

/ VIRTUAL WOST 2021

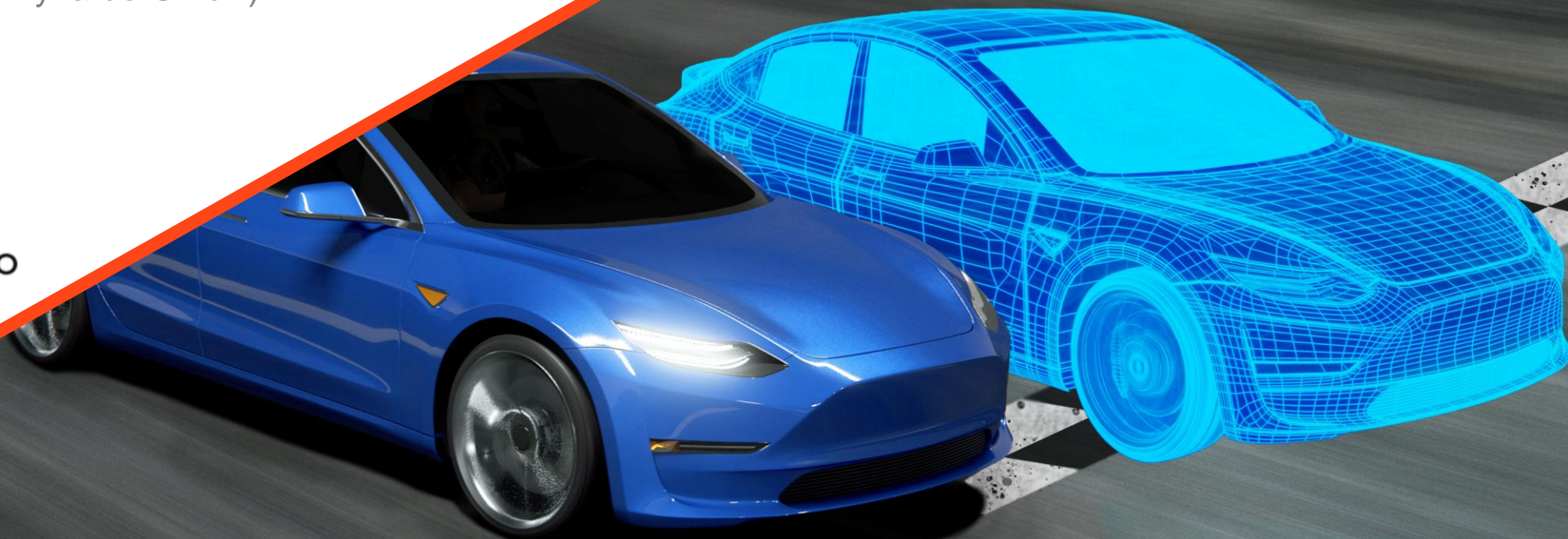
COMPAS

Metamodels generated from thermo-mechanical simulation for the design of a test setup for microelectronics packages

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Roland Niemeier (ANSYS Dynardo GmbH)



June 17th 2021





COMPAS

Compact modelling of high-tech systems for health management and optimization along the supply chain



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L I G H T Y E A R





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Motivation

2

Step #1: Homogenization for reducing computational effort

3

Step #2: AMOP analysis of test setups

4

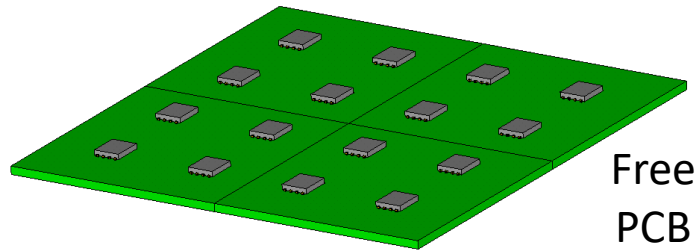
Outlook: “Fragility surface plots”

5

Summary

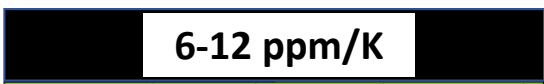
Tested for at Tier2

Solder fatigue due to CTE mismatch of components vs. PCB



Free PCB

Microelectronics package

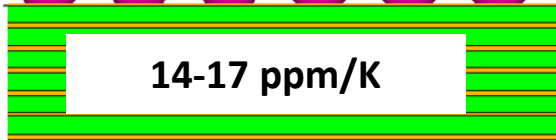


6-12 ppm/K

Solder balls

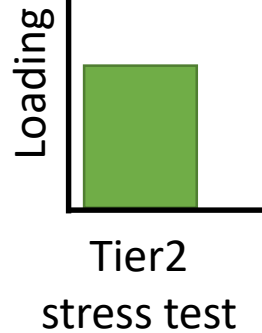
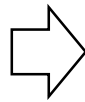
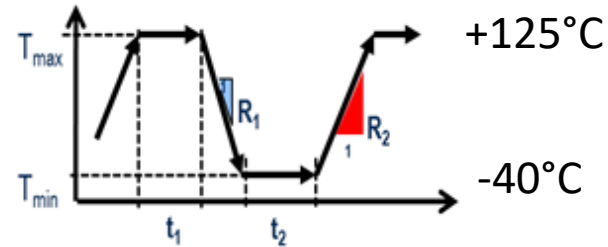


PCB



14-17 ppm/K

Temperature cycling (accelerated test)



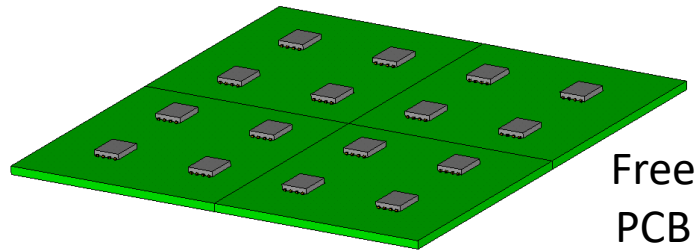
Source: [2]

[1] R. Dudek *et al.* , Results TRACE/CATRENE, EuWoRel 2018.
 [2] G. Haubner *et al.*, "77 GHz automotive RADAR", Microelectronics Reliably , 2016.
 [3] M. van Soestbergen *et al.* , COMPAS, EuWoRel 2020.

- Solder fatigue is one of the major failure modes in automotive hardware

Tested for at Tier2

Solder fatigue due to CTE mismatch of components vs. PCB



Free PCB

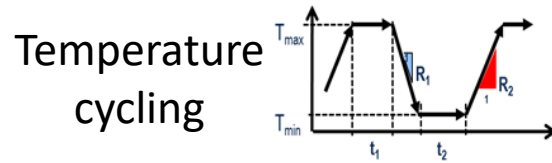
Microelectronics package

6-12 ppm/K

Solder balls

PCB

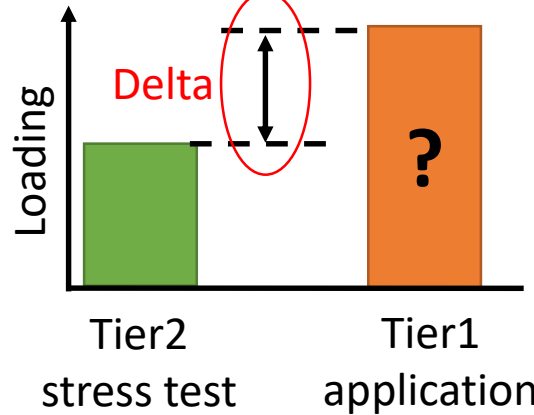
14-17 ppm/K



Temperature cycling

Consequence:

Unknown delta



Tier2

stress test

Tier1

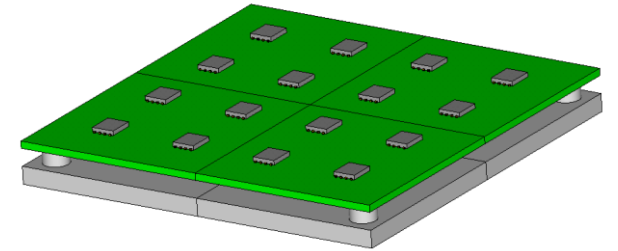
application



Source: [2]

Not tested for at Tier2

Solder fatigue due to external PCB bending from Tier1 ECU housing



Free PCB

External bending

-40°C



+125°C

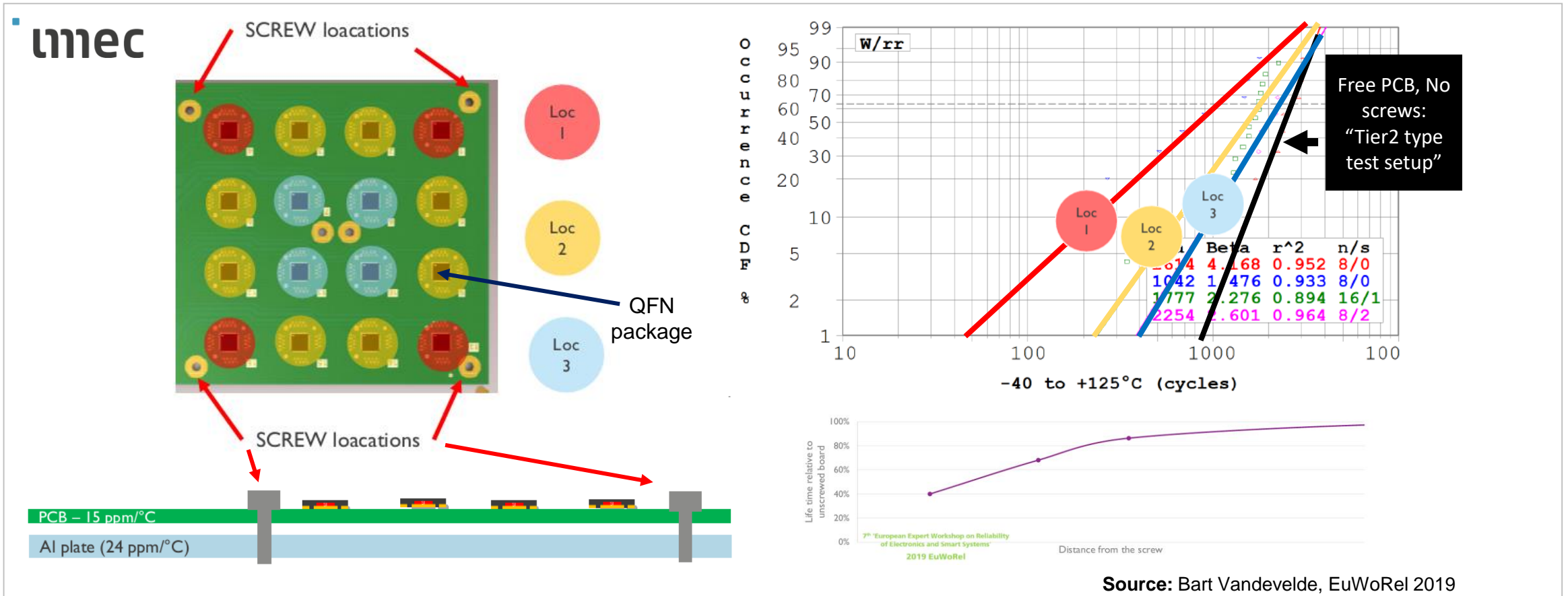


[1] R. Dudek *et al.*, Results TRACE/CATRENE, EuWoRel 2018.

