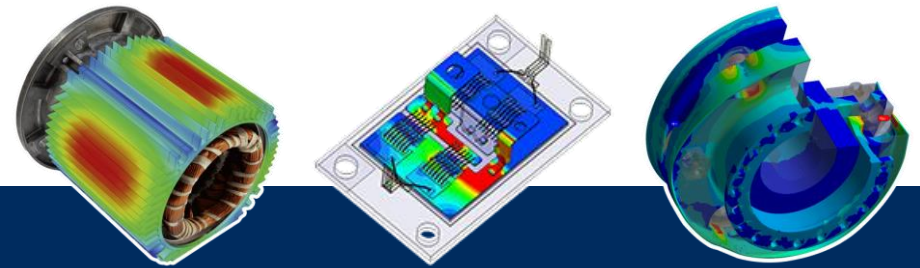


CADFEM[®]



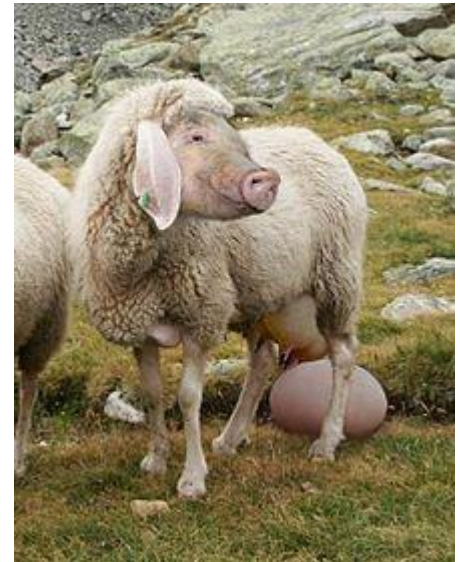
Simulation ist mehr als Software[®]



Automatized optimization of a machine tool cascade controller based on system simulation

Motivation

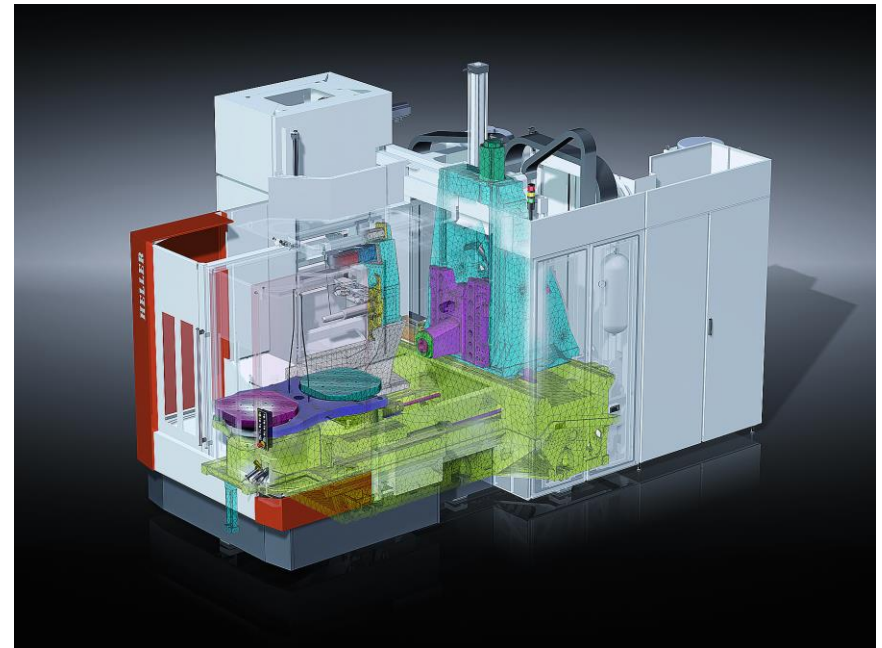
- machine tools:
 - highly complex electrified system (mechanics, electrical machines, sensors, control, influences from the environment,...)
 - interaction of several components across physical domains with controller
- tasks for the manufacturer
 - high cutting speed (HPC) $\rightarrow$ dynamics $\uparrow \rightarrow$ mass $\downarrow$
 - surface quality $\rightarrow$ stiffness $\uparrow \rightarrow$ mass $\uparrow$
 - robust processes/ high life times
 - reduce costs $\rightarrow$ competing goals



Source: Wikipedia

How to reach these targets?

- try-and-error
 - expensive (physical prototypes)
 - time consuming
- optimization based on numerical models
- Challenge: model the whole systems behavior → system simulation



Source: Gebr. Heller Maschinenfabrik GmbH

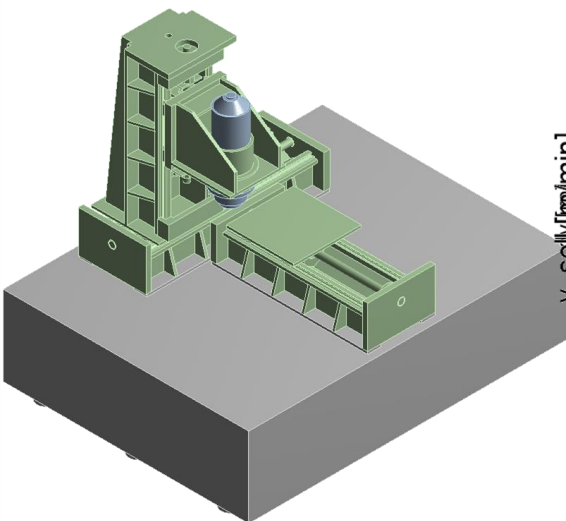
Some general thoughts on system simulation and abstraction

choice of the correct level of abstraction:

- What should be simulated?
- Which time constants for which effects?
- Are the time constants in the same range?
- Which effect has to be taken into account, what can be neglected?

