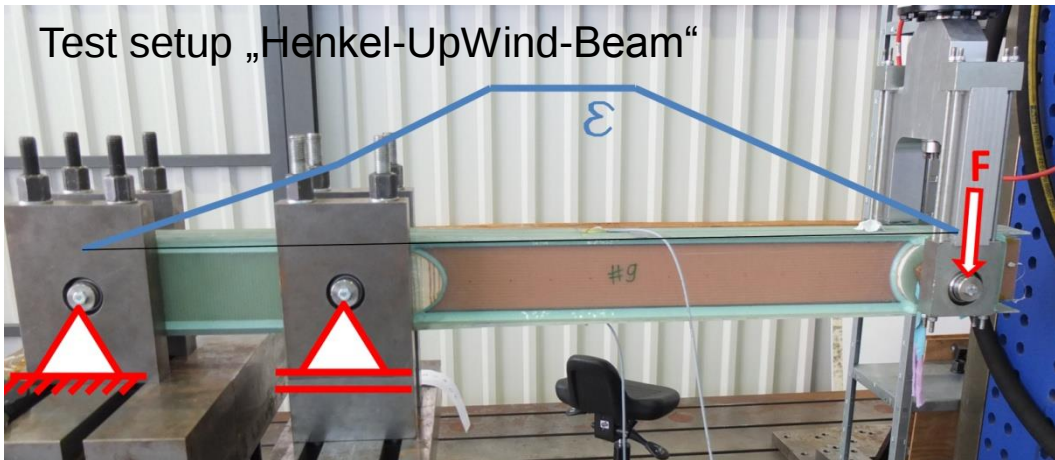
ODiSI System (Luna Technologies):

- Fiber length max. 10 m / 50 m
- Spatial resolution 1,25 mm / 5 mm
- Noise level 20 $\mu\epsilon$ / 5 $\mu\epsilon$
- Measurement rate 23,5 Hz / 50 Hz
- max. measurable strain ca. 1%



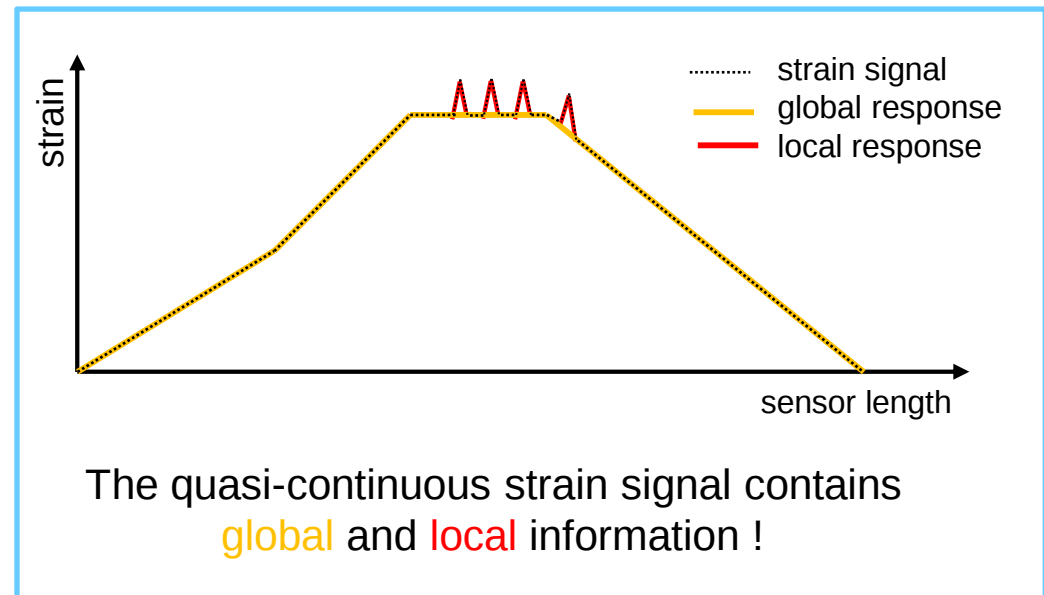
4. Fiber-Optic Strain Sensing

Test setup „Henkel-UpWind-Beam“

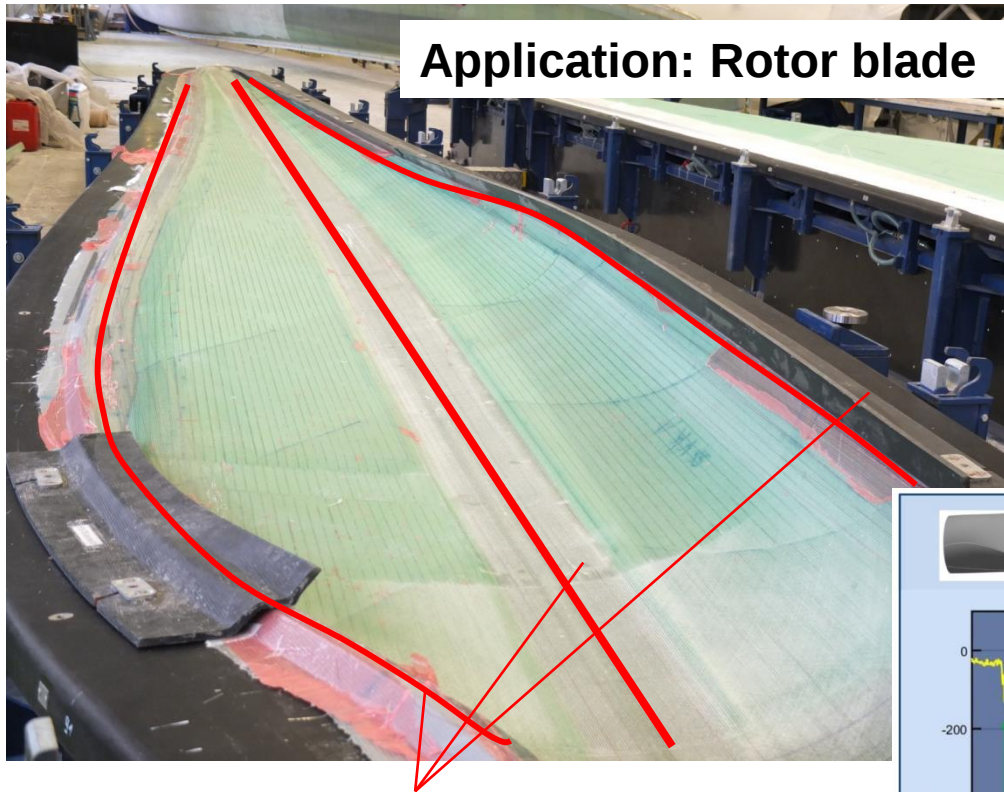


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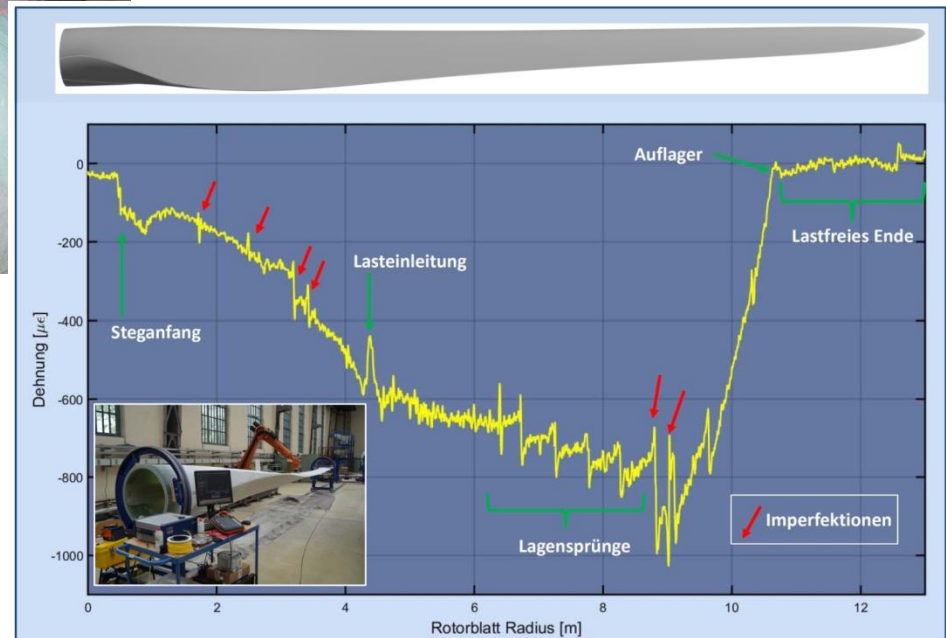
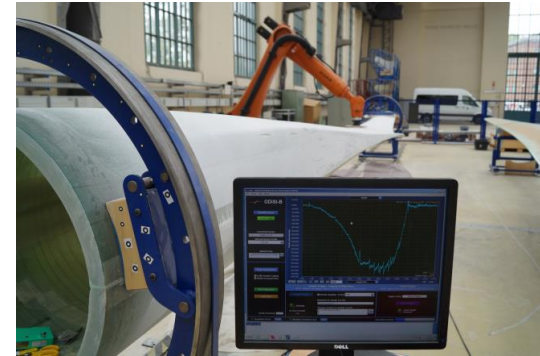
4. Fiber-Optic Strain Sensing