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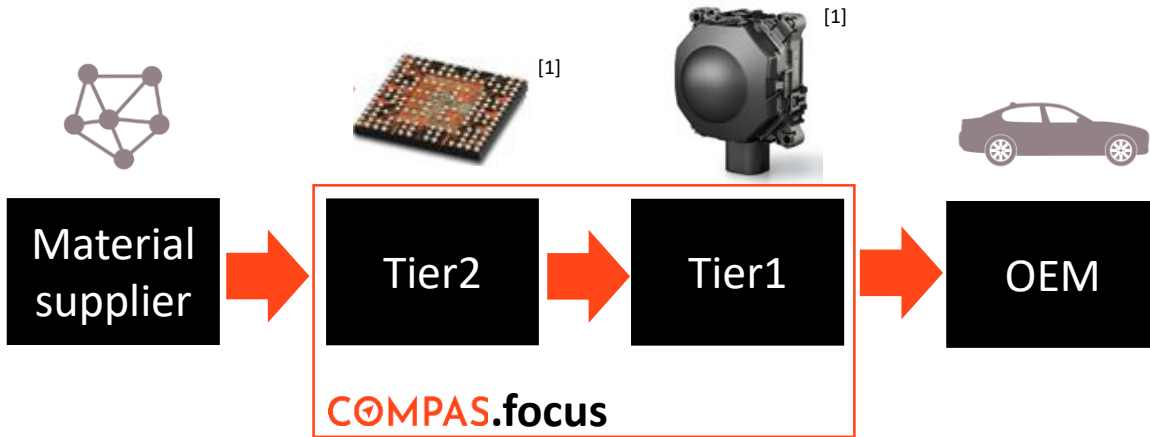
[3] M. van Soestbergen *et al.*, COMPAS, EuWoRel 2020.

- Solder fatigue is one of the major failure modes in automotive hardware
- Tier2 tests do not cover all possible loading conditions at Tier1



- Bart Vandeveld (IMEC) demonstrated the impact of PCB mounting on solder joint reliability using a simplified test setup

COMPAS.idea:



[1] M. van Soestbergen *et al.*, COMPAS, EuWoRel 2020.

Pass along thermo-mechanical compact models

Feedback data about loading conditions

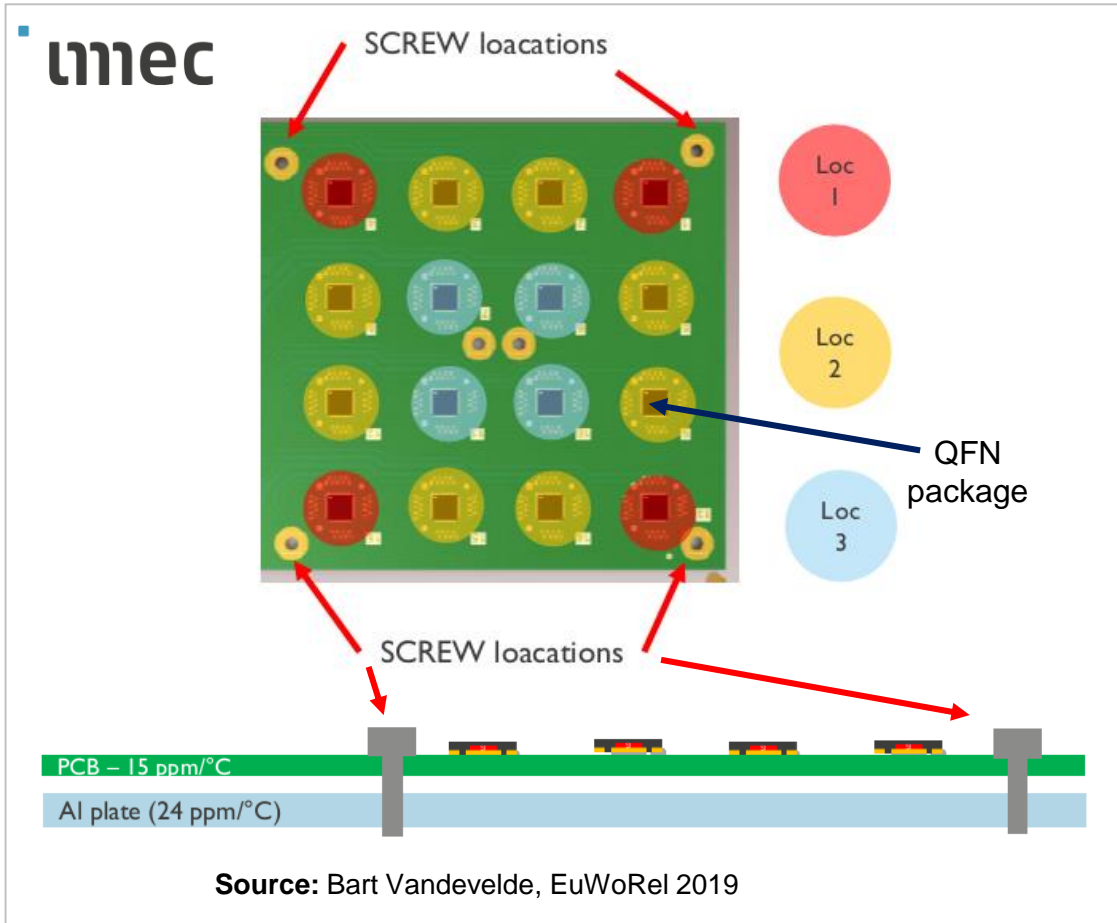
COMPAS.paradigm

- Thermal compact models are already standardized and passed along value chain

COMPAS.challenge

- Thermo-mechanics is more complex
- No suitable automatic compact modeling frameworks or standardized exchange formats yet
- Reduction of computational effort
- IP-safe compact models

- COMPAS funding project aims at developing thermo-mechanical compact models



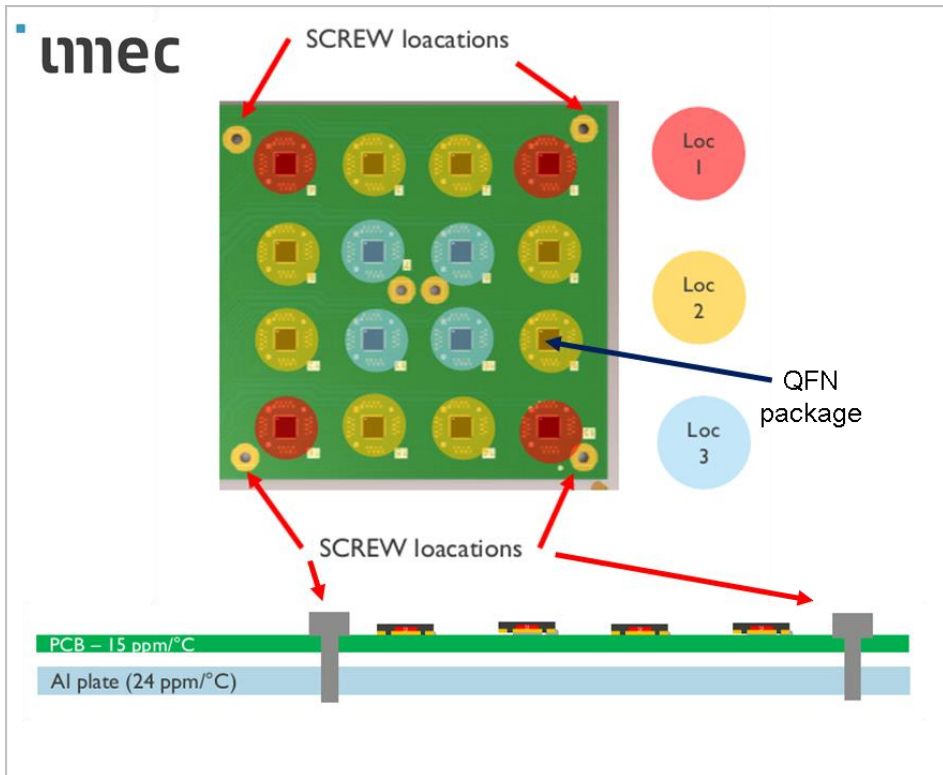
COMPAS.validation

- Rebuild the setup used by IMEC for experimental validation of thermo-mechanical compact models
- Adapt the design used by IMEC to the type of packages investigated in COMPAS
- Understand sensitivities of this setup and generate MOP for discussion with layout/test

- For the validation of the compact models developed in COMPAS, a tailored test setup shall be developed based on the concept used by Bart Vandeveld

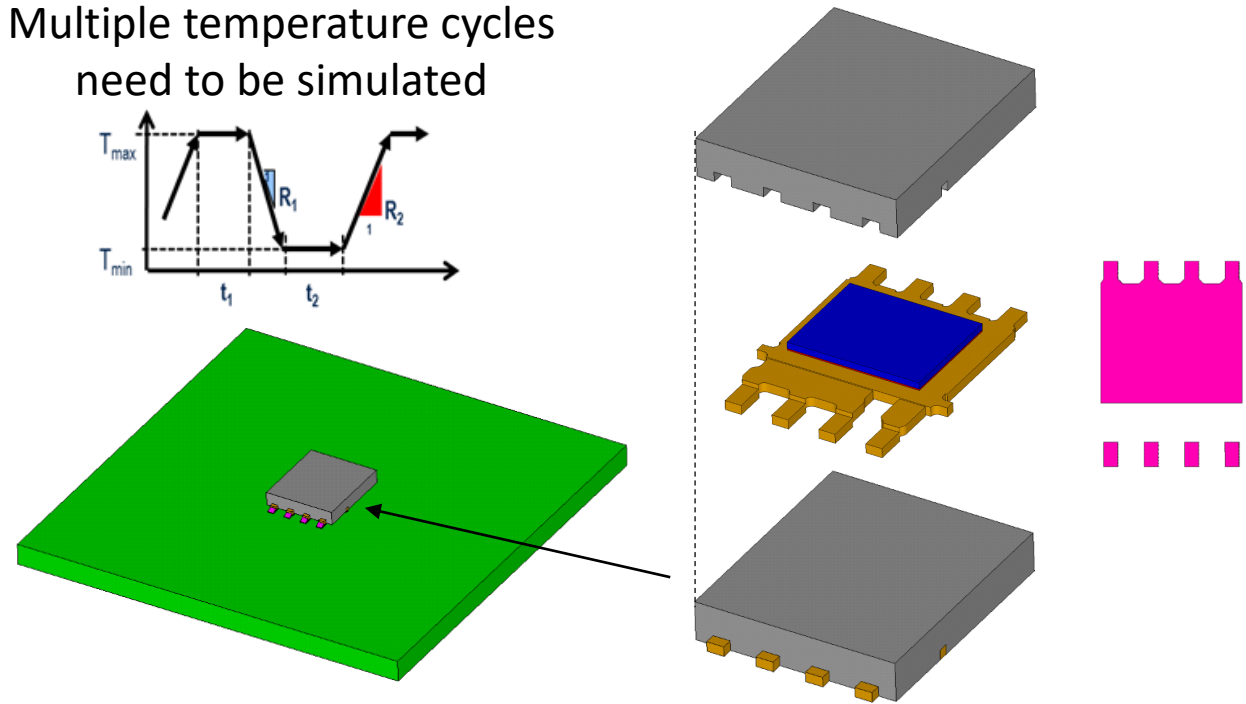
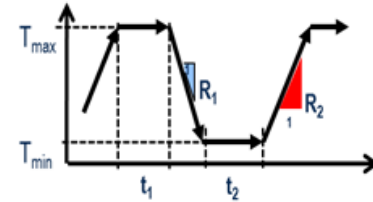