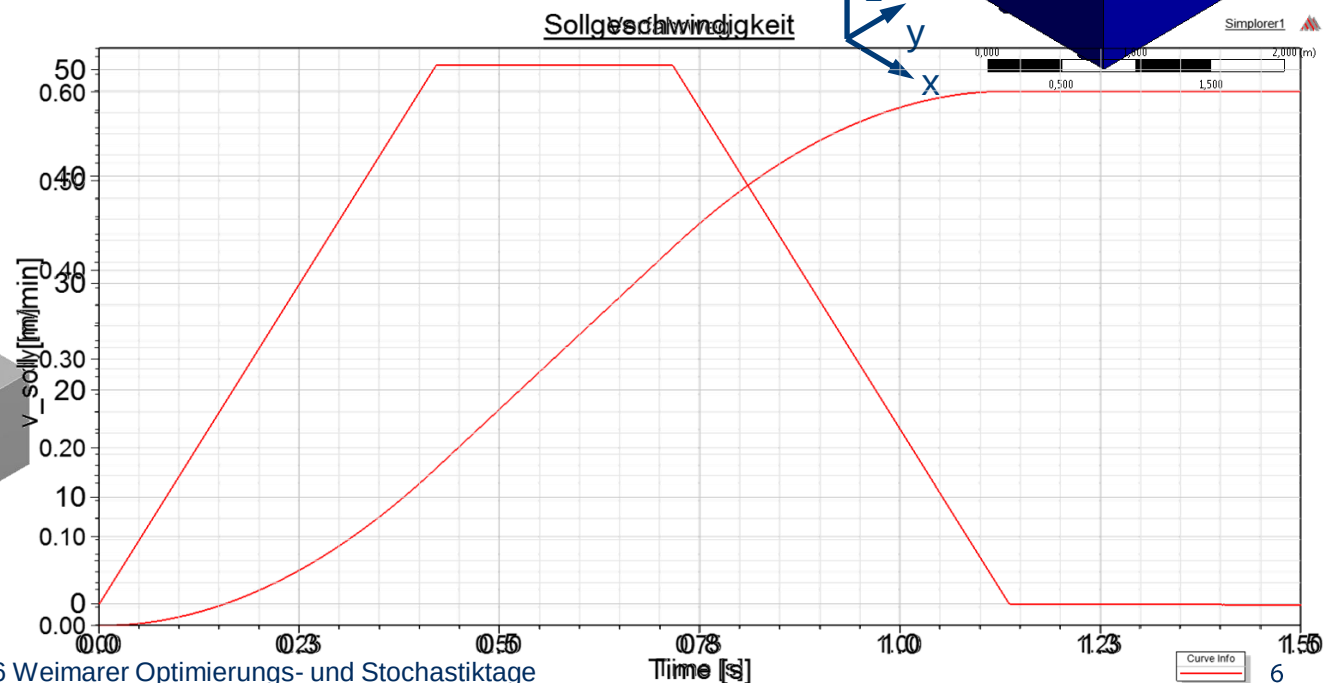
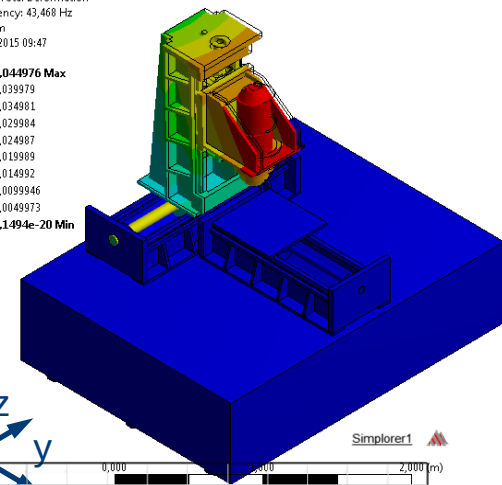
Scenario: rapid traverse from tool changer to workpiece

- fast traverse of the machine tool column from tool changer to WP → tool is not cutting
- travel distance 60cm in ~ 1.1s,
 $v_{\max} \sim 50\text{m/min}$
- Oscillation peak to peak at TCP after 1.5s < $2\mu\text{m}$



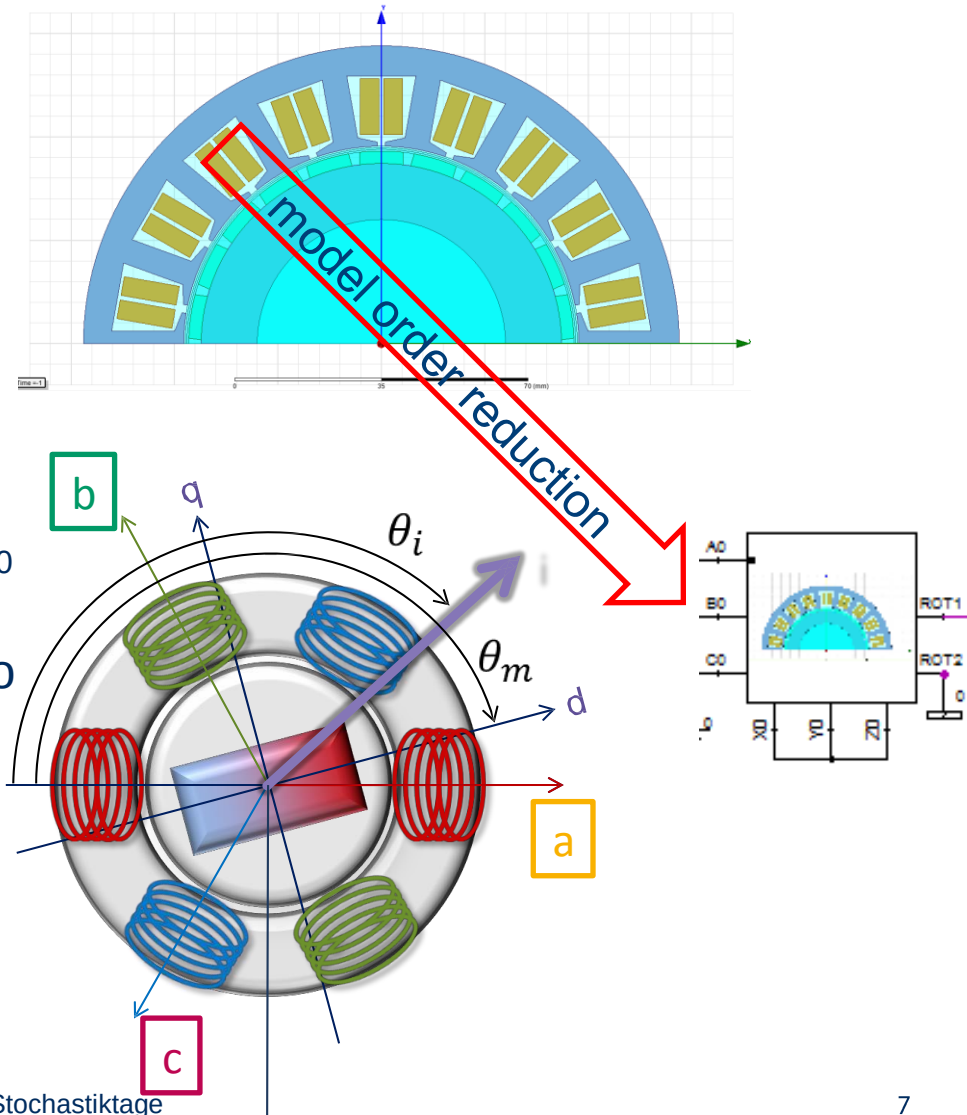
B: Bushings
Total Deformation 4
Type: Total Deformation
Frequency: 43,468 Hz
Unit: m
11.05.2015 09:47

0,044976 Max
0,039979
0,034981
0,029984
0,024987
0,019989
0,014992
0,0099946
0,0049973
1,1494e-20 Min