- Sensor positions:
- Leading and trailing edge
 - Spar caps

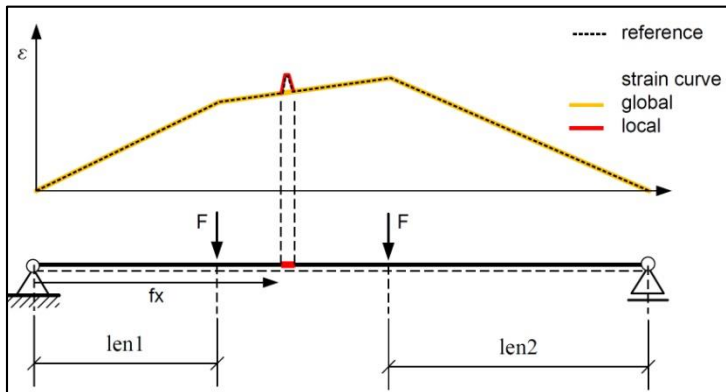
Interpretation of measured signal

Strain in the fiber along the spar cap due to bending load and beam-like support



5. Stepwise Parameter Identification Approach

Quasi-continuous strain signal

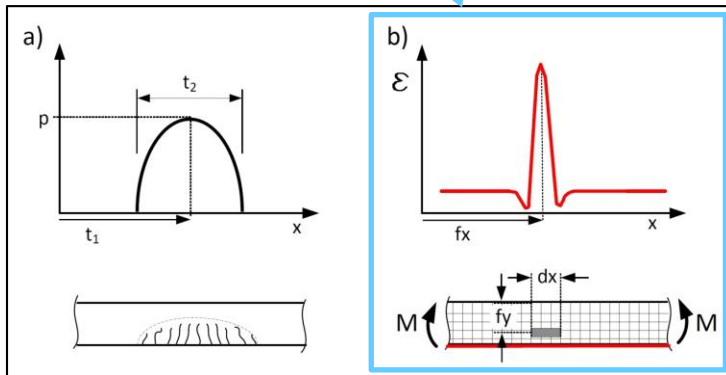
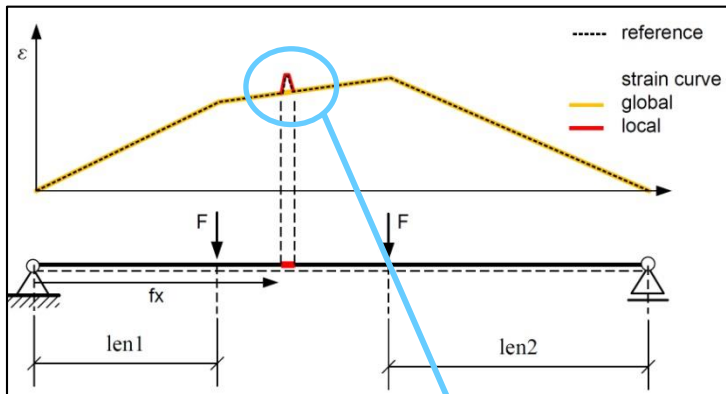


Classic parameter identification approach:

- Local properties (e.g. Young's modulus) variable in each element
- Very large space of unknowns: $n = m^k$
- Different kinds of value / resolution types for local and global parameters

5. Stepwise Parameter Identification Approach

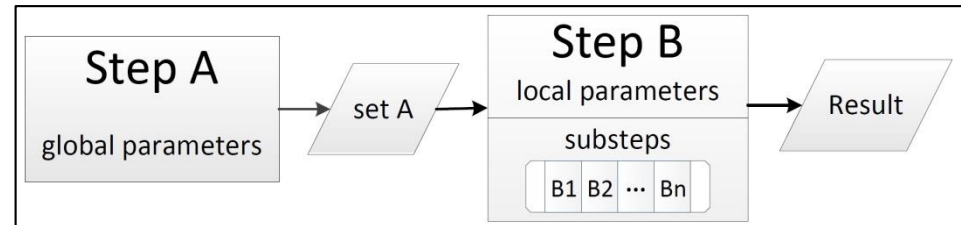
Quasi-continuous strain signal



Damage function
(analytical)

Shape function
(FE-Model)

Solution: Stepwise approach:



First step: Identification of global parameters

➡ Step A

Second step: Identification of local parameters

- Introduction of shape functions covering effect of local discontinuity (b)

- Basis: Damage functions for concrete (a) (Teughels and De Roeck 2005)

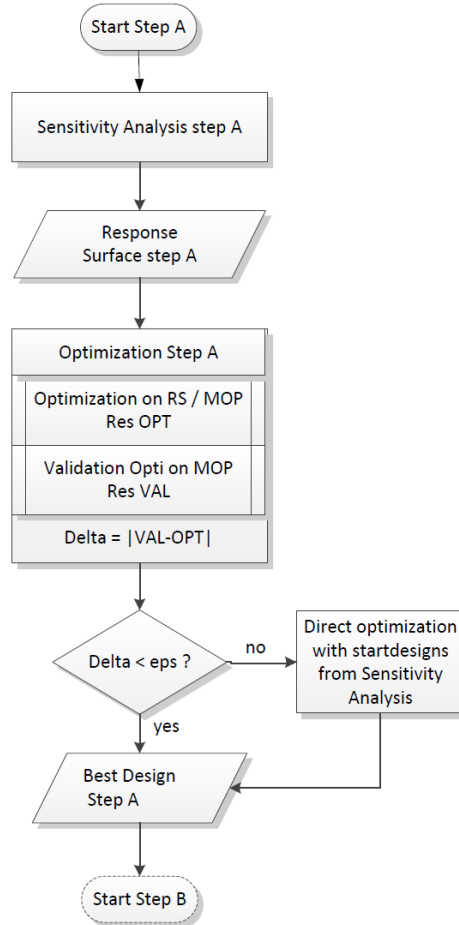
- Iterative identification of local discontinuities in substeps

➡ Step B

5. Stepwise Parameter Identification Approach

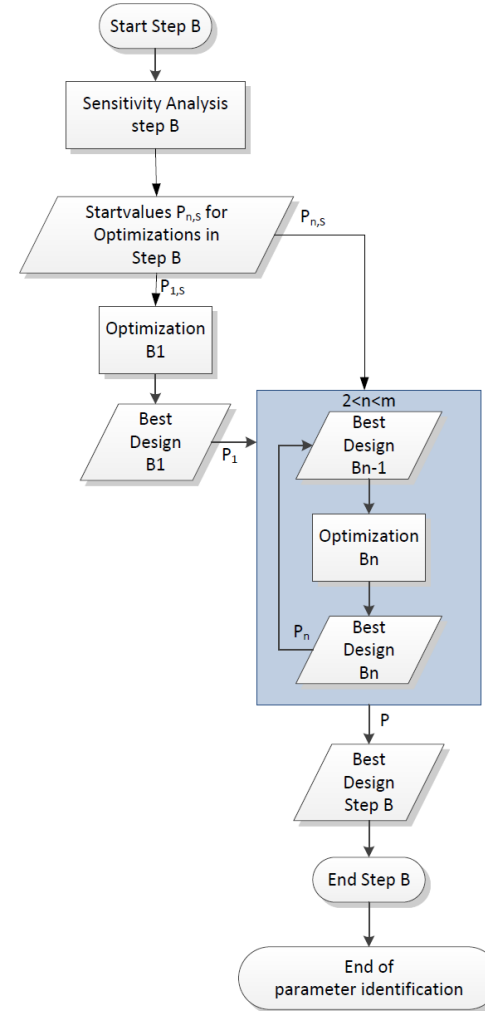
Identification of
global
parameters

Step A



Reference state
for Step B

Step B



Reference state
from Step A

Completely
identified
parameter set

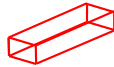
Simulation example

➤ Global portion of strain signal

- due to global parameters E , $len1$, n
- large influence on objective function
- obscuring local effects
- parameters of continuous distribution type