- 1 Motivation
- 2 **Step #1: Homogenization for reducing computational effort**
- 3 Step #2: AMOP analysis of test setups
- 4 Outlook: “Fragility surface plots”
- 5 Summary



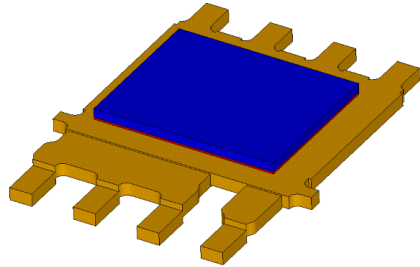
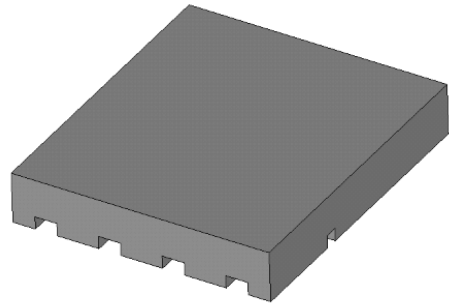
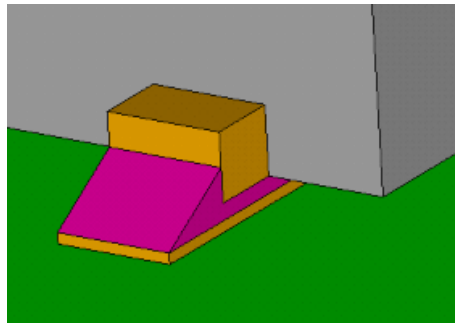
Source: Bart Vandeveld, EuWoRel 2019

Multiple temperature cycles need to be simulated

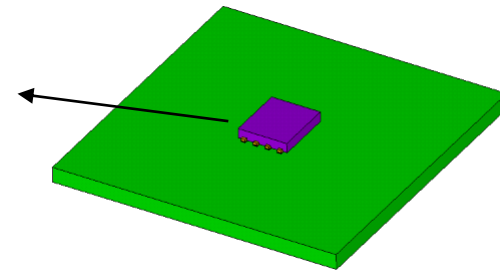
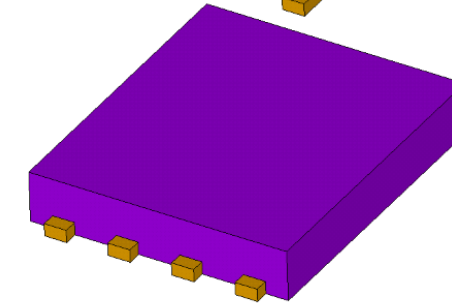
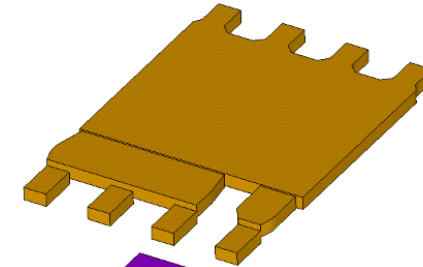
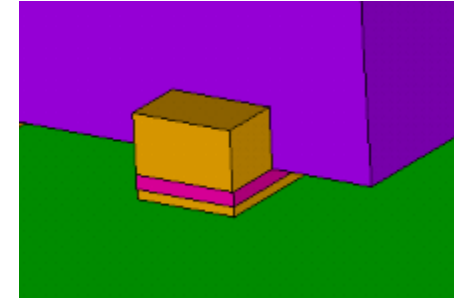
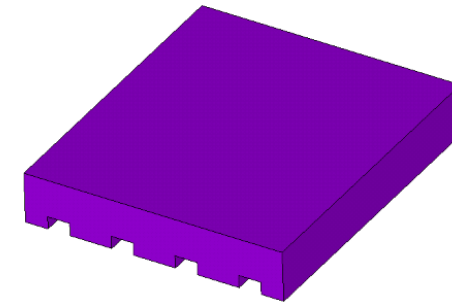


Effort for a solder joint analysis run for one (detailed) package on one PCB:
x*hours @ 40 cores

- In order to perform thermo-mechanical simulation of such a setup with multiple packages, the computational effort of the package model needs to be reduced



De-feature manually & Homogenize by AMOP

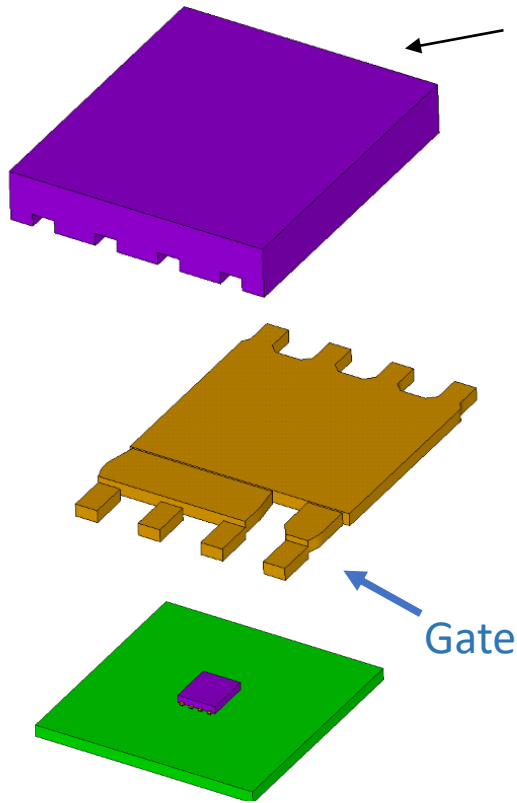


Note:
Non-productive BoM is chosen in order to reduce duration of test

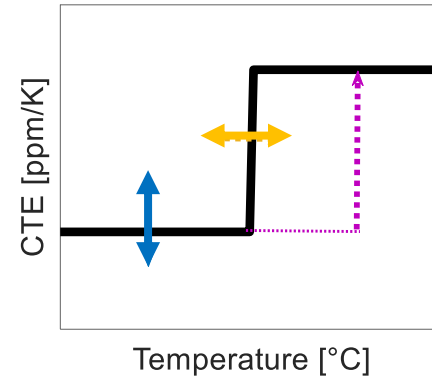
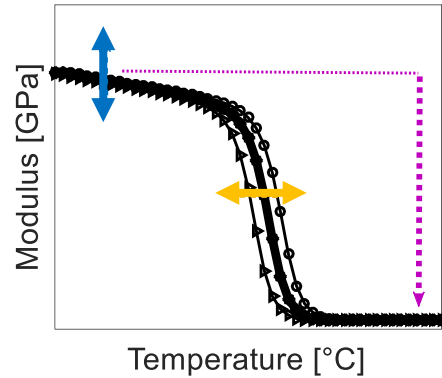
x*hours @ 40 cores

x*minutes @ 40 cores

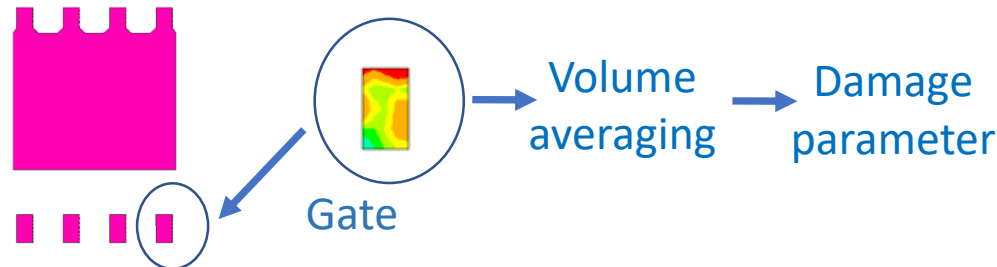
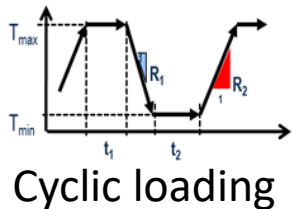
- Since COMPAS approach is still being developed, a mixture of manual de-features and homogenization using optiSLang AMOP is used



WHAT: Effective linear-visco-elastic material model shall be used for homogenized block

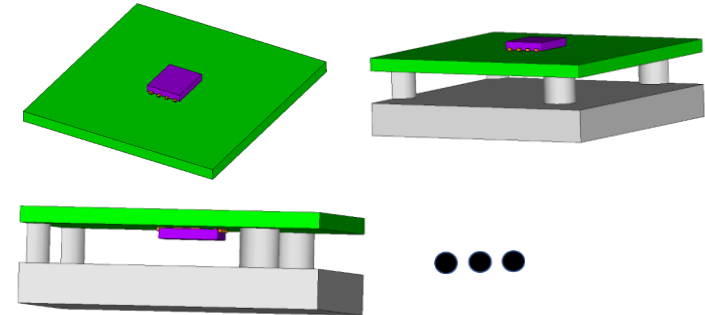


CRITERION: Loading of gate solder joint is evaluated as criterion for homogenization



Merged objective:

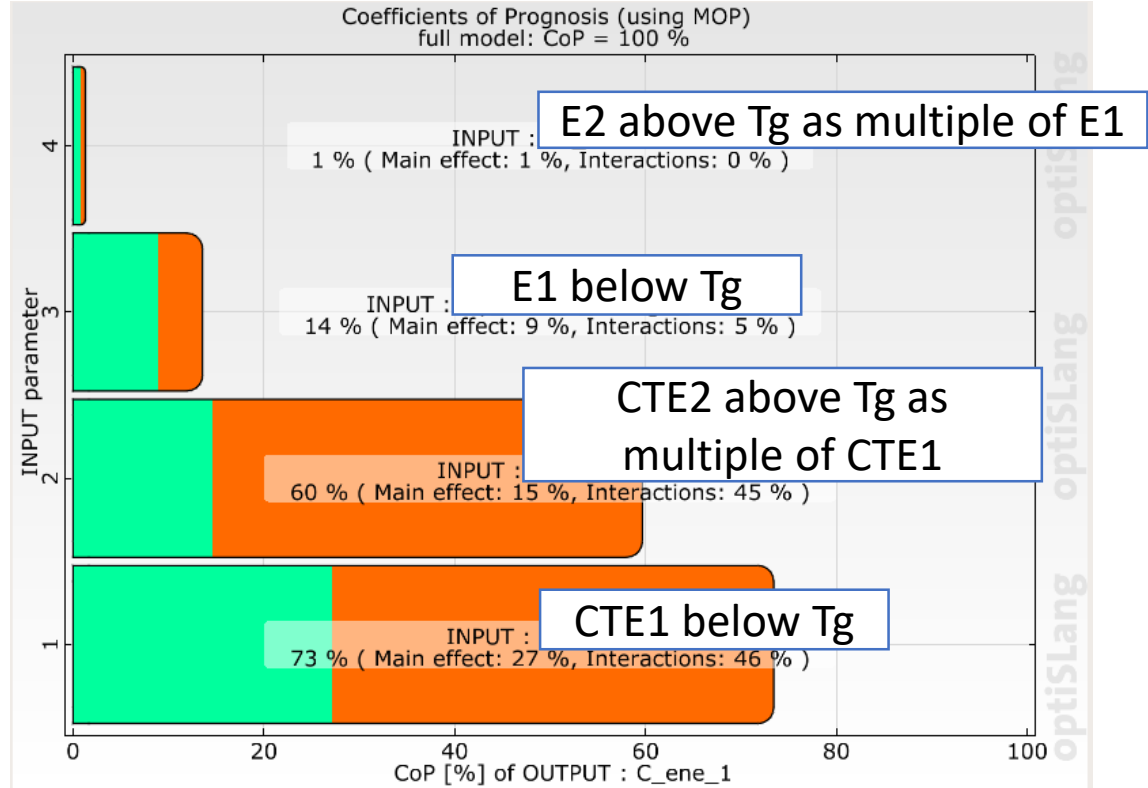
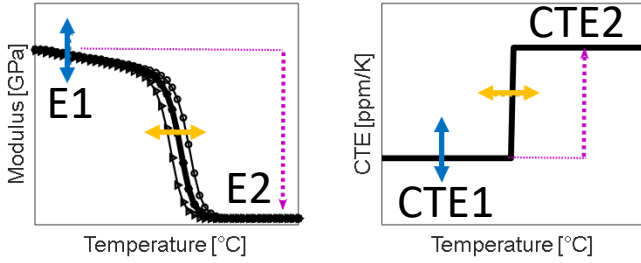
- High weighting on capturing relative change in loading of different configurations