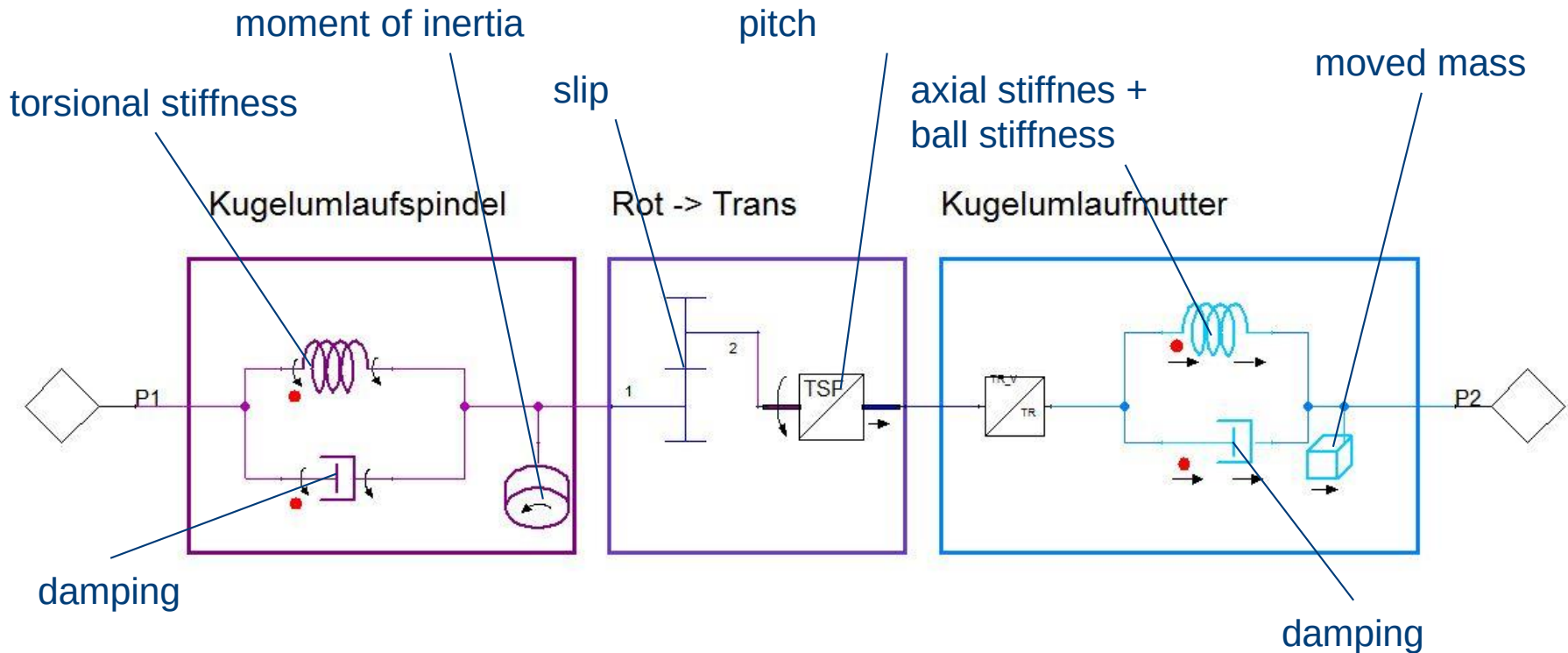


components: axis drive

- PMSM
- 11 pole pairs
- model order reduction: ECE-model (equiv. circuit extraction)
- variation of currents I_d , I_q and rotational angle θ_m
- lookup-table: flux linkage Ψ_d , Ψ_q , Ψ_0 + torque
- takes into account: saturation due to material nonlinearities
- does not take into account: eddy current effects



components: ball screw drive



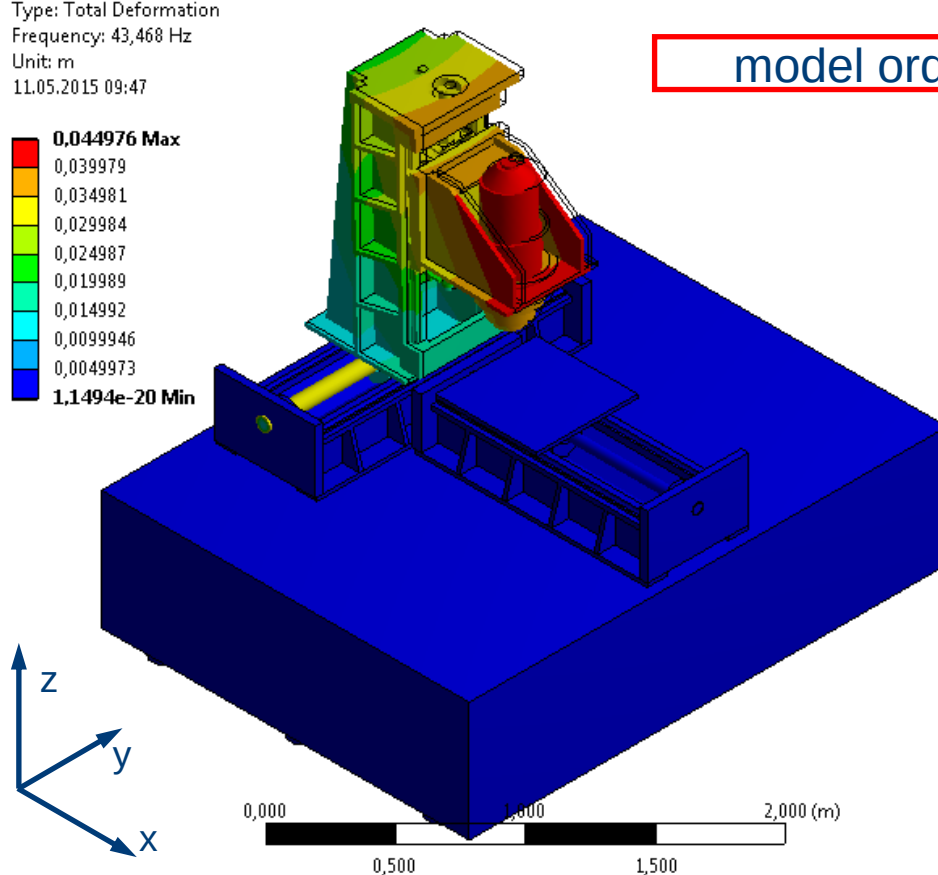
- nonlinear stiffness: function of position
- nonlinear behavior (clearance, etc.): nonlinear contacts

components: moved machine tool column

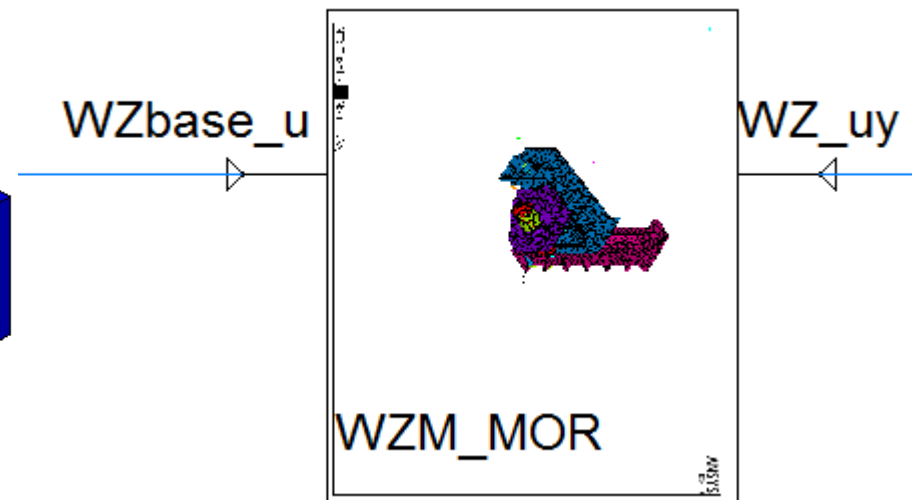
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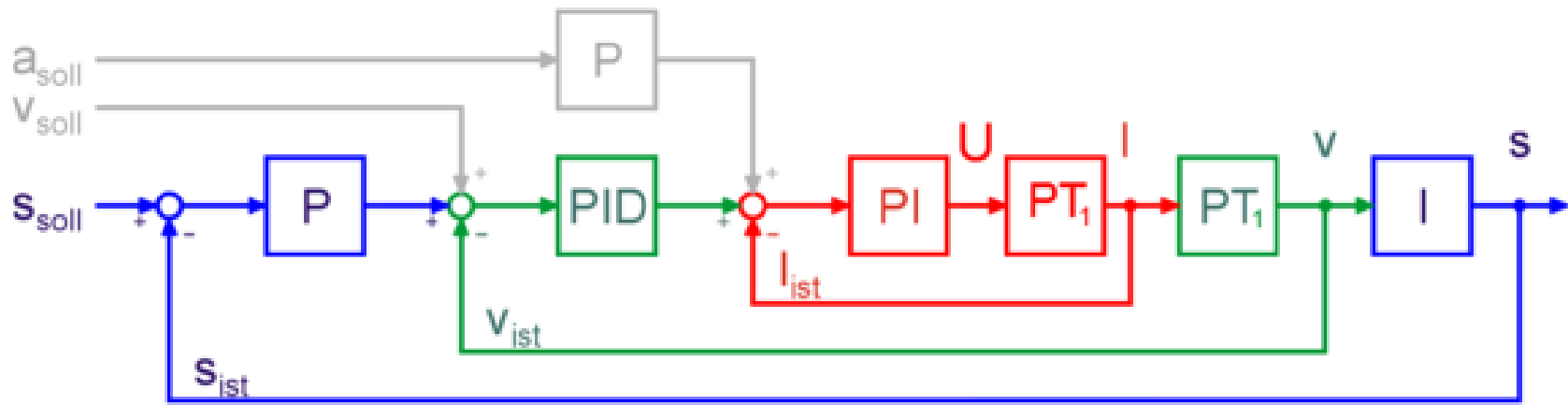
model order reduction