➤ Local portion of strain signal

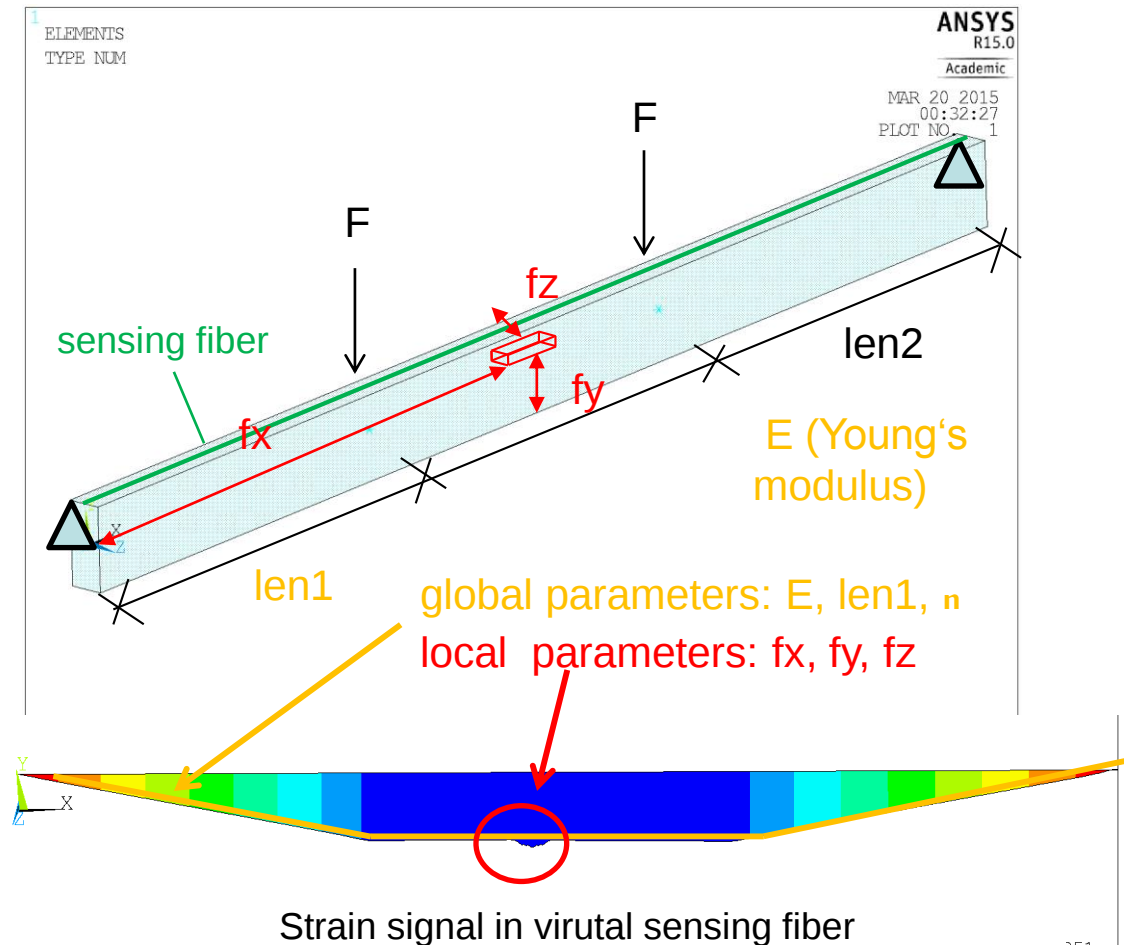
- due to local parameters fx , fy , fz of disturbance
- location assumed to be unknown
- parameters mesh-dependent and therefore of discrete type



➤ Separation of parameters

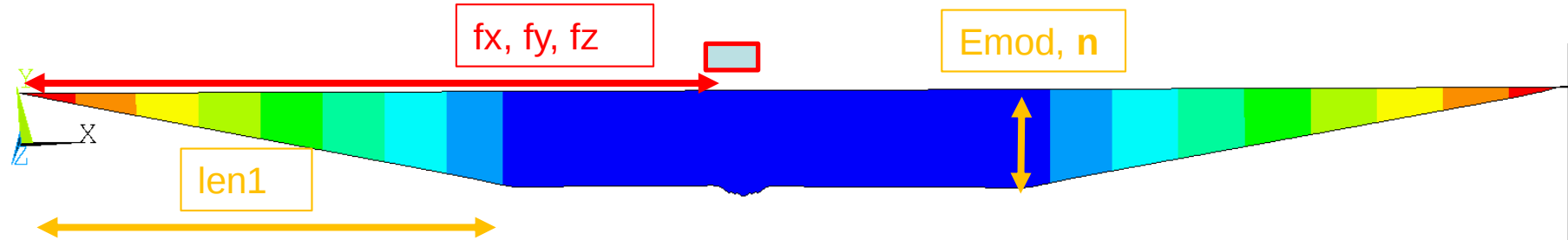
- E , $len1$, n - Step A
- fx , fy , fz – Step B

Beam in 4-point bending test (FE-Simulation)



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5. Stepwise Parameter Identification Approach



Definition of the model's parameters in OptiSlang

Parameter	Name	Parameter type	Reference value	Constant	Value type	Resolution	Range	Range plot
4	Emod	Optimization	2.1e+10	☐	REAL	Continuous	1.8e+10 2.2e+10	
5	fy1	Optimization	0	☒	REAL	Ordinal discrete by value	-0.04; -0.035; -0.03; -0.025; -0.02; -0.01; 0; 0.01; 0.02; 0.025; 0.03; 0.035; 0.04	
6	fy2	Optimization	0	☒	REAL	Ordinal discrete by value	-0.04; -0.035; -0.03; -0.025; -0.02; -0.01; 0; 0.01; 0.02; 0.025; 0.03; 0.035; 0.04	
7	fy3	Optimization	0	☒	REAL	Ordinal discrete by value	-0.04; -0.035; -0.03; -0.025; -0.02; -0.01; 0; 0.01; 0.02; 0.025; 0.03; 0.035; 0.04	
8	fz1	Optimization	0	☒	REAL	Ordinal discrete by value	-0.01; 0; 0.01	
9	fz2	Optimization	0	☒	REAL	Ordinal discrete by value	-0.02; -0.01; 0; 0.01; 0.02	
10	fz3	Optimization	0	☒	REAL	Ordinal discrete by value	-0.02; -0.01; 0; 0.01; 0.02	
11	len_1	Optimization	0.5	☐	REAL	Continuous	0.45 0.55	
12	len_3	Optimization	0.53	☒	REAL	Continuous	0.45 0.55	
13	Nue	Optimization	0.32	☐	REAL	Continuous	0.27 0.33	
14	nx1	Optimization	60	☒	INTEGER	Ordinal discrete by index	[0-140];	
15	nx2	Optimization	60	☒	INTEGER	Ordinal discrete by value	[0-140];	
16	nx3	Optimization	60	☒	INTEGER	Ordinal discrete by index	[0-140];	

☐ Prefer parameter from slot

global,
continuous

local,
discrete

(parameter set for 3 iterations in step B)

5. Stepwise Parameter Identification Approach

Objective function: Minimum of sum of least squares

```

23
24 ! ----- Parameter -----
25 breite = 0.04
26 hoehe = 0.1
27 laenge = 1.5
28 len_1 = 0.48
29 len_3 = 0.53
30 len_2 = laenge-len_1-len_3
31
32 ! ----- Vernetzung -----

```

Step A: Portion of strain signal with low influence of local effects preferred:

$$f_a = \min(S(\text{eps1}_i - \text{eps1}_{i_ref})^2 + S(\text{eps2}_i - \text{eps2}_{i_ref})^2)$$



Step B: Whole signal evaluated:

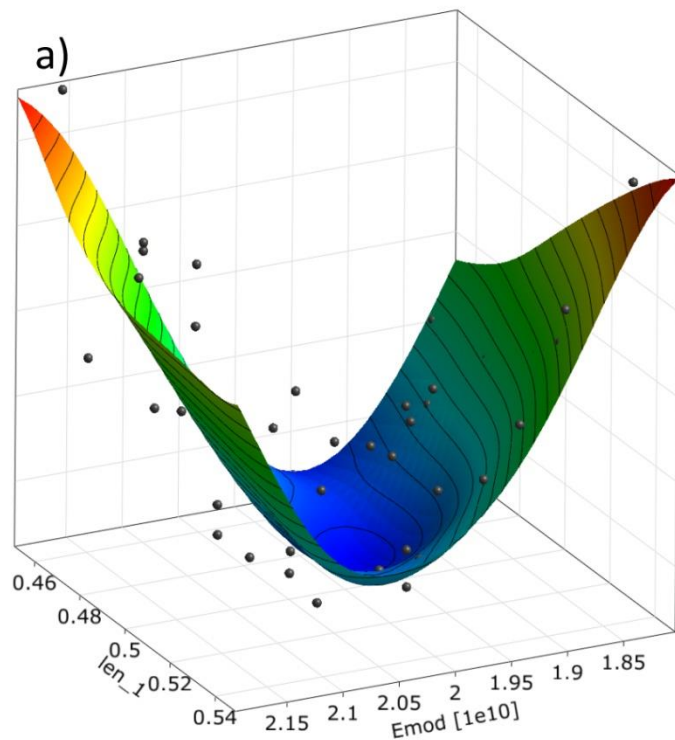
$$f_b = \min(S(\text{epsi} - \text{epsi}_{ref})^2)$$