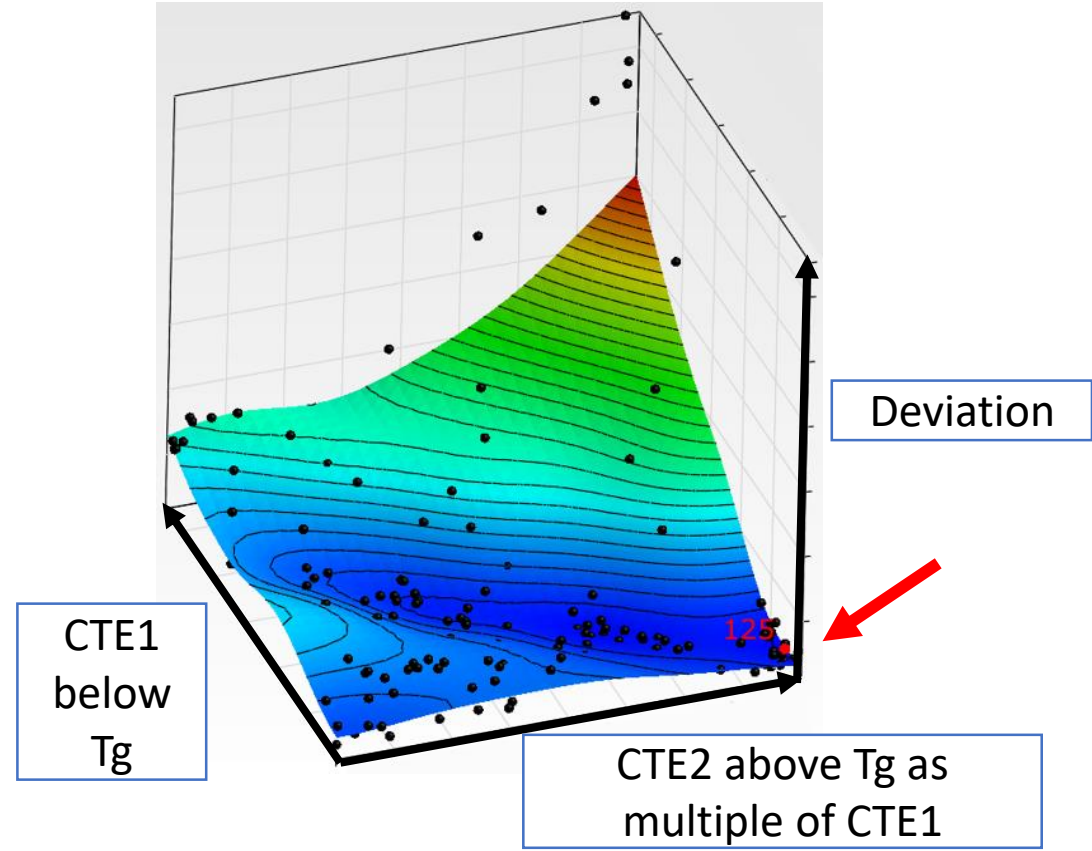
- Reduced weighting on quantitative accuracy (solder joint geometry changed)

- Effective linear-visco-elastic material model is calibrated using the loading of the gate solder joint (→ damage parameter) as a criterion

As per design:
Strong interactions



Response surface from AMOP shows important trends helping to select parameters



- Best design/parameters selected and confirmed using additional considerations
- Reduced model has only 10% of DOFs and 5% of compute time of full model