components: control

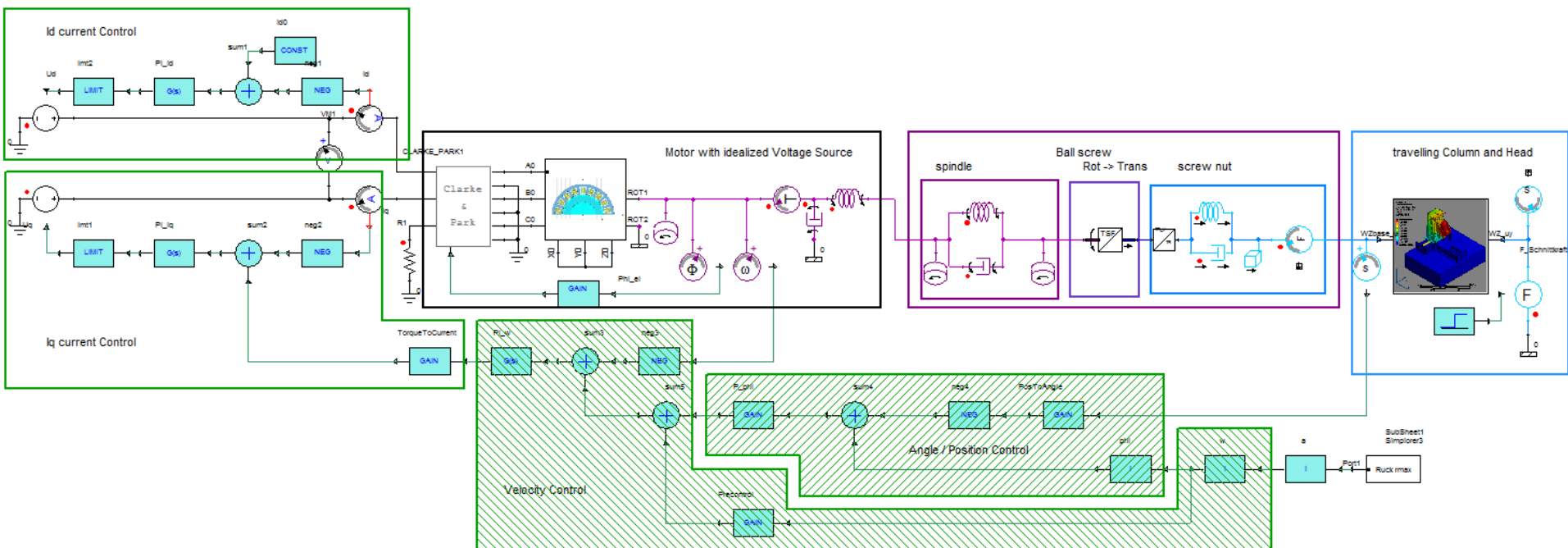
basic concept: cascade control

- control of processes with time constants of different orders of magnitude
- basic control concepts (P, PI, PID)
- stepwise activation
- can be extended to more advanced control algorithms



Source: www.Wikipedia.de

system model of machine tool in SIMPLORER

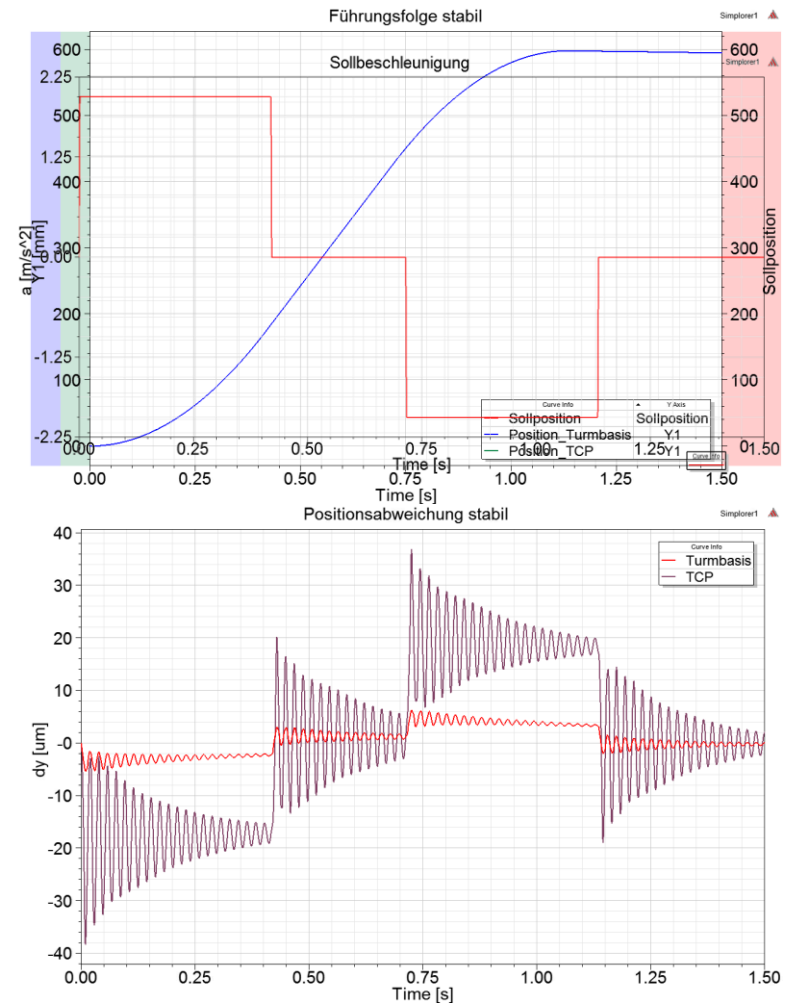


application example: control optimization

- state of the art:
 - in frequency domain
 - sequential closing / optimization of the cascades
- advantages:
 - Easily feasible
 - well-proven
- disadvantages:
 - no consideration of nonlinearities
 - manual tuning necessary
- alternative:
 - in time domain
 - based on systems simulation
 - parallel optimization of cascades
- advantages:
 - consideration of nonlinearities
 - automated optimization of control parameters
 - starting values from rules of thumb

Educated guess: find control parameters

- Based on analytical approaches and some manual tuning for stabilization
- position of TCP and column base follow the set-point in desired manner
- Persistent control deviation for accelerated movement
- Oscillation with peak-to-peak amplitude at TCP $\sim 4.5 \mu\text{m}$ after 1.5 s
- Goal: Amplitude p2p $< 2 \mu\text{m}$



Optimization in time domain

- Basic requirements:
- Control must behave stable
- Control value should follow setpoint value the fastest possible way
- Maximum overshoot ~40%