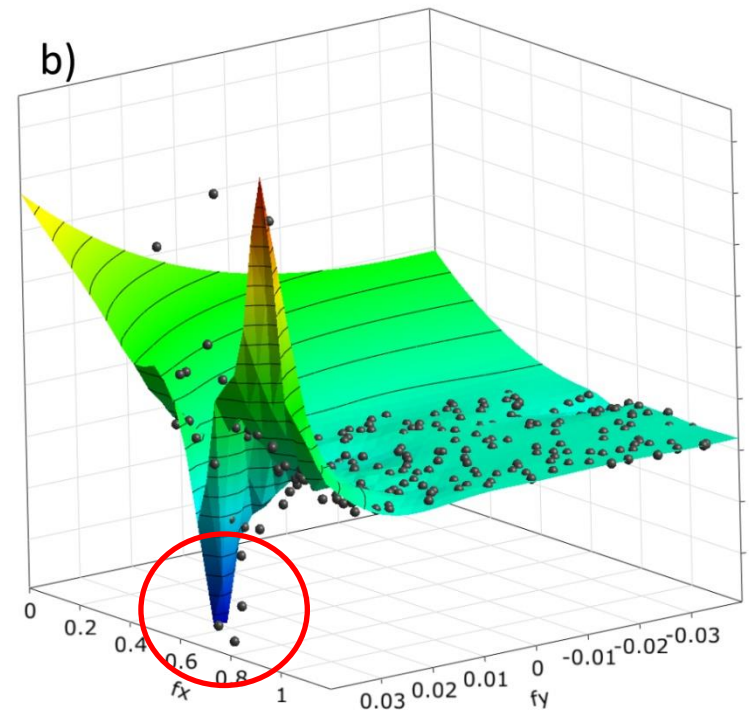
Visualization of optimization characteristic by MOP / RS

Evaluation of sensitivity analysis

Step A: Smooth and convex RS

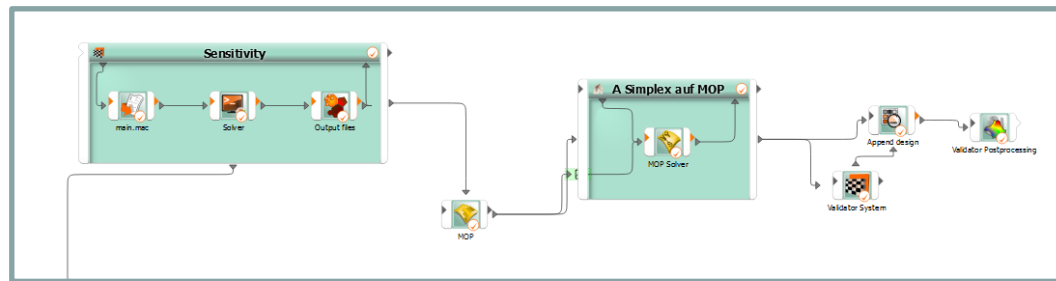


Step B: sharply bounded minimum



5. Stepwise Parameter Identification Approach

Implementation in OptiSlang

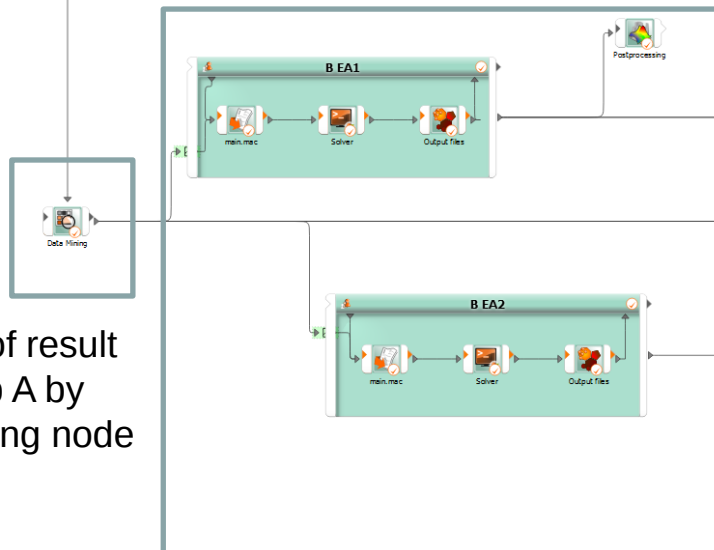


Step A:

Sensitivity analysis (SA)

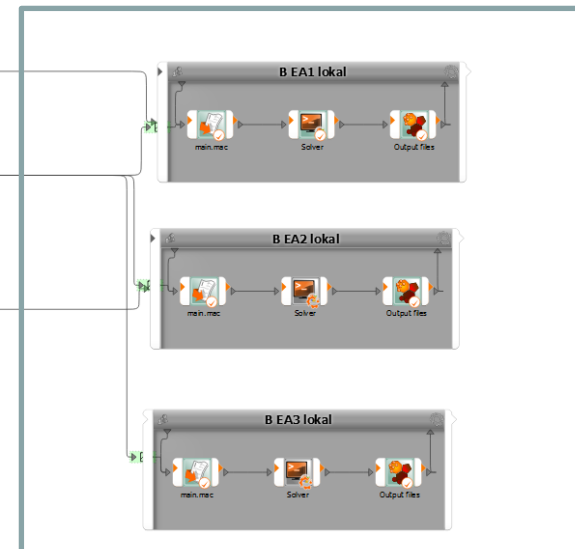
MOP generation

Optimization on MOP (Simplex)



Step B:

Optimization with EA



Step B:

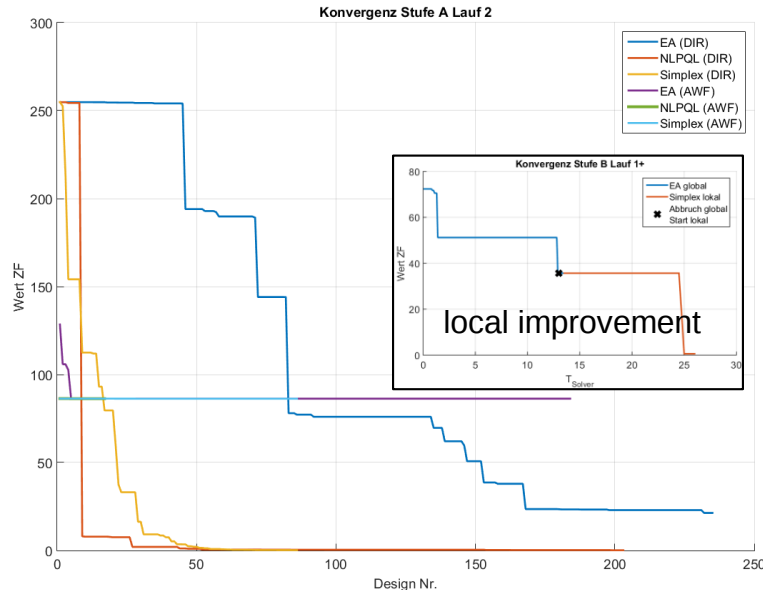
Local improvement with EA

Capture of result
from Step A by
Data Mining node

5. Stepwise Parameter Identification Approach

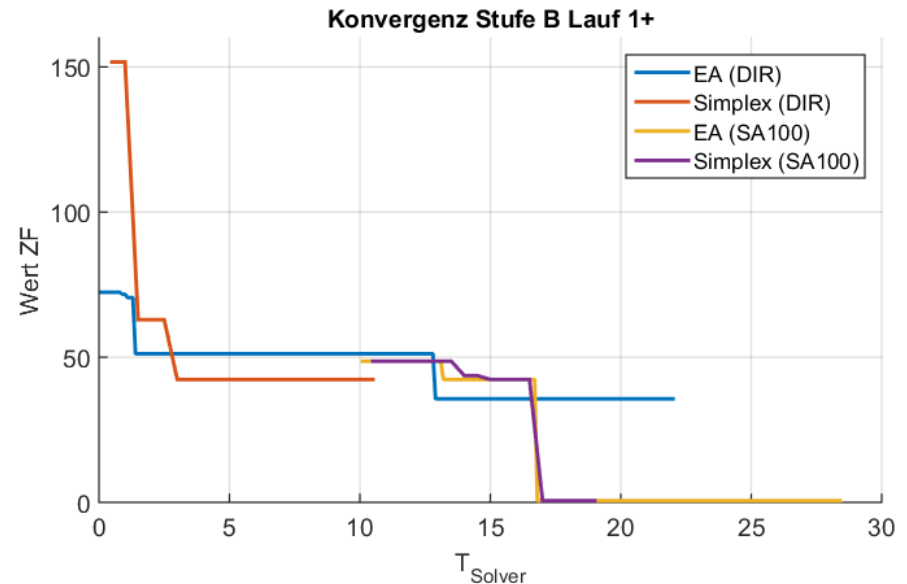
Performance

Step A



- Fastest convergence for NLPQL
- Simplex comparable to NLPQL
- EA needs many solver calls but allows for parallel solver runs
- Local improvement of EA result by Simplex is best solution