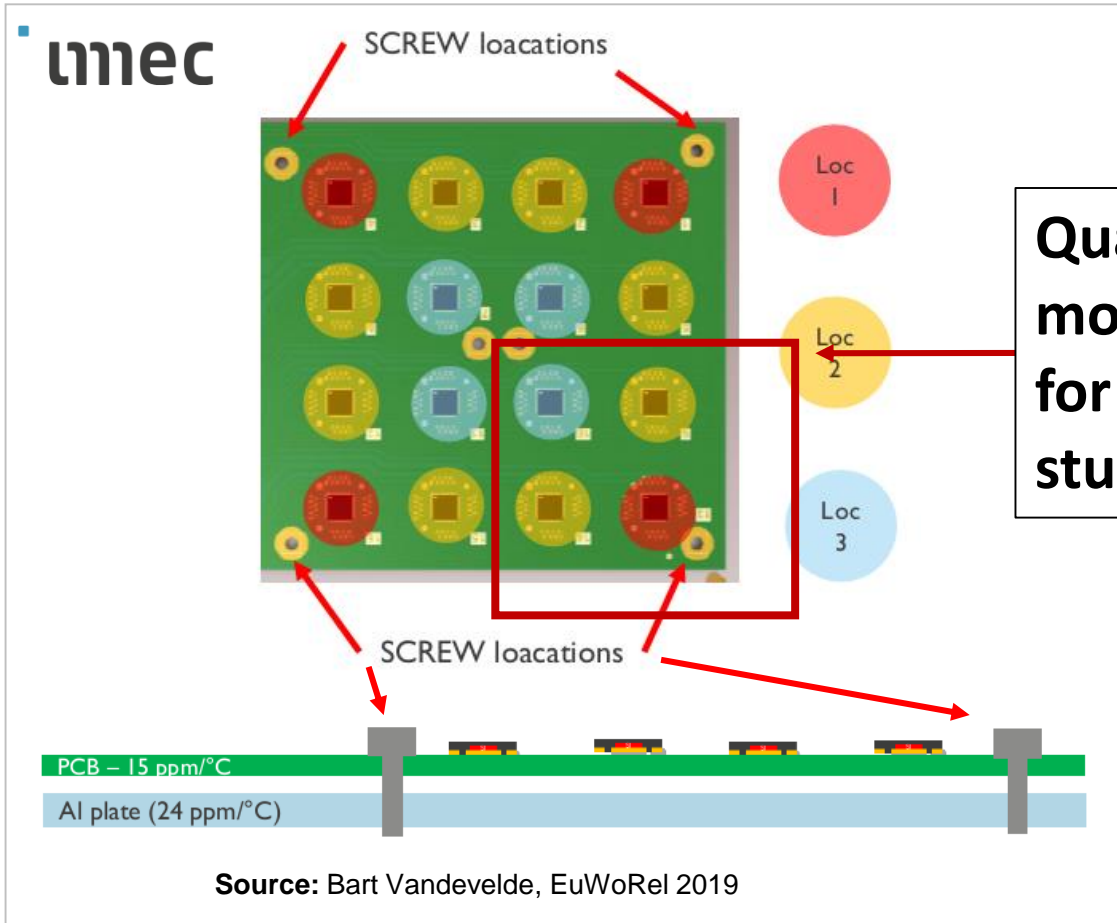
1 Motivation

2 Step #1: Homogenization for reducing computational effort

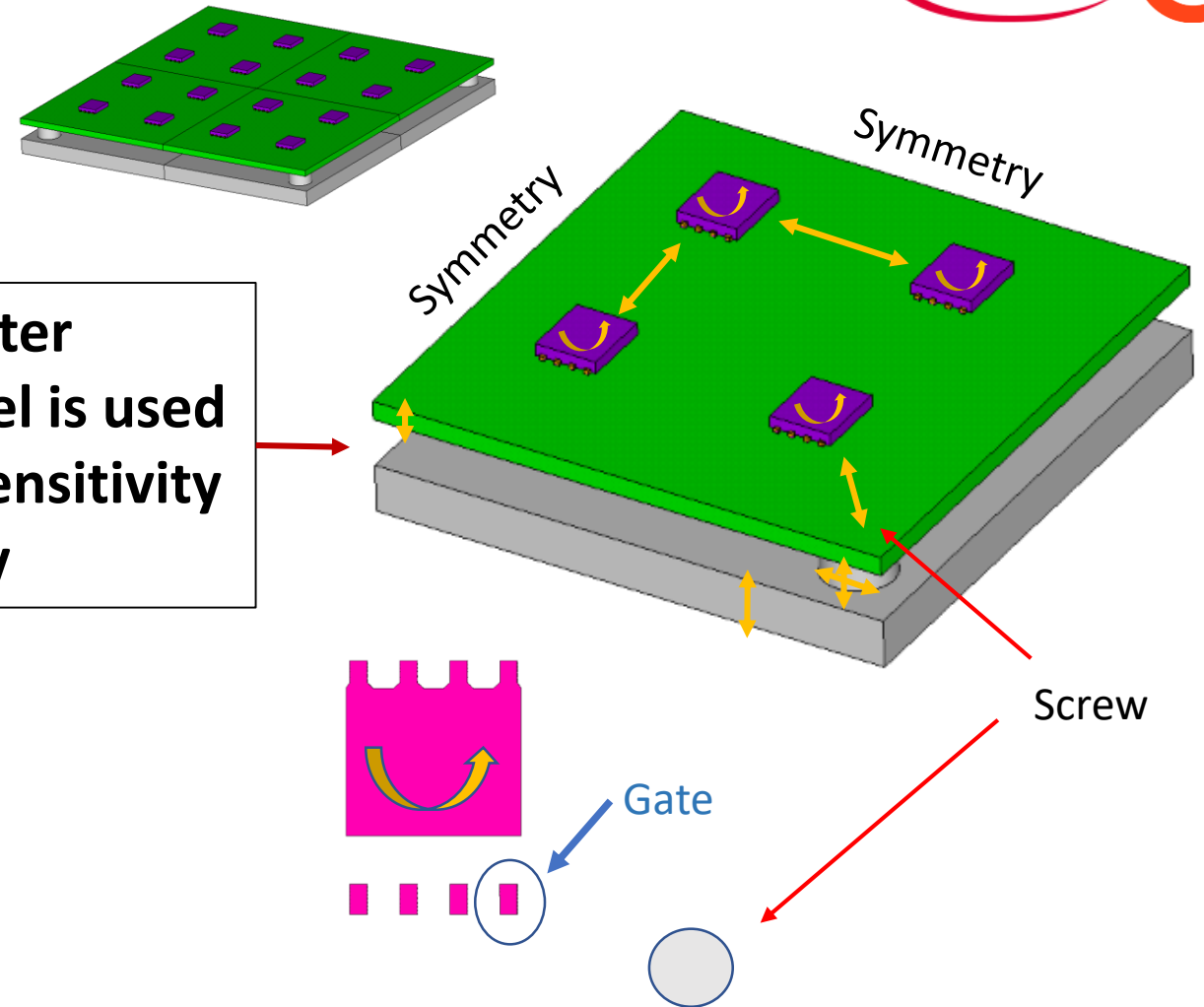
3 Step #2: AMOP analysis of test setups

4 Outlook: “Fragility surface plots”

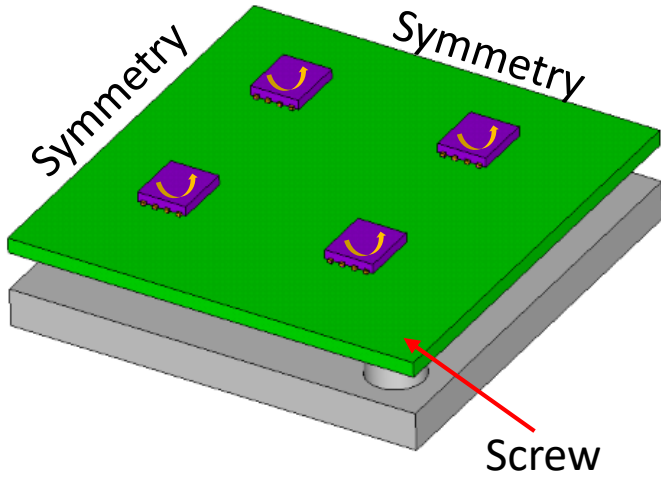
5 Summary



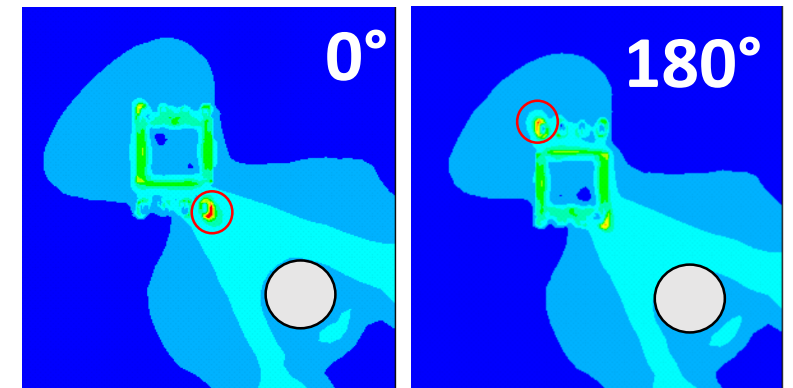
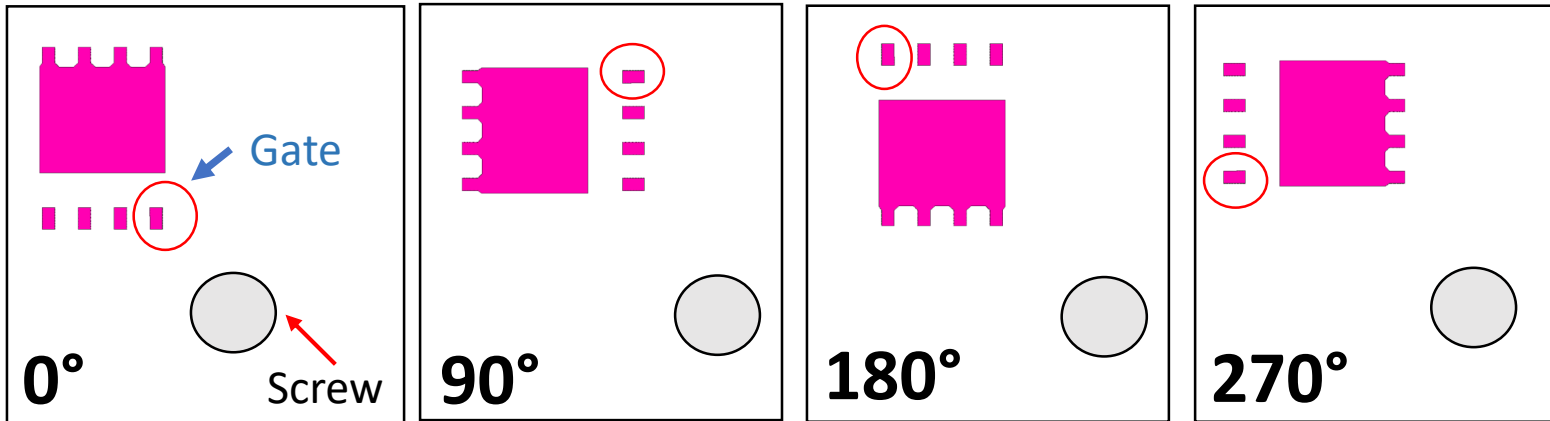
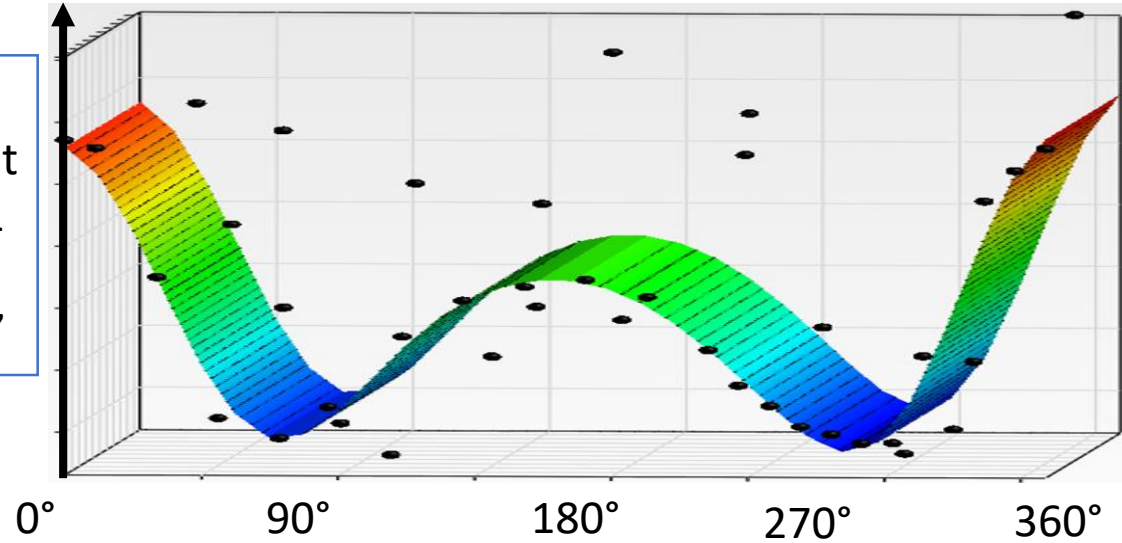
Quarter model is used for sensitivity study



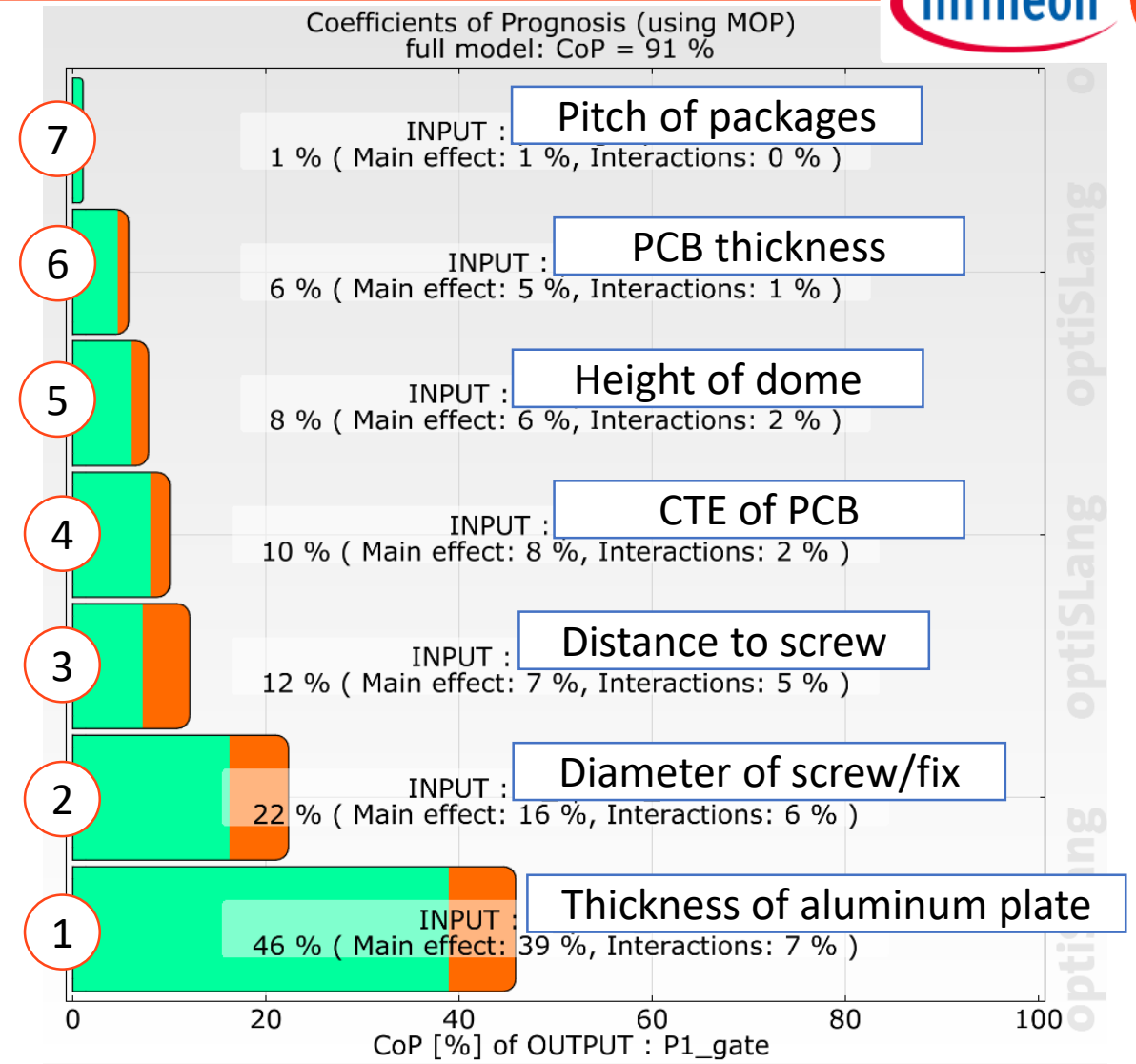
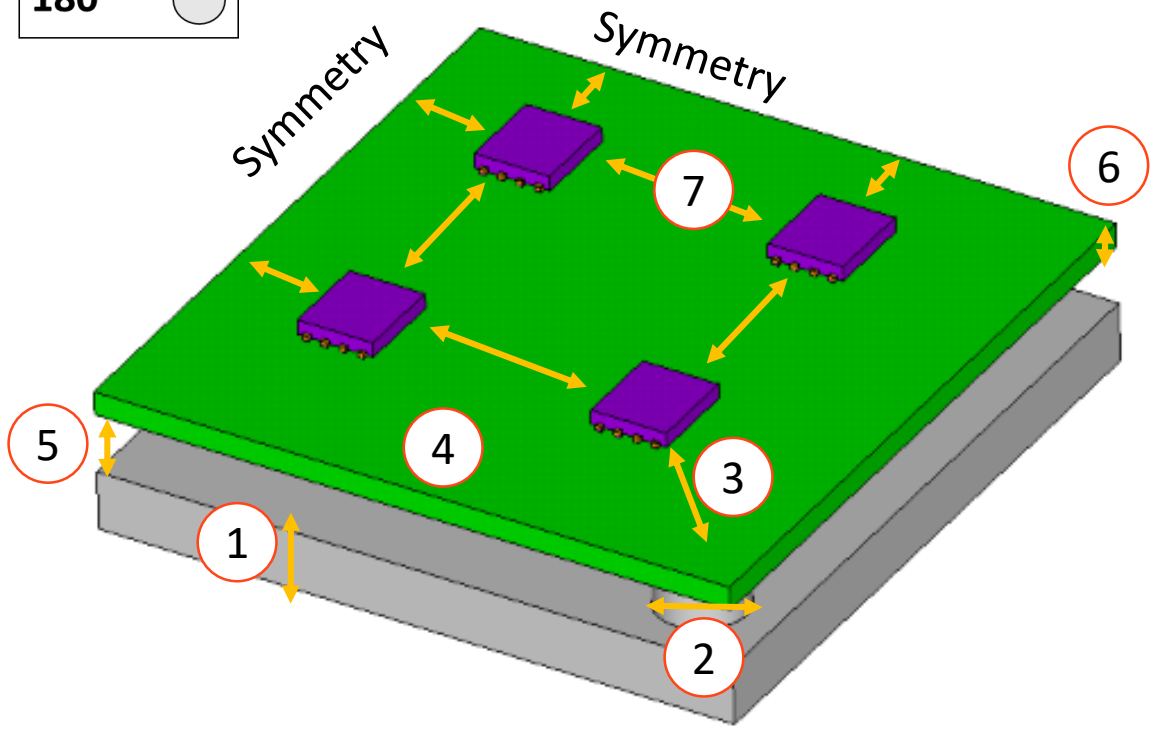
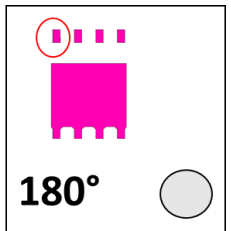
- Quarter model is used for performing a sensitivity study (AMOP) → MOP
- Focus is to design a setup which leads to high loading → short testing times