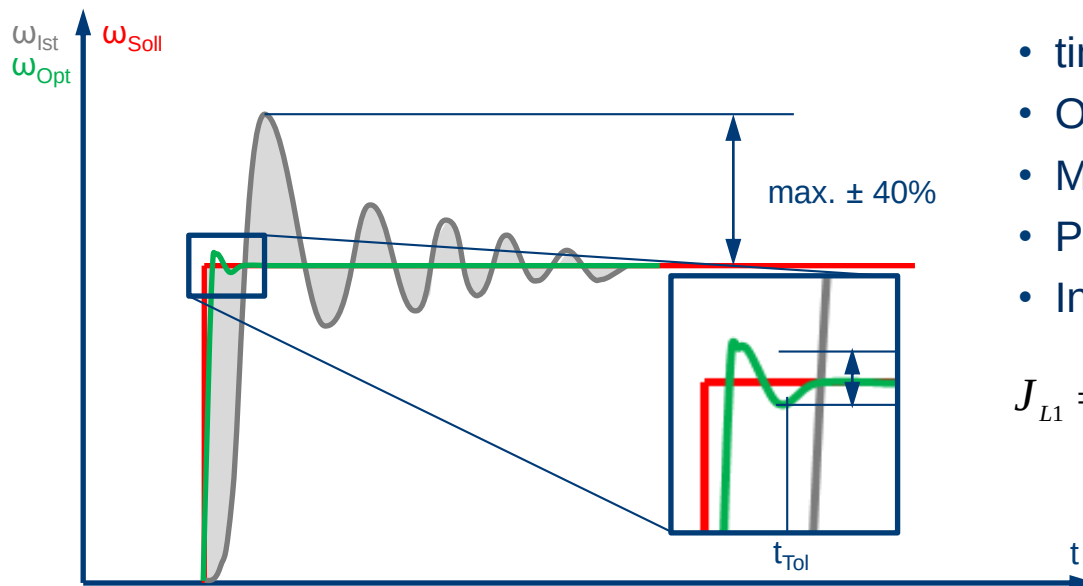
- Optimization goals:
 - Minimal control deviation
 - Fast settlement to final value
 - Few oscillation at end of observed time

→ transfer to characteristic values:

- time t_{Tol} to settle in tolerance band
- Oscillation amplitude at t_{End}
- Maximum control deviation e_{max}
- Persistent control deviation e_{end}
- Integral quality factors:

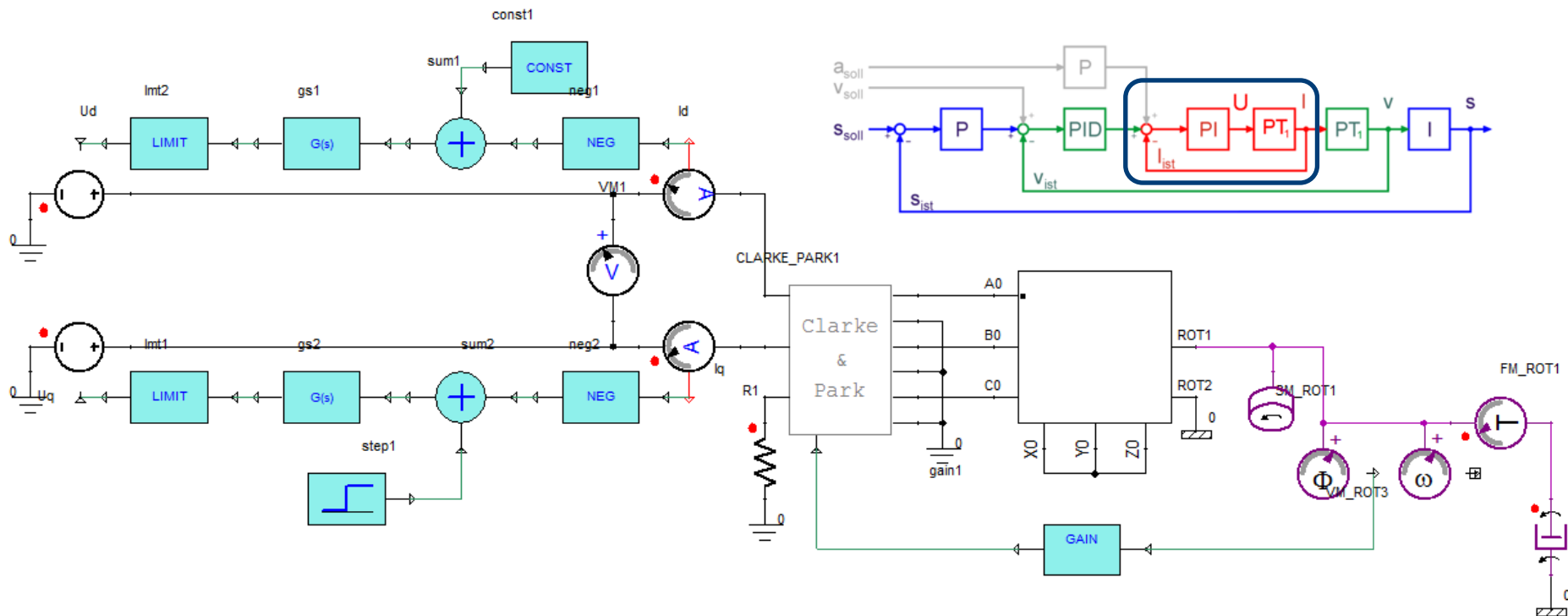
$$J_{L1} = \int_0^{t_{end}} |e(t)| dt \rightarrow \min \quad J_{L2} = \int_0^{t_{end}} e(t)^2 dt \rightarrow \min$$

$$J_{ITAE} = \int_0^{t_{end}} |e(t)| \cdot t dt \rightarrow \min$$

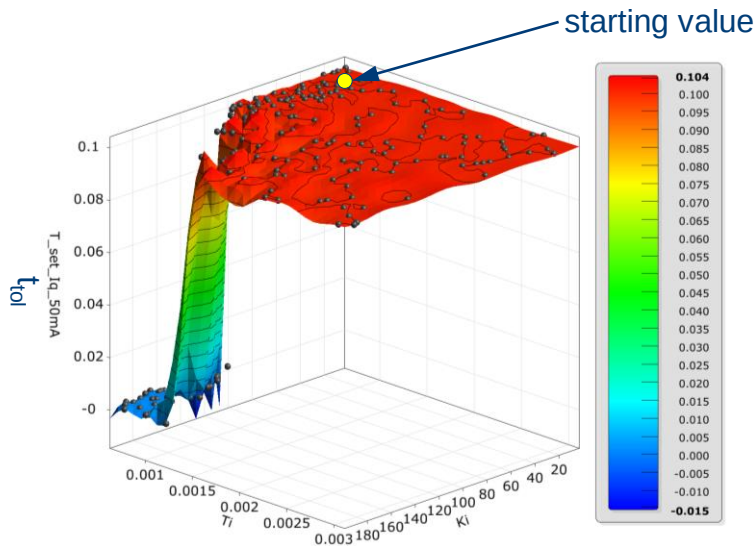


1: Current controller– pre-selection of fast designs

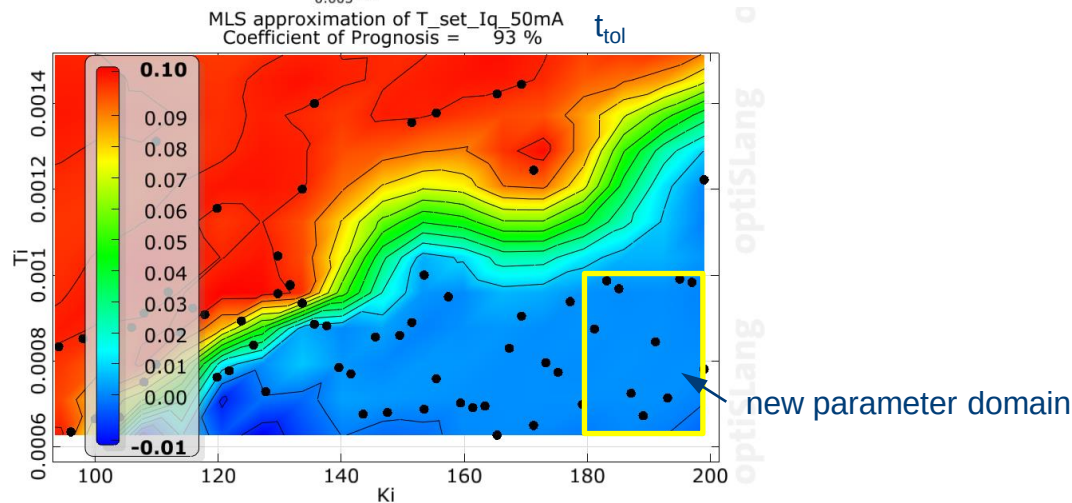
- Take a look at the motor
- DOE: Control parameters gain and integration time constant
- Starting point: parameters derived from analytical solution
- Output parameters: t_{tol}