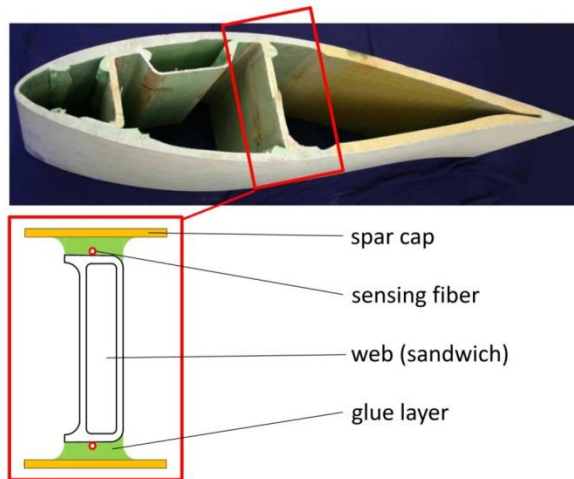
Step B



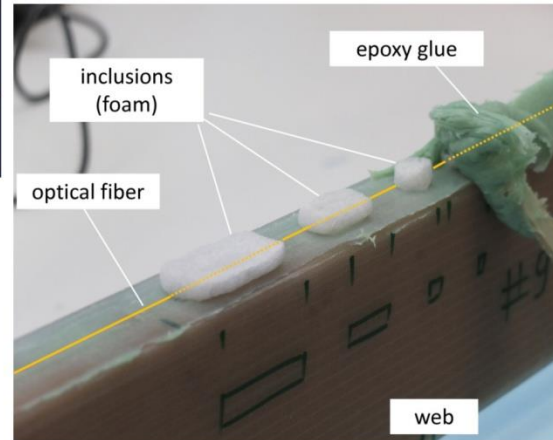
- Gradient-based algorithms not feasible due to discrete parameters
- Best results when combining start values from SA with local optimization settings
- All local parameters identified correctly by EA and Simplex with SA

6. Experimental Work

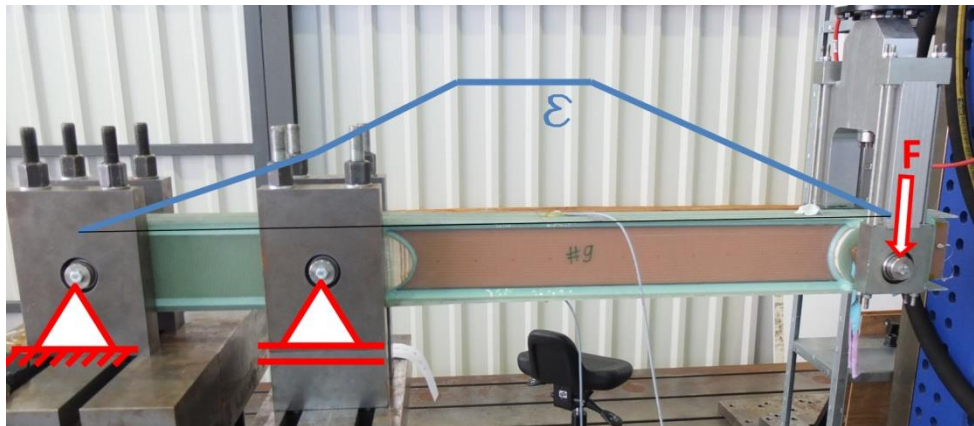
Sub-component of rotor blade structure in test setup „Henkel-UpWind-Beam“ (Fraunhofer IWES)



Definition of sub-component



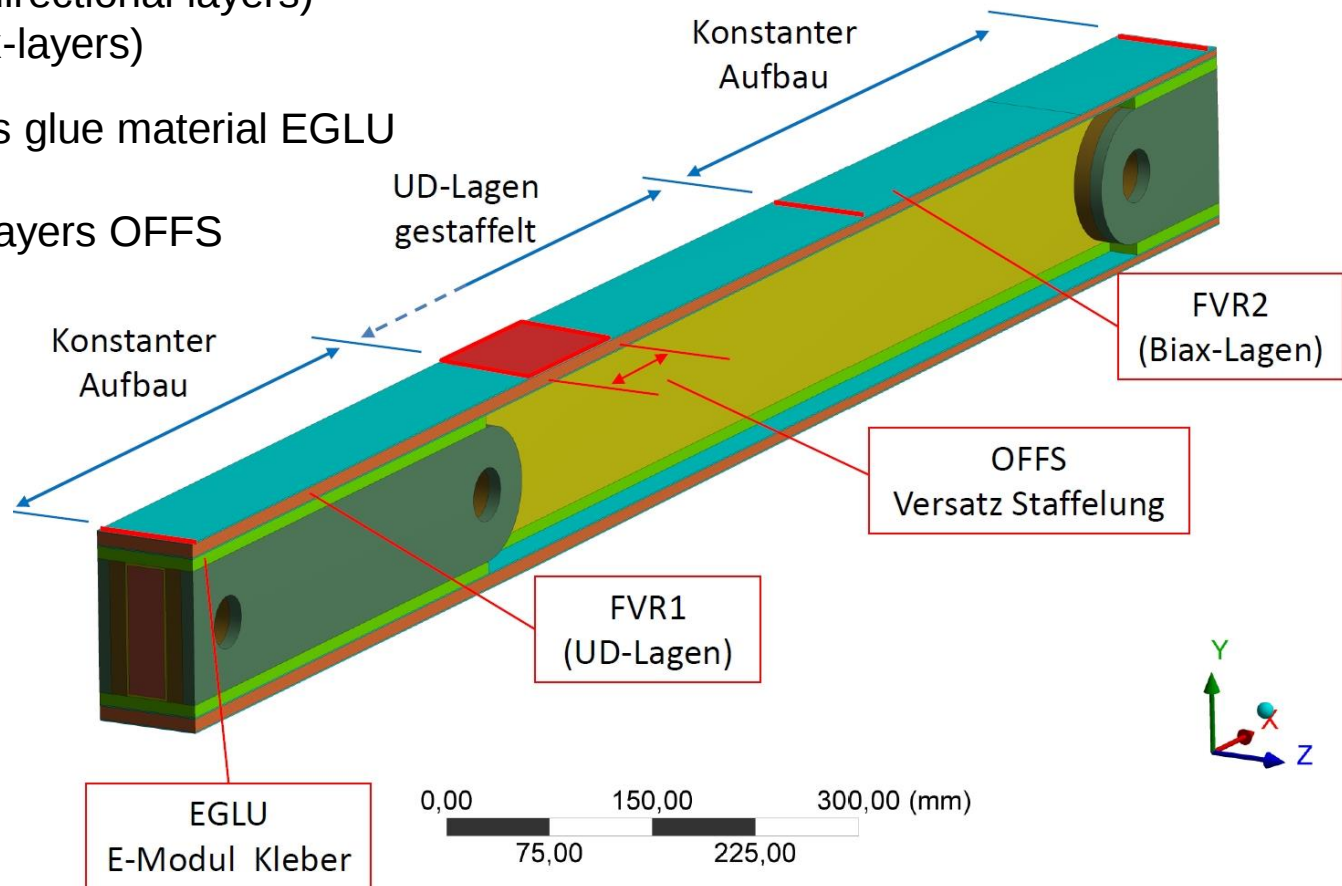
Sensing fiber and artificial defects in glue layer