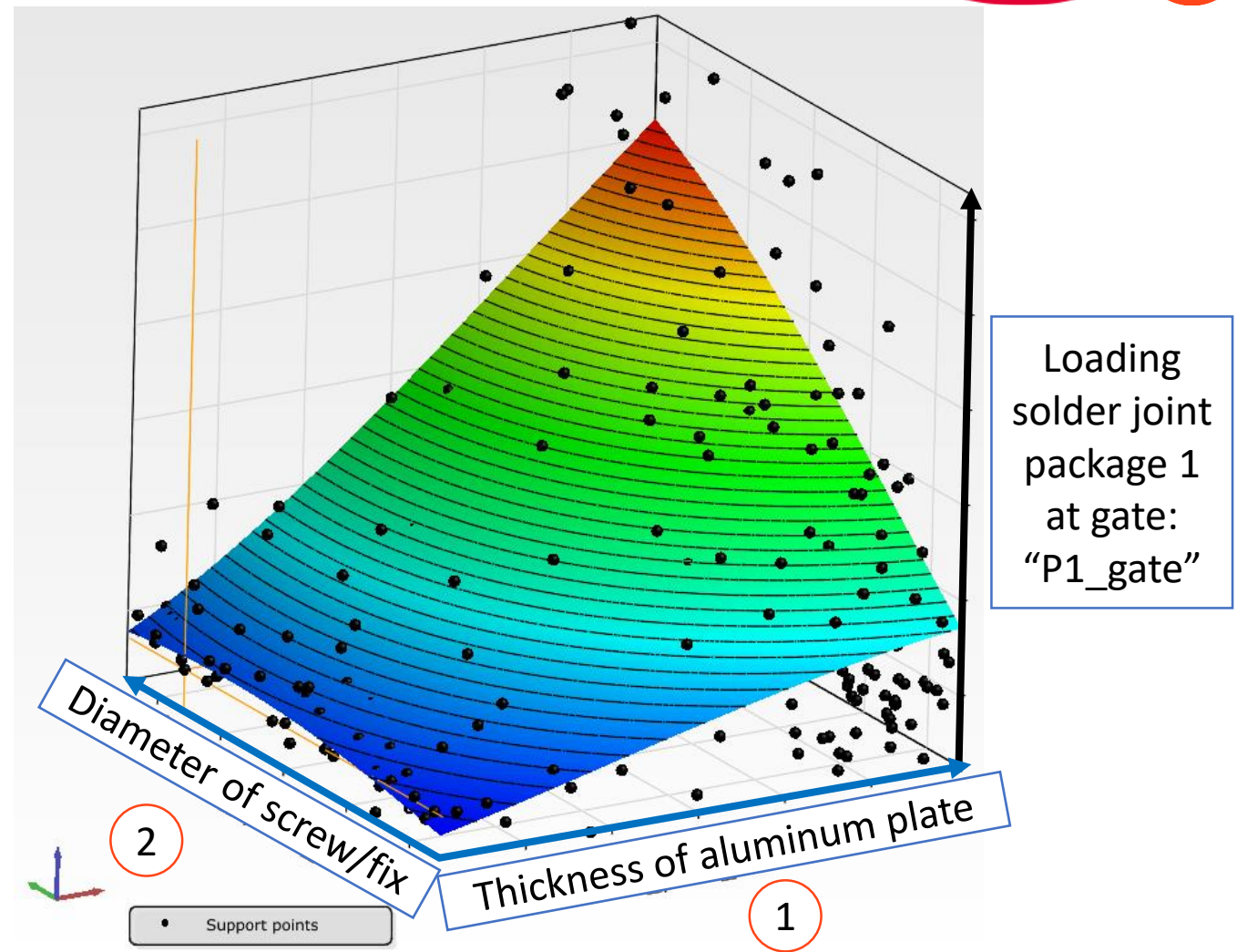
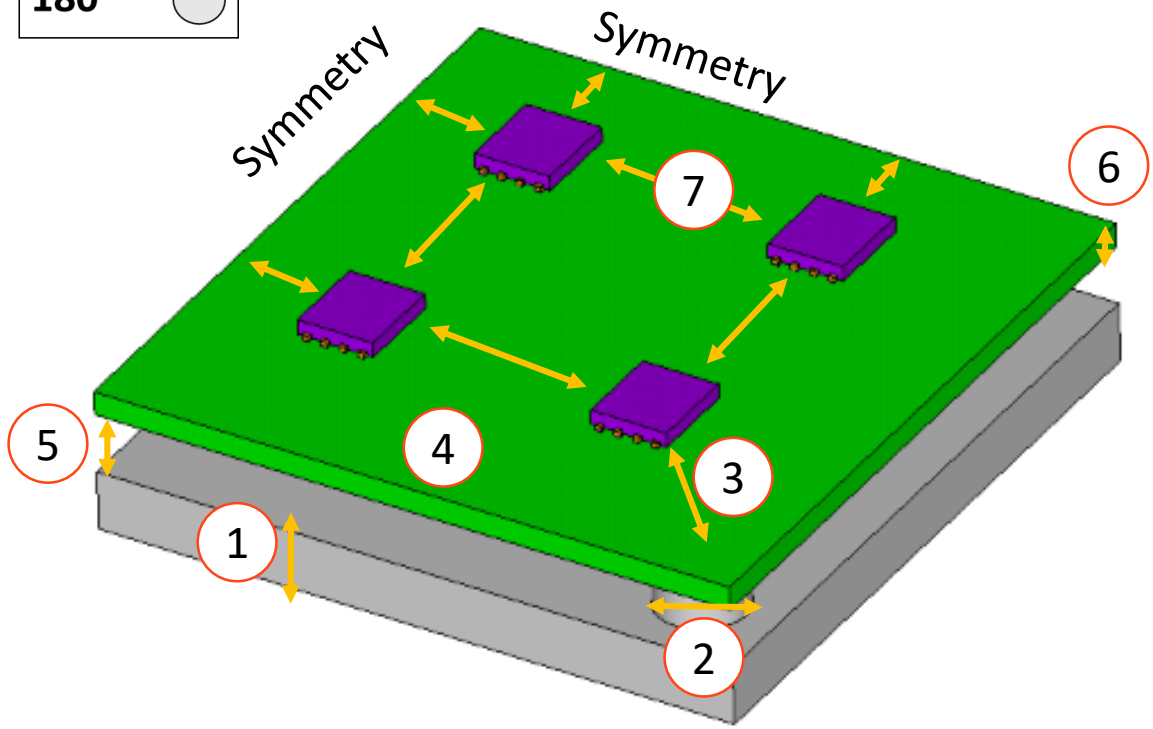
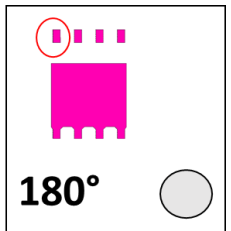
Loading solder joint package 1 gate: "P1_gate"



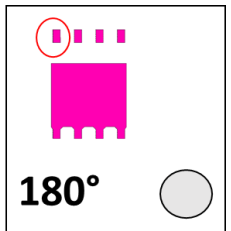
- Rotation of asymmetric footprint w.r.t. screw has high impact
- Rotation of 180° is chosen