1: Current controller– pre-selection of fast designs

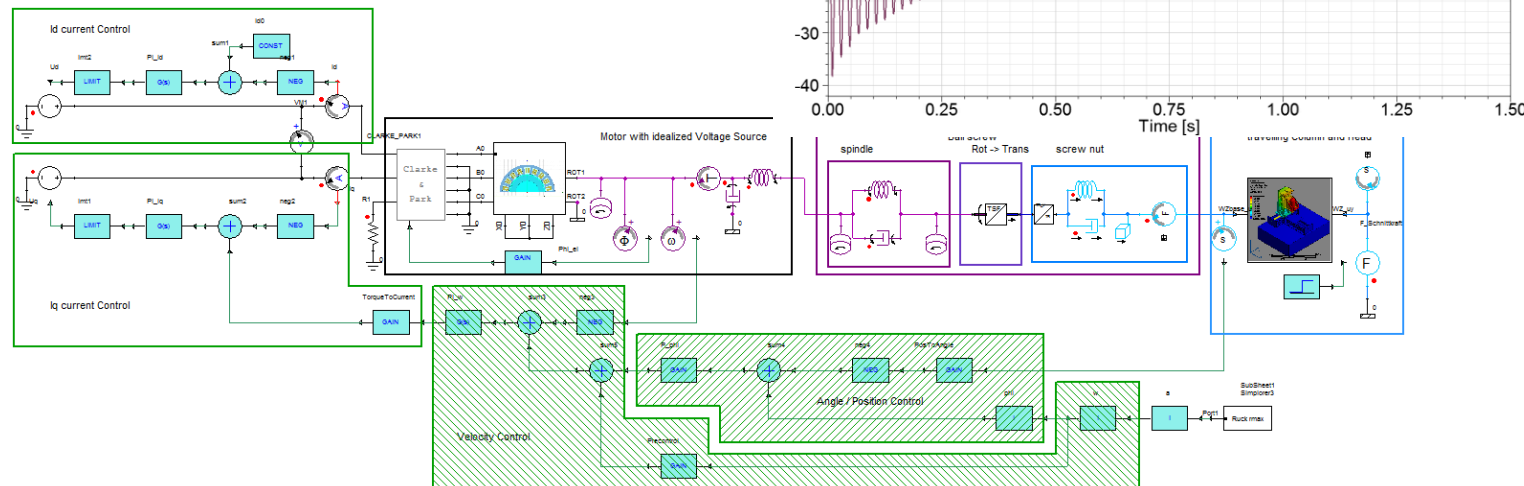


- steep gradient
 - separation between fast and accurate and slow and or inaccurate designs
- reduction of parameter range

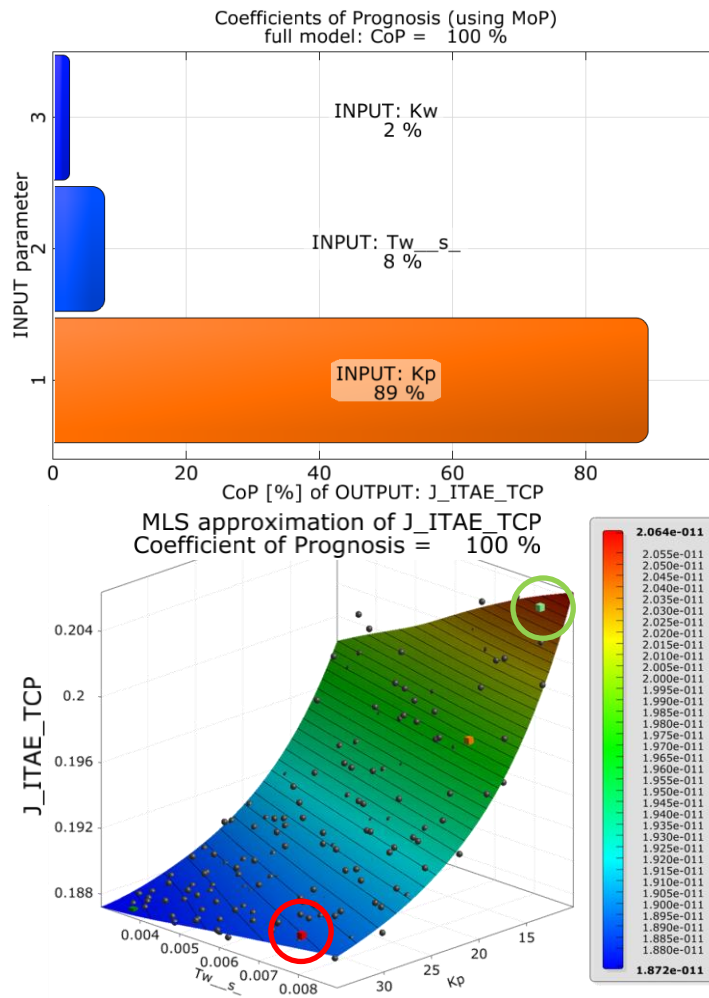


2: Control of the entire system

- DOE: control parameters for all 3 cascades:
 - PI current control: reduced parameter domain from 1. iteration
 - PI velocity control: from analytical solution
 - P position control: from analytical solution
- Results:
 - Integral quality factor ITAE
 - Amplitude of oscillations
 - At column basis
 - At TCP