Test setup: Support conditions, load and strain signal

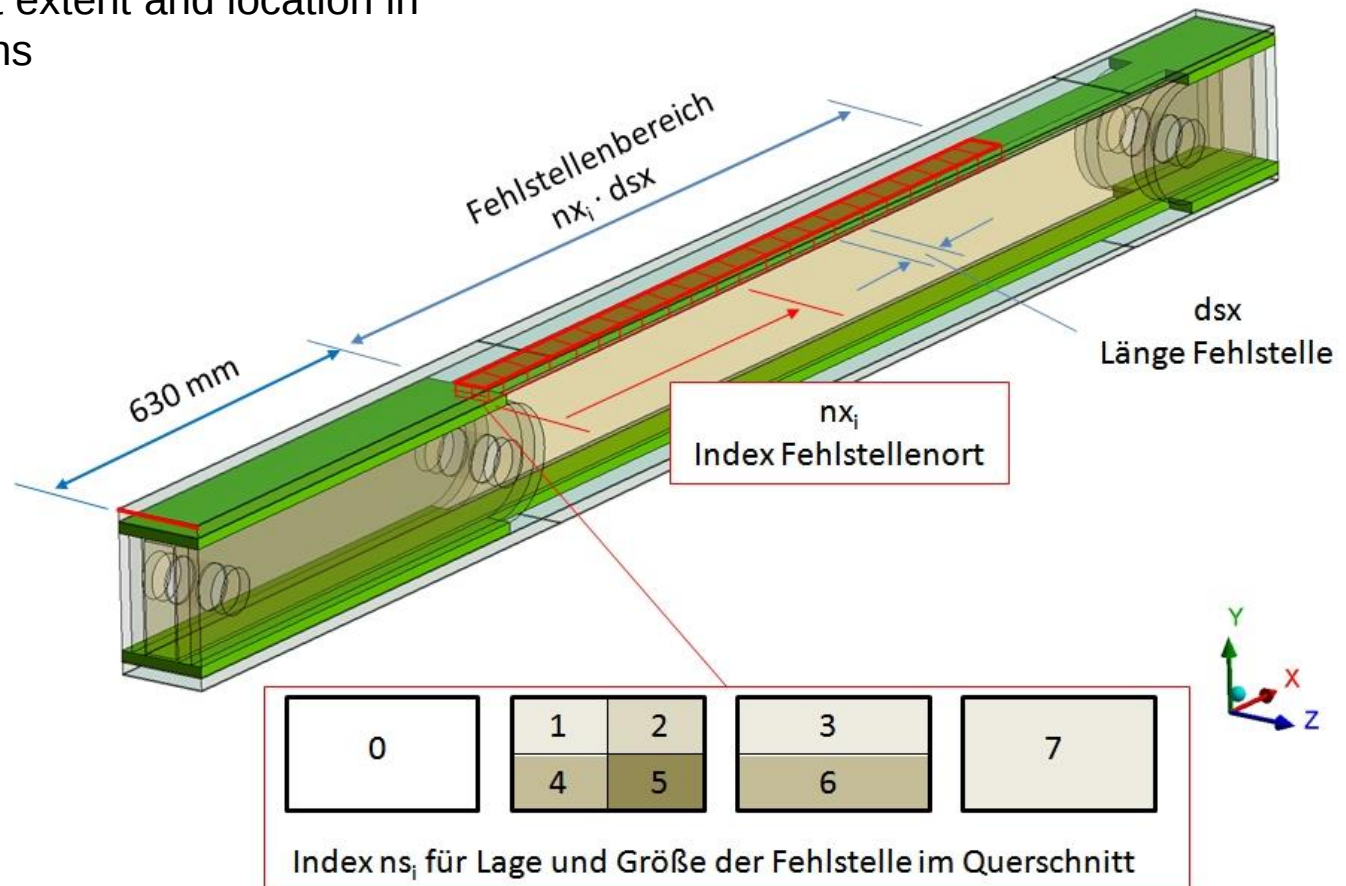
Definition of model parameters in step A:

- Stiffness determining parameters for GFRP-components
 - FVR1 (unidirectional layers)
 - FVR2 (biax-layers)
- Young's modulus glue material EGLU
- Offset spar cap layers OFFS



Definition of model parameters in step B:

- Location of local defect nx
- Index of defect extent and location in cross section - ns



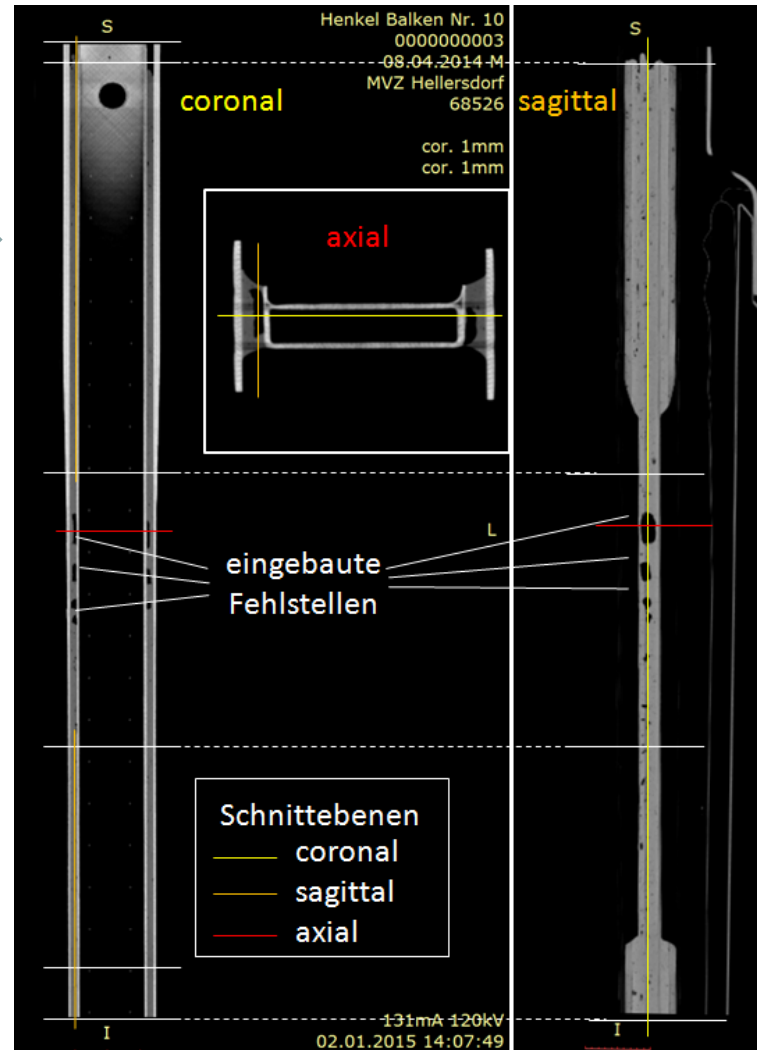
6. Experimental Work



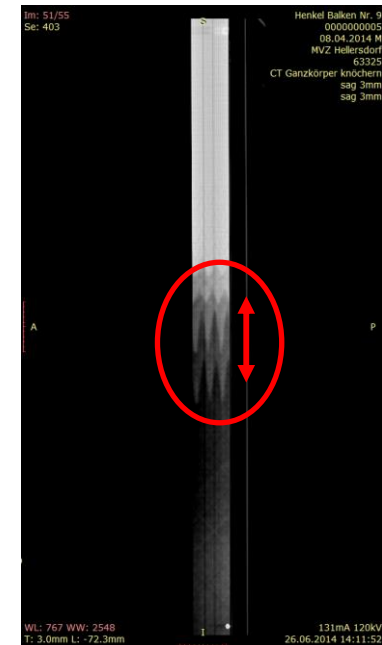
CT-scans are used to evaluate parameter identification results