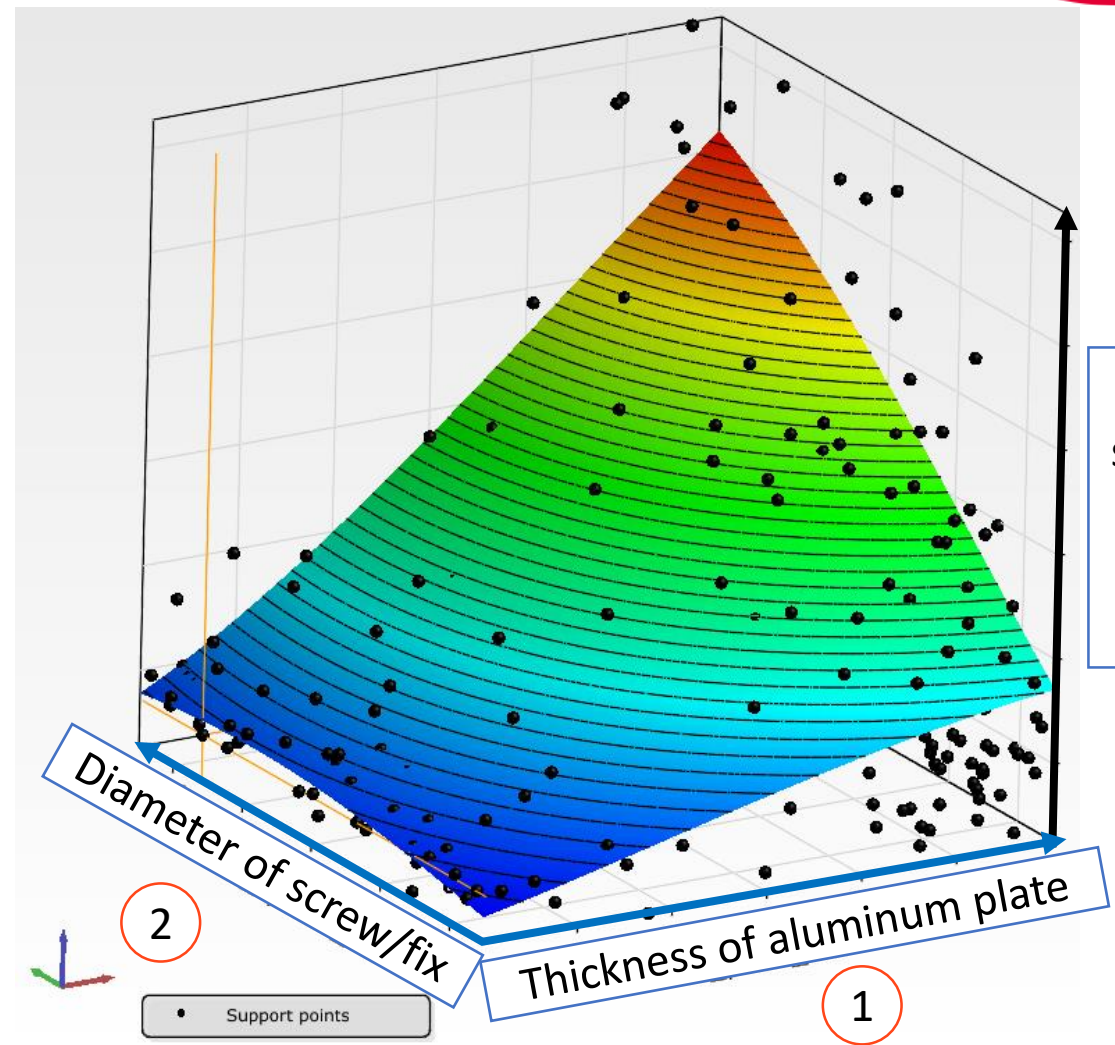
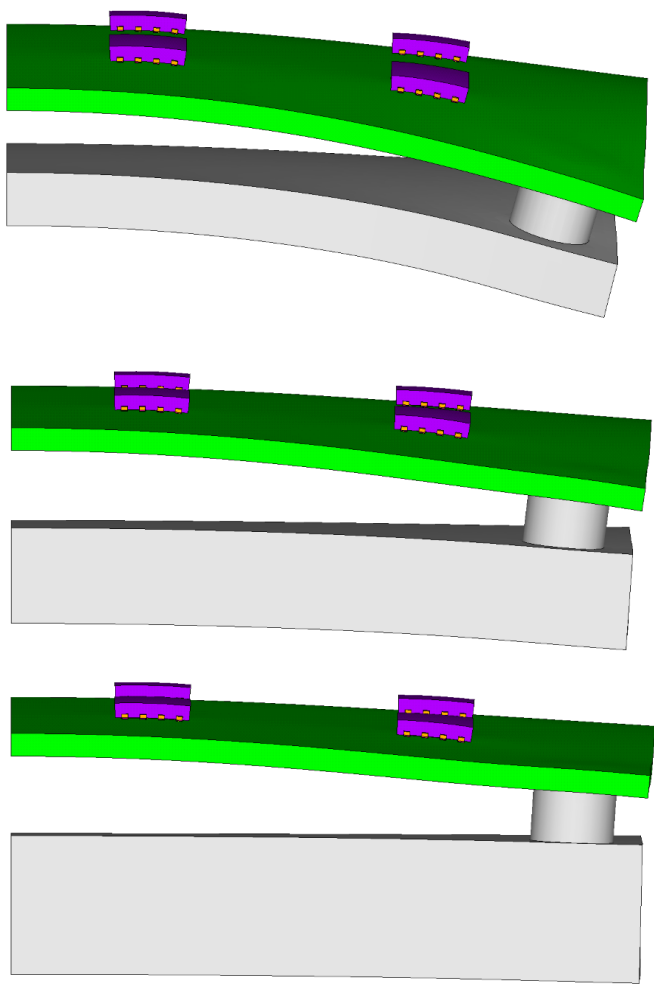
- Highest impact not from distance to screw, but from thickness of aluminum plate and diameter of screw/fix



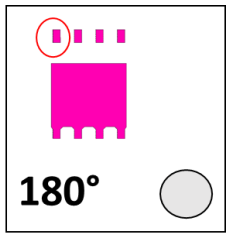
- Highest impact not from distance to screw, but from thickness of aluminum plate and diameter of screw/fix



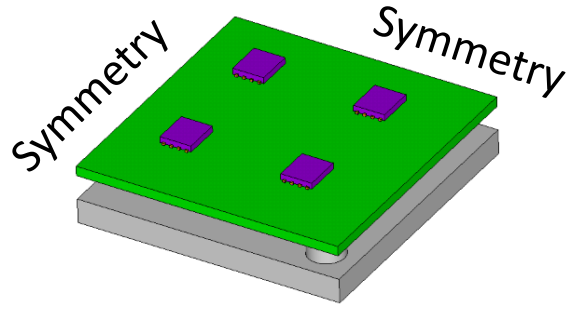
Deformation plots at -40°C
Factor 100x over-scaled



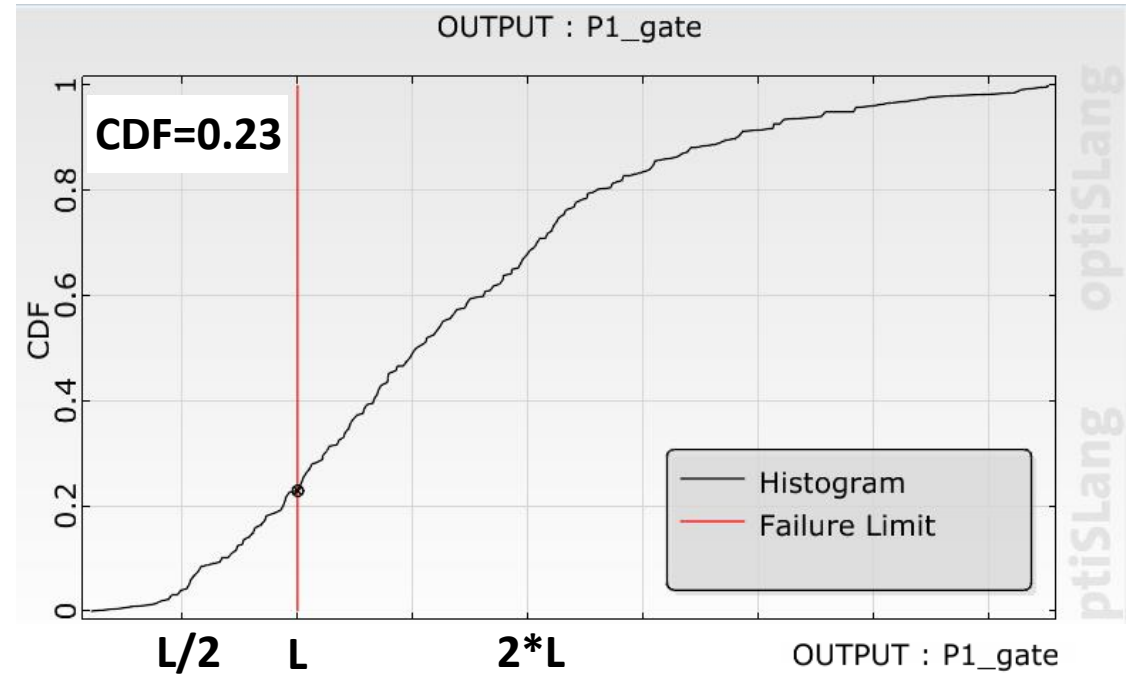
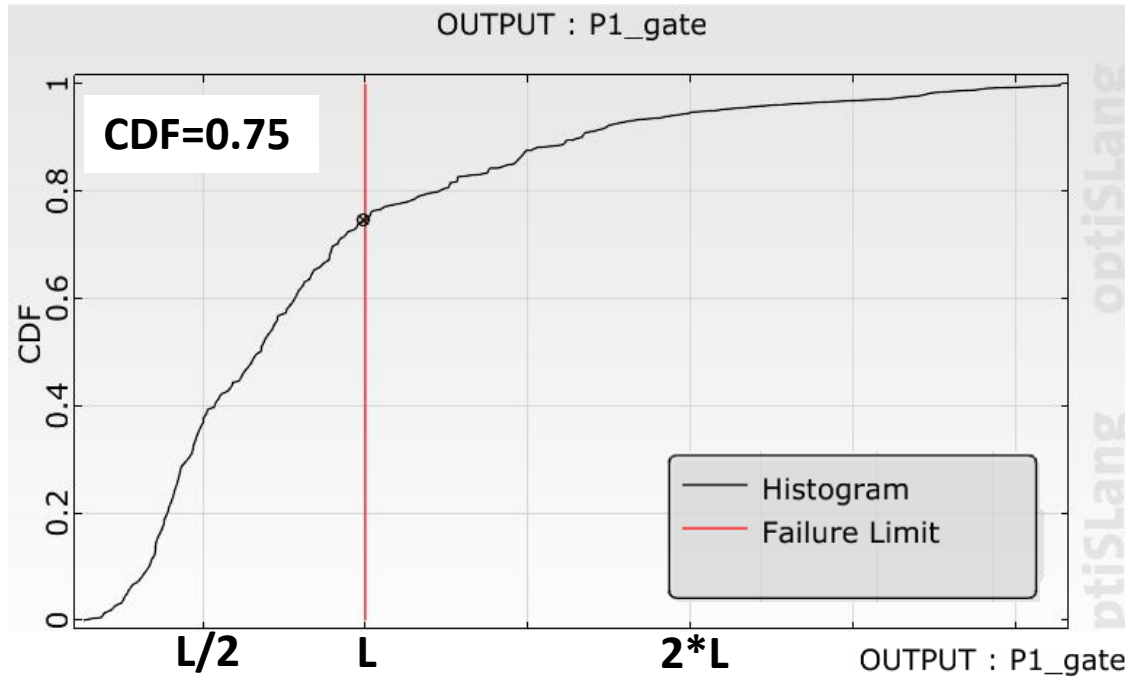
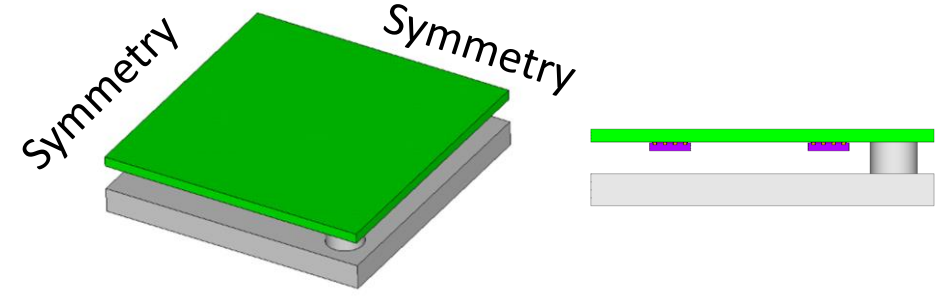
- Thicker aluminum plate will result into stiffer step, no longer bend and, consequently, induce more stress into PCB