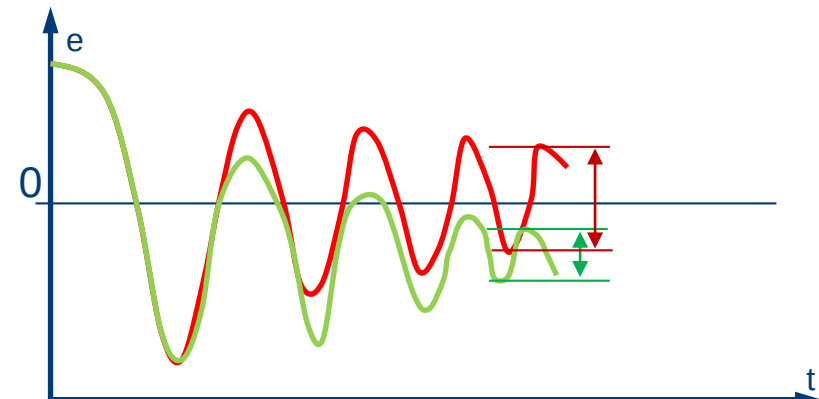
Integral quality factor ITAE



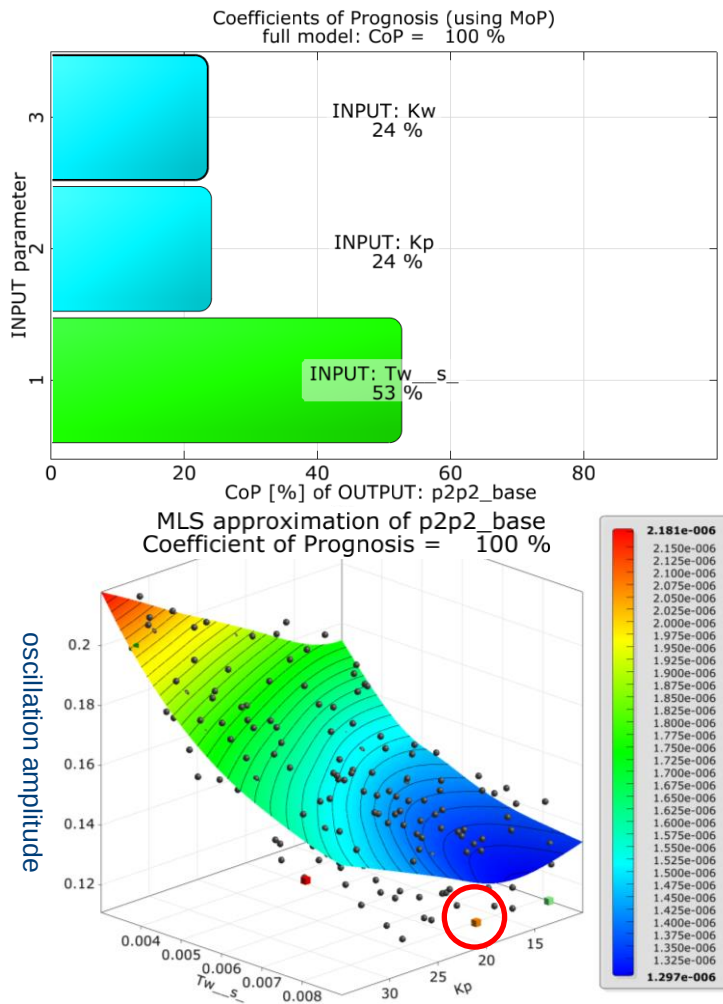
$$J_{ITAE} = \int_0^{t_{end}} |e(t)| \cdot t dt \rightarrow \min$$

- Dominated by position controller gain
- Steady state control deviation penalized stronger than oscillation
- Difference between min and max value small

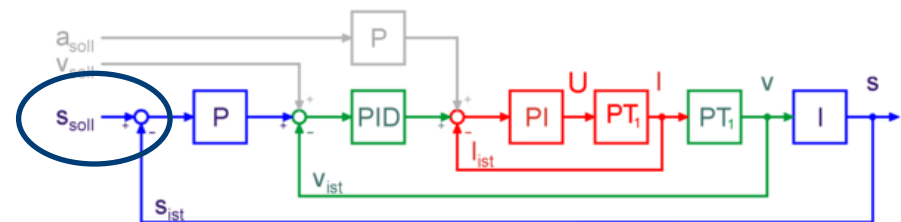
→ Criterium here no good choice



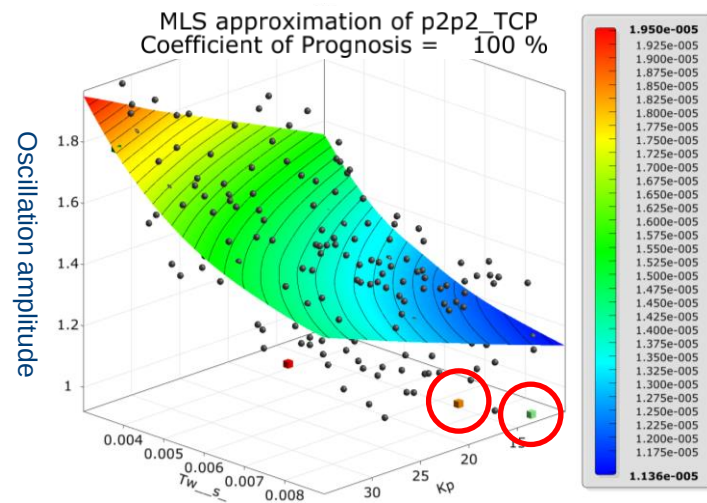
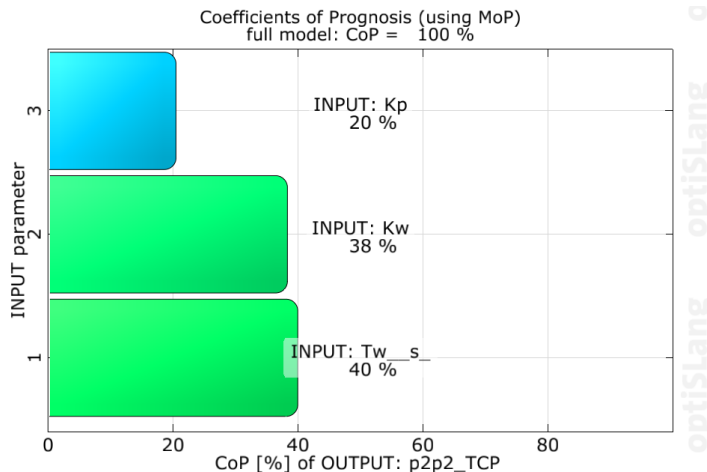
Oscillation amplitude at column basis



- Complete systems behavior at column basis == position of measurement device
- Position control: $k_p \uparrow$ oscillation amplitude $\uparrow$
- Position oscillation amplitude dominated by velocity control



Oscillation amplitude at TCP

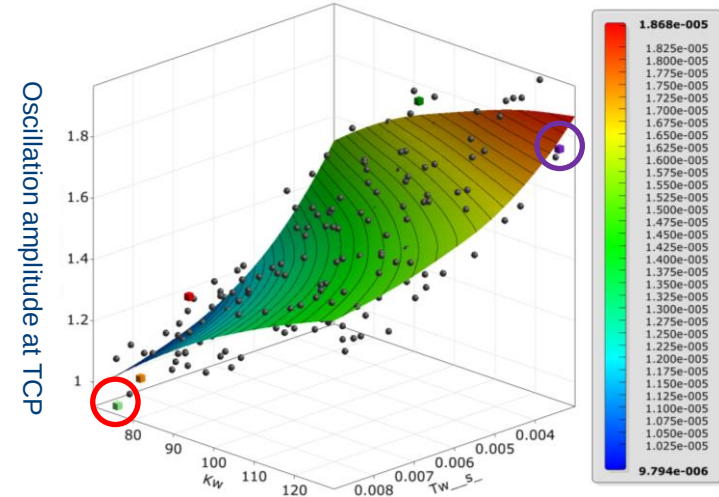
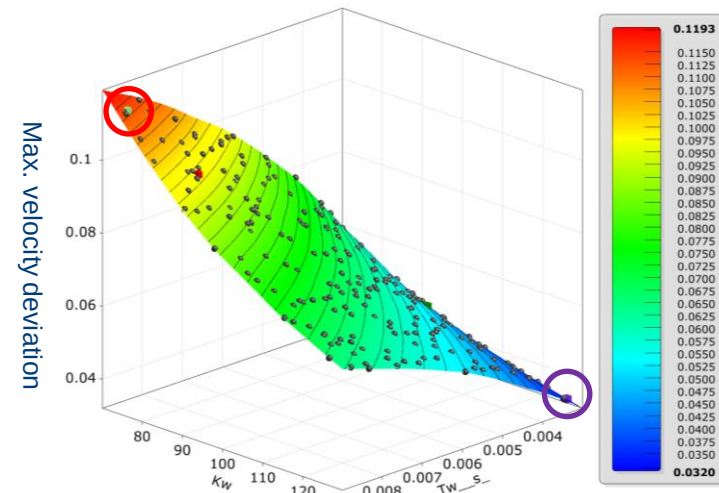
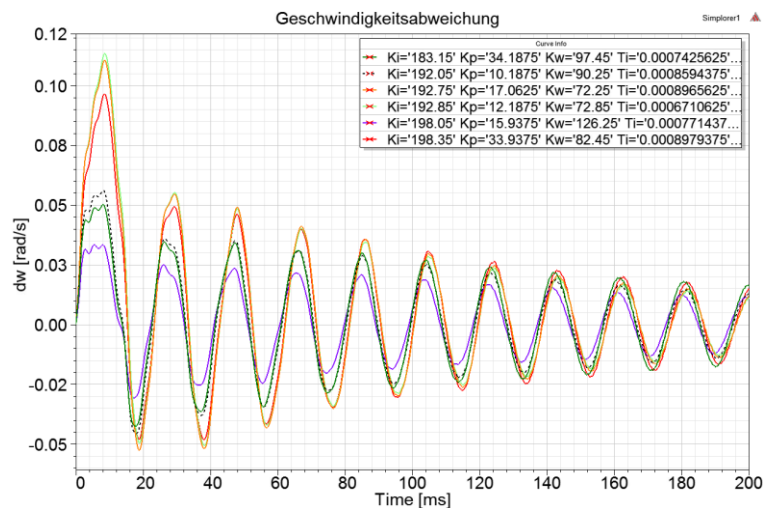