Artificial defects as well as unintended voids are visible in CT-scan

Local imperfections



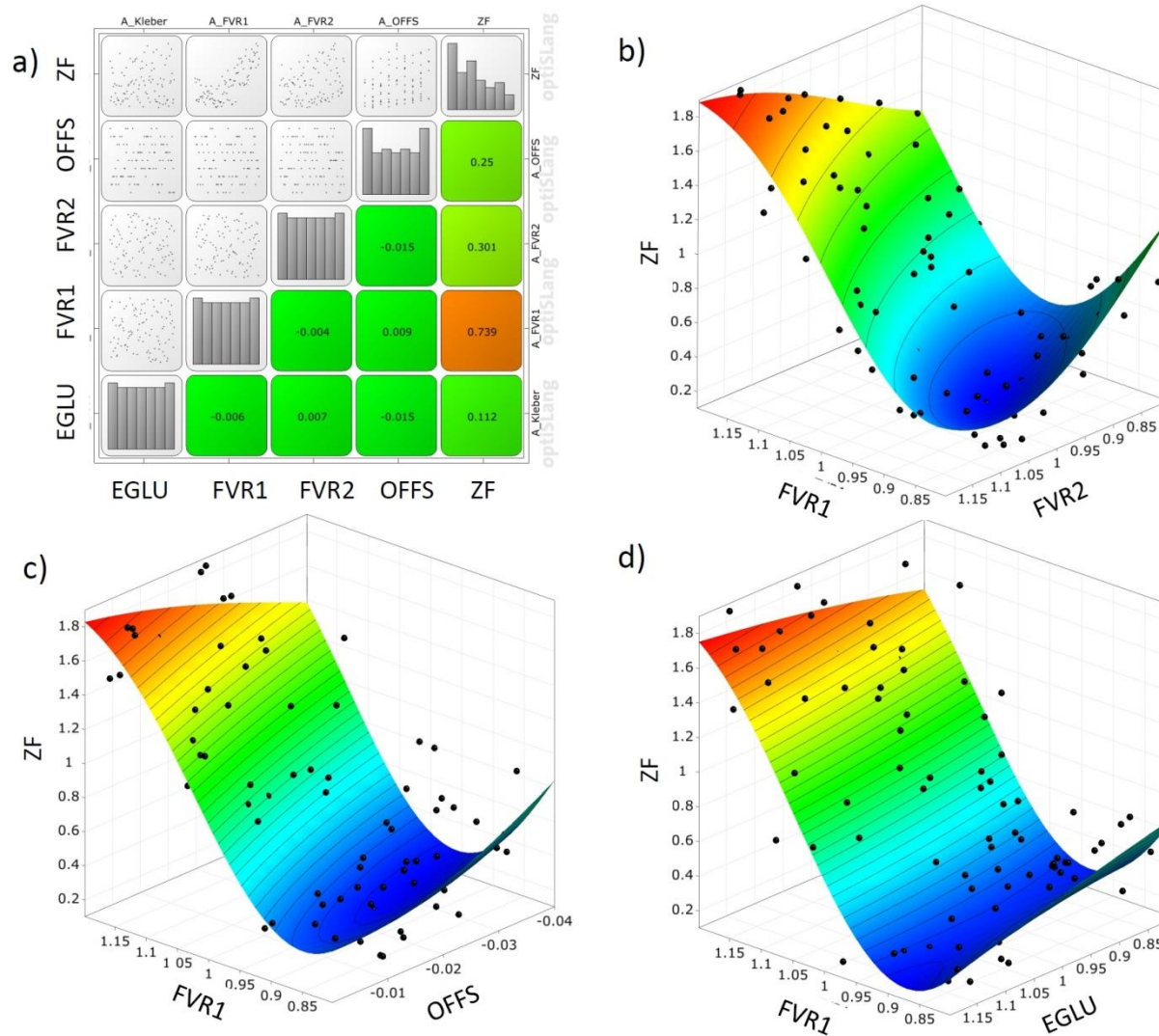
global imperfections



Tapered GFRP-layers in spar caps

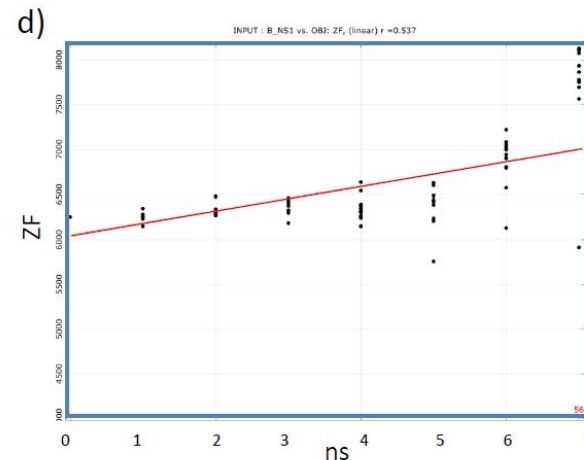
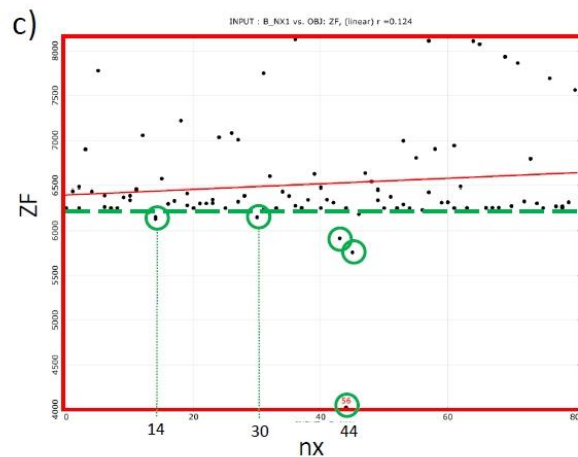
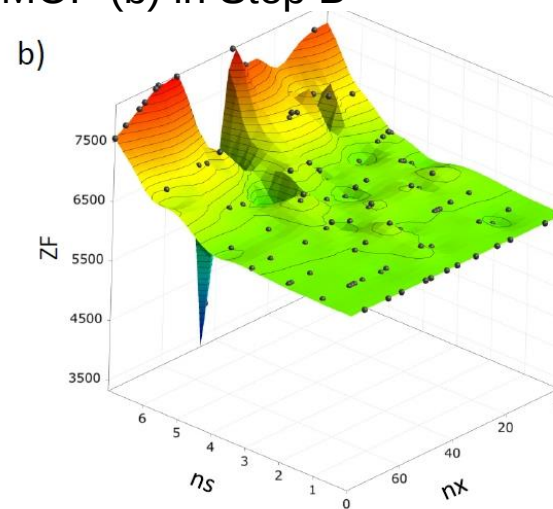
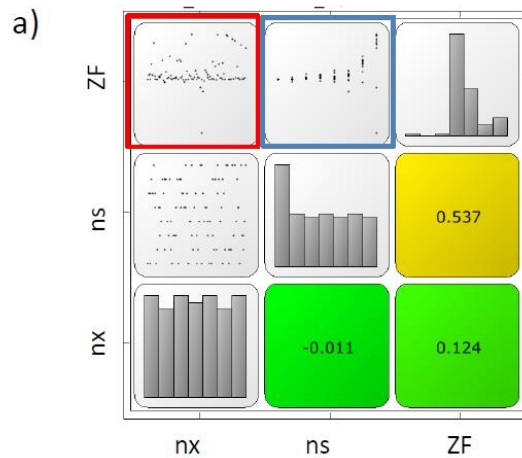
6. Experimental Work

Correlation matrix and MOP in Step A



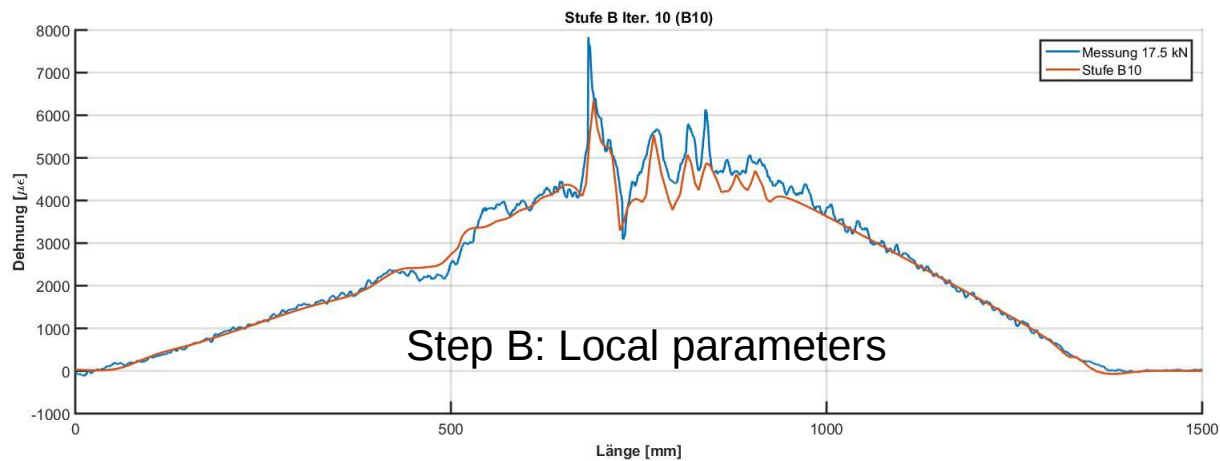
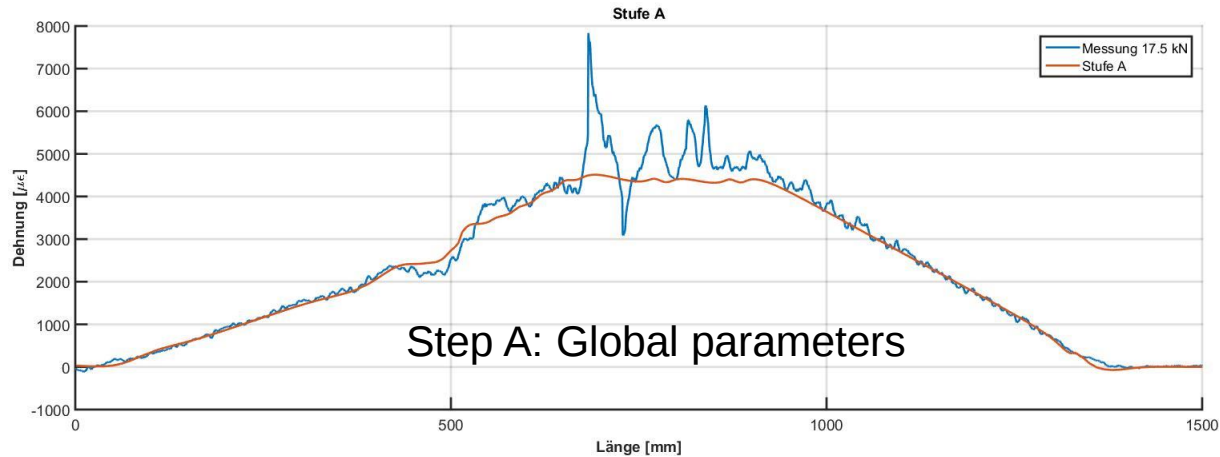
6. Experimental Work

Correlation matrix (a) and MOP (b) in Step B



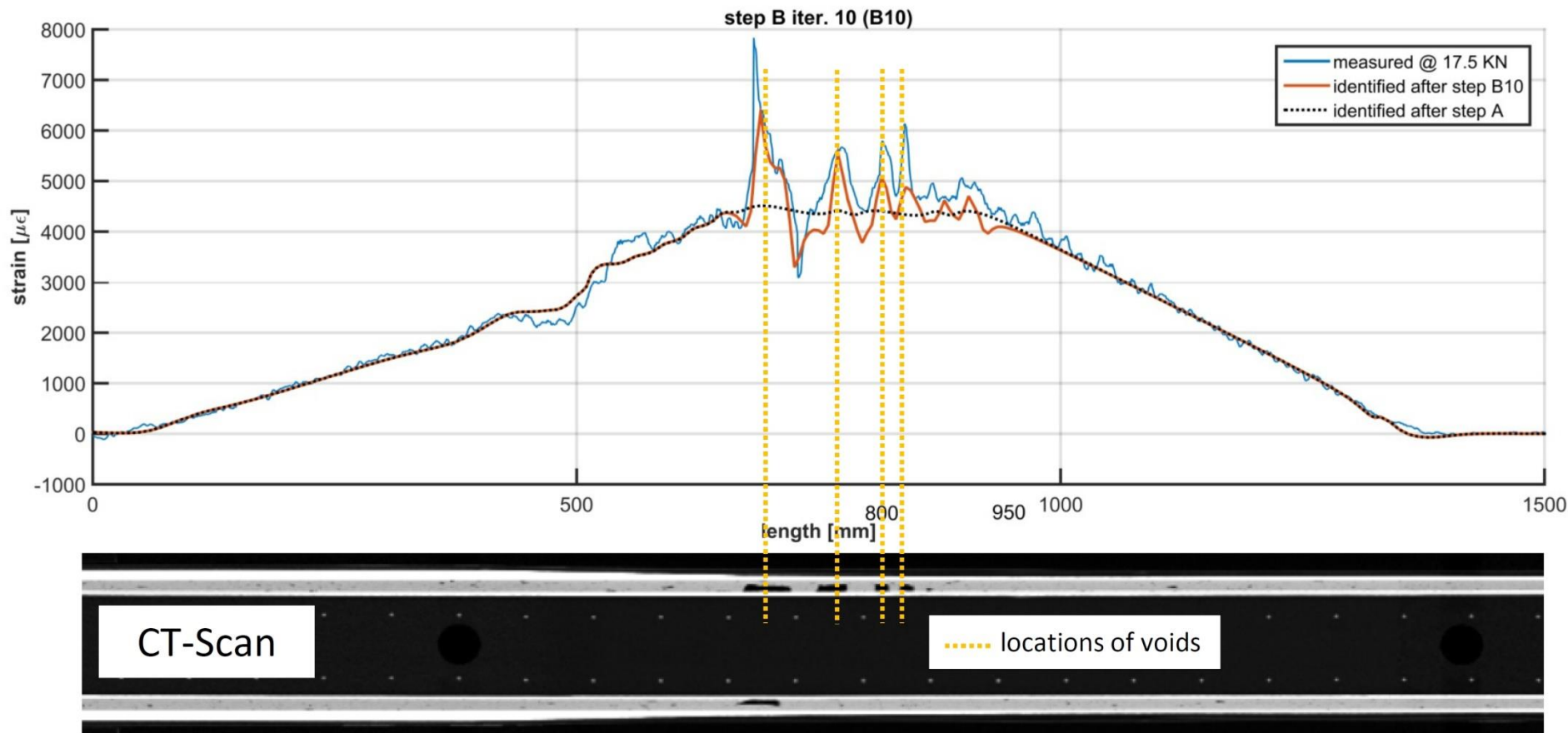
Anthill plot for x-.location nx (c) and defect index ns (d)

Results



Results

Comparison of identified voids with CT-scan

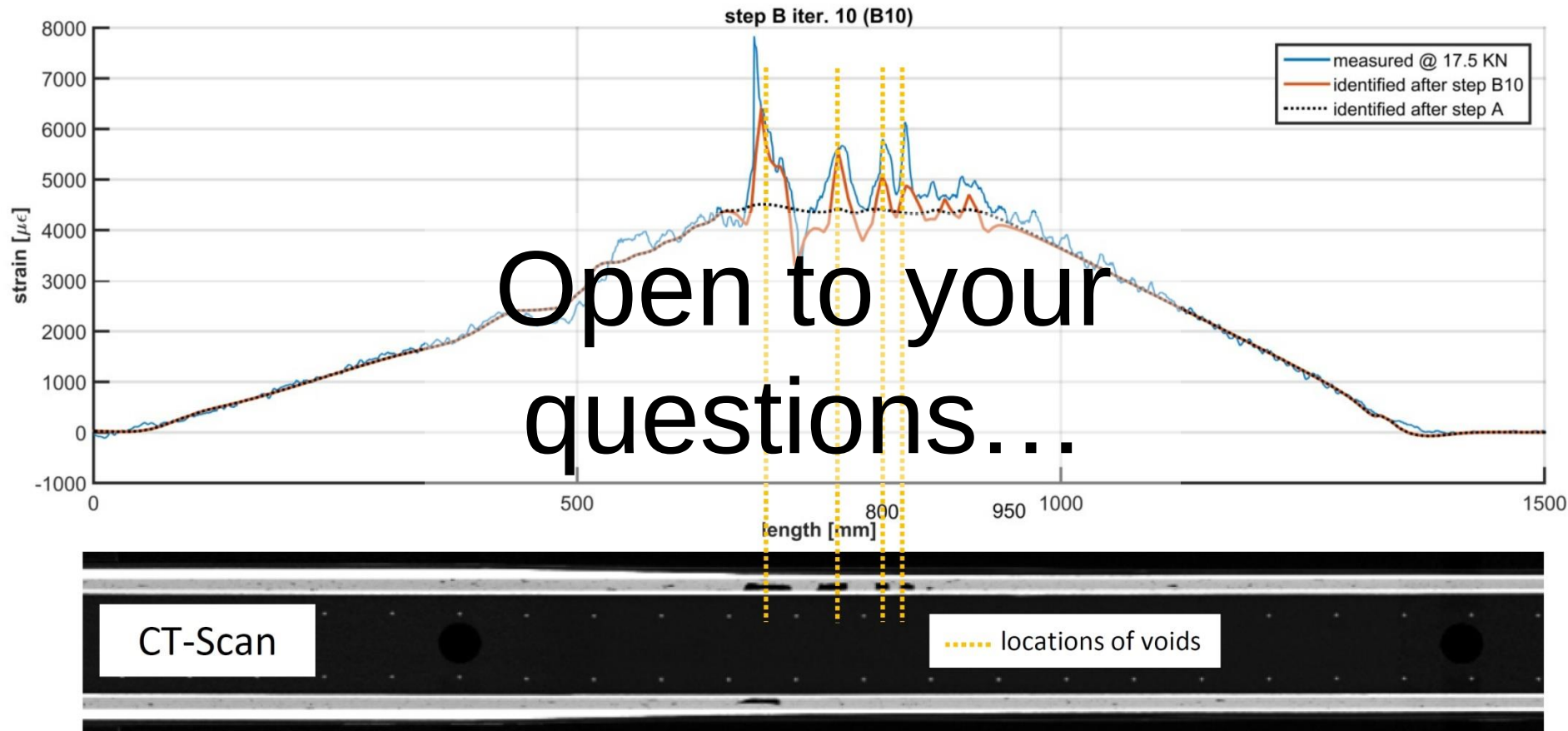


Summary:

- Stepwise parameter identification approach for strategic evaluation of quasi-continuous strain data
- Signal capturing by high-resolution fiber optic sensing system
- Determination of global and local parameters
- Efficient optimization task due to grouping of parameters by physical meaning and distribution type
- Successfull application to „real-world“ experimental setup

Outlook:

- Enhancement of efficiency (optimization algorithms, settings)
- Application / extension to dynamic sytems
- Software integration



Special thanks to: Fraunhofer IWES, Fa. Polytec, MVZ Hellersdorf