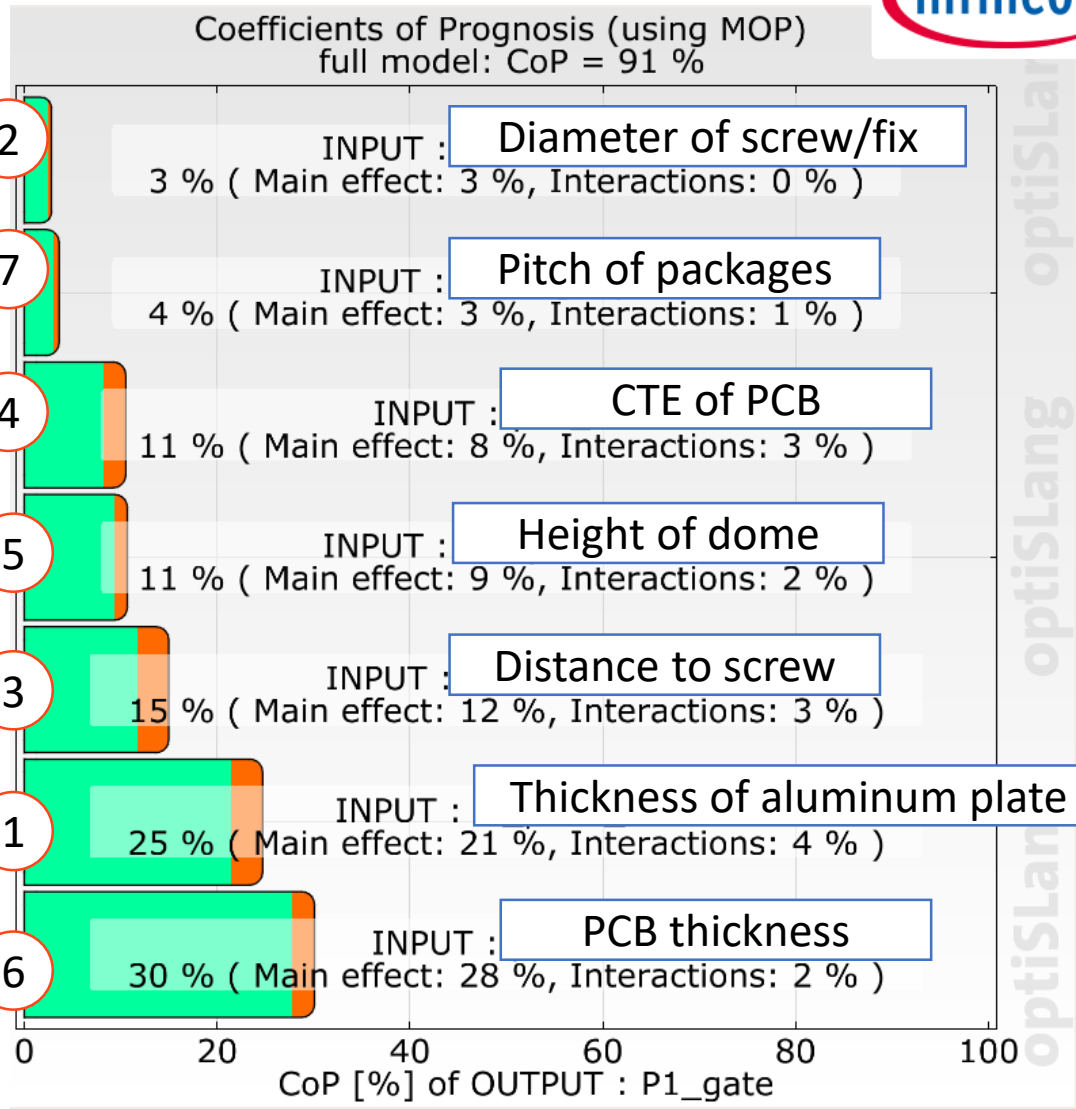
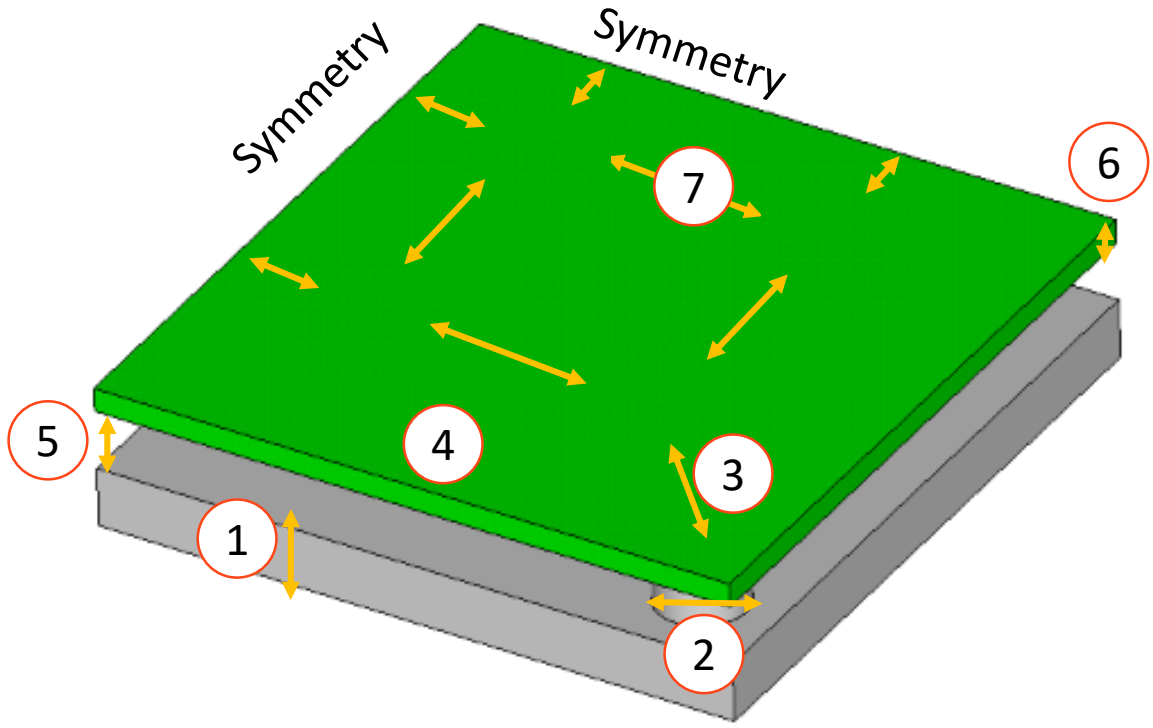
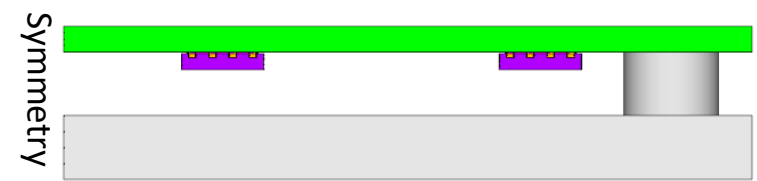
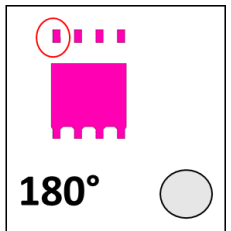
Config #1



Config #2



- Flipped PCB leads to overall increased loading
- CDF: For arbitrarily selected limit L , config #1 has 3x designs below limit than #2



• CoP ranking of parameters changes significantly



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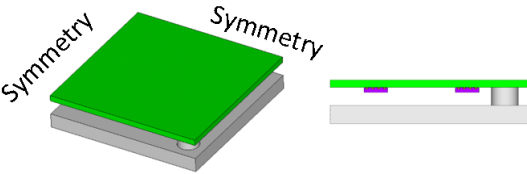
Outlook: “Fragility surface plots”

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Summary

Question:




Which loading is achieved with which distance to screw when the PCB varies?

Config: **Config #2** 

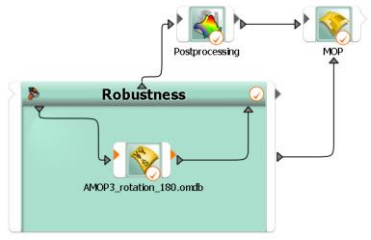
Fixed:

- Thickness of aluminum plate
- Pitch of packages
- Height of dome
- Diameter of screw/fix

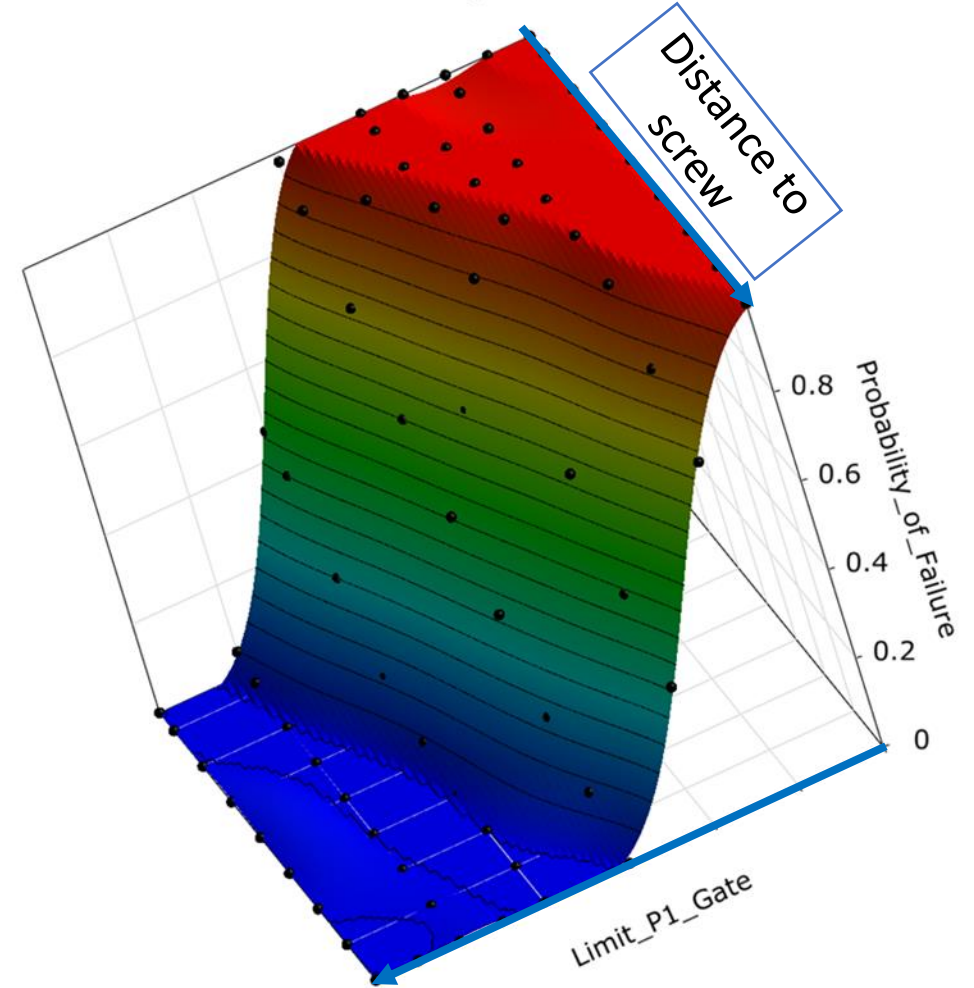
Vary:

PCB thickness	Opt.+Stoch.		UN...	+/- 5%
CTE of PCB	Opt.+Stoch.		UN...	+/- 7%
E-modulus of PCB	Opt.+Stoch.		UN...	+/- 7%

➔ Distance to screw



Isotropic Kriging approximation of Probability_of_Failure
Coefficient of Prognosis = 100 %



- "Fragility" surface plots allows for thorough analysis of this impact



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Summary

- optiSLang AMOP functionality was successfully used to calibrate a homogenized simulation model which allowed to significantly reduce the computational effort
- optiSLang AMOP functionality was successfully employed to study the sensitivities of two test setup configurations w.r.t. solder joint loading:
 - Strong difference in overall loading level as well as sensitivity to the individual parameters was identified
- “Fragility surface plots” are investigated in order to assess the impact of PCB variation w.r.t. solder joint loading of the test setups
- Next step: Use MOPs for discussion with layout and test teams in order to develop the test setup

COMPAS

Thank you for your attention!