- Investigation of systems behavior at TCP
- In most machines no possibility to measure this behavior
- Relevant for machining results
- Behavior similar to behavior at coulumn basis but not equal → tuning potential
- Position oscillation amplitude dominated by velocity control

Best velocity control = best positioning behavior?

- No!!!
- Parameter (low oscillation @ TCP) $\neq$ parameter (low velocity deviation)!
- aggressive behavior of velocity control leads to high oscillation at

→ Best results through optimization of position and velocity control in one step



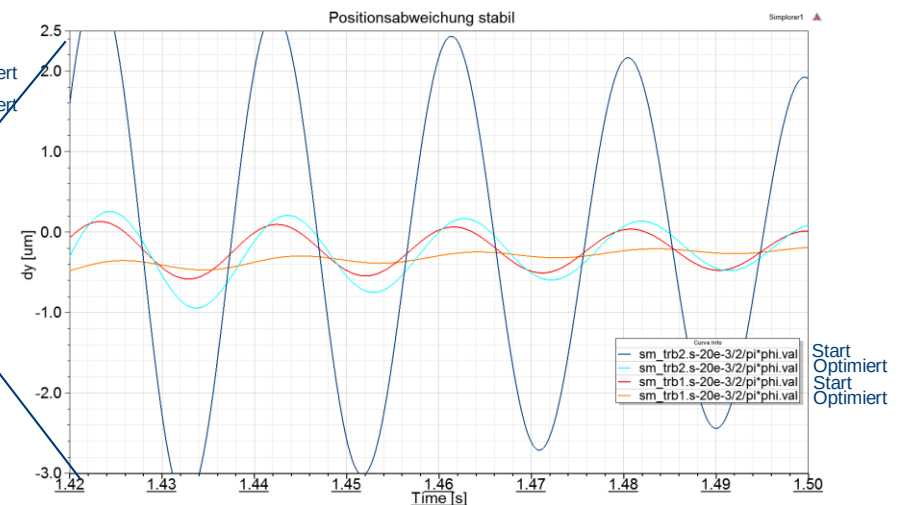
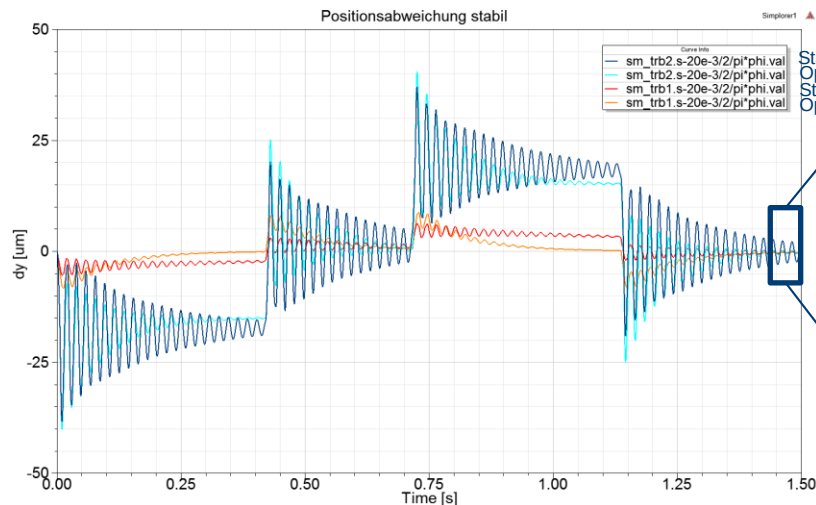
Optimization

- Sensitivity analysis results:
- Position control performance dominated by position and velocity controller
- Current controller in preoptimized shape does not influence position control (as control theory predicts)

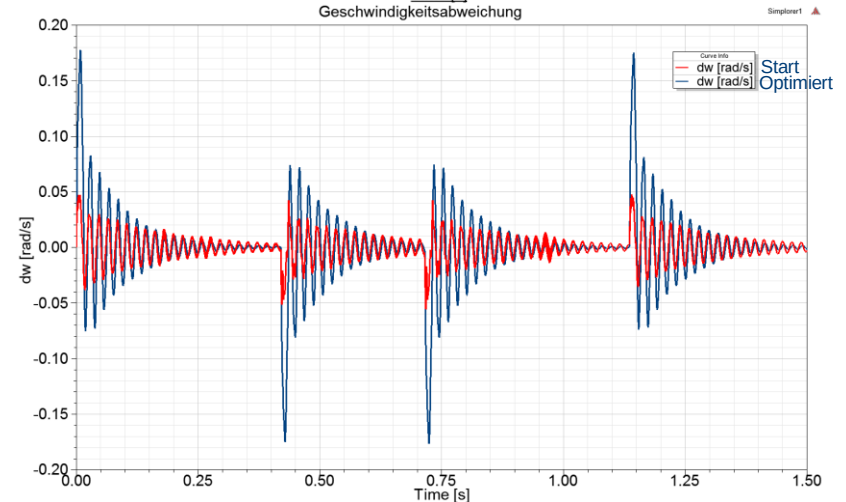
Optimization:

- ARSM
- Objective: minimize oscillation at TCP ($< 2 \mu\text{m p2p}$)
- Constraints: maximum stationary control deviation $1 \mu\text{m}$
- Handle controller parameters for position and velocity control in one optimization run, leave current controller parameters constant

Machine tool behavior at TCP for start values and optimized values



- Automatized optimization of control parameters
- 0.5µm p2p Oscillation at TCP after 1.5s with a stationary position deviation of 0.1µm
- Optimal position control achieved by accepting slight performance losses for velocity control
- Pairing developer know-how with sensitivity analyses and optimization: in very short time excellent results



Conclusion

- Systems simulation: bidirectional interaction of components across different physical domains together with controller interaction
 - Reduced order models: Excellent balance between speed and accuracy
 - Parameterized Systems: automatized determination of optimal parameters
 - Taking into account the nonlinearities of the system
-
- Better understanding of the systems behavior
 - Avoid late stage integration failure
 - reduce costs for physical testing